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NRL Memorandum Report 5160

Data Validation and Summary for the NRL Remote Sensing Experiment:
Phelps Bank, July, 1982

Part II: Meteorology

J. A. C. KAISER

Ocean Dynamics Branch Marine Technology Division

R. A. MUNCH

Sociative man Americana, Inc.

August 26, 1983

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NAVAL RESEARCH LABORATORY Washington, D.C.

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DATA VALIDATION AND SUMMARY FOR THE NRL REMOTE SENSING EXPERIMENT: PHELPS BANK, JULY, 1982

Part II: Meteorology

I. INTRODUCTION

For several years, Synthetic Aperture Radar (SAR) images of the sea surface revealed planar signatures which were remarkably similar to the bathymetric contours below the water in depths less than about 30m. Such sea-surface bathymetric signatures were also observed by side-looking airborne radar (SLAR). address the scientific questions raised by these observations, a multi-institutional program (the Airborne Surveillance Phenomenology Program; ASPP) was established at the Naval Research Laboratory, Washington, DC (The original plans are described in Valenzuela and Chen, 1983.). In July, 1982 as the initial field effort of ASPP, a pilot experiment was conducted southeast of Nantucket Island centered around the Asia Rip of Phelps Bank (40°50'N, 60°20'W). The experiment was to establish techniques for a comprehensive experiment in 1984, to learn about the oceanographic and meteorological environs of Asia Rip, and to obtain a data set for preliminary analysis.

The Nantucket Shoals area was chosen for the experiment because SAR imagery obtained in this area by SEASAT in 1978 (Beal, et al, 1981; p.22) showed a wealth of bathymetric signatures.

During the pilot experiment, meteorological, hydrographic, radar and wave buoy data were gathered. The data was confined to the tessera 40°30' to 41°10'N and 68°55' to 69°45'W. The data was obtained in two segments: 11 to 14 and 17 to 21 July, 1982. This report summarizes the meteorological conditions in the operational area during the experiment. The hydrographic situation is summarized in Kaiser (1983).

Manuscript approved July 20, 1983.

II. INSTRUMENTATION

Sensors were placed on the <u>USNS HAYES (T-AGOR 16)</u> to measure air temperature, air humidity, wind speed and direction, upper ocean temperature and salinity, ship roll, heading, latitude and longitude. The ship course and speed were calculated by the Loran-C navigation aid. Ship screw speed and pitch were also monitored.

The list of data channel labels and function are given in Table 2. 1. In some cases both primary and backup systems were deployed and these are indicated. For all other variables only one sensor was used. Fig. 2. 1, a side view of the <u>USNS HAYES</u>, shows the location of the various environmental sensors. The air temperature and dew point/humidity sensors were 10m above the dead water line (DWL). The wind sensors were 22.5m above the DWL and the ocean temperature and salinity sensors were 7m below the DWL. The ship roll sensor was on the main deck level mid-ship.

A. Description of instrumentation:

1. Air temperature and dew point/relative humidity

The primary air temperature/dew point system was a General Eastern 2100 MPS. The temperature sensor (TA1) is a platimum resistance thermometer (PRT). The dew point (TDP1) is measured directly by a PRT embedded in an optically controlled cooled mirror. Both sensors are mounted in an aspirated airway in a Dewer and external white radiation shield. The mirror is automatically "cleaned" once every 24 hours.

The backup air temperature (TA2) and relativity humidity (TDP2) sensor was a General Eastern Model 411 sensor and Model 450 signal processor. The temperature sensor is a PRT and the humidity sensor is of the sulfonated polystyrene ion exchange type with temperature compensation provided by a thermistor. Both sensors were mounted in a double-radiation-shielded aspirated horn (Climet 016-2). Both sensors were mounted on the starboard jackstaff 10m above the DWL (Fig $2.\ 1$).

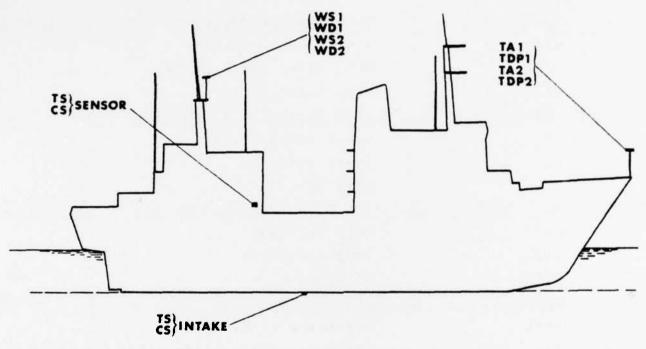


Fig. 2.1. Location of the meteorological sensors on the $\underline{\text{USNS}}$ $\underline{\text{HAYES}}$. Water for TS and CS is pumped at 300 cc/sec through insulated hose to the sensor located in the laboratory.

Table 2. 1 Data channels, labels and functions

Channel/Label	Function
TA1	Air temperature - primary sensor
TDP1	Air dew point - primary
TA2	Air temperature - backup
-TDP2	Relative humidity - backup
WS1	Wind speed - primary
WD1	Wind direction - primary
WS 2	Wind speed - backup
WD2	Wind direction - backup
TS	Ocean temperature
CS	Ocean salinity
ROLL	Ship roll
HD	Ship heading
LAT	Ship latitude
LONG	Ship longitude
SPEED	Ship speed
COURSE	Ship course
RPM1	Starboard screw speed
PII	Starboard screw blade pitch
RPM2	Port screw speed
P I 2	Port screw blade pitch

2. Wind speed and direction

The primary and backup wind speed and direction instruments were Model WS201 systems manufactured by Teledyne Geotech. Wind speed is measured in with a three cup anemometer which drives an optical chopper producing a frequency output proportional to the wind speed. Direction is determined with a vane driving a potentiometer. The direction signal spans 0 to 540 degrees to suppress the discontunity between 0 and 360 degrees. Since 0 and 360 degrees points towards the bow of the ship, transiting into a headwind would cause the wind vane to oscillate around 0° and an average of this wind direction would be about 180° without the overrange to 540°.

Both wind systems were mounted on 3m masts on the aft platform (Fig. 2. 1). The primary system was on the starboard side and the backup system on the port side. They were both 22.5m above the DWL. This location was a compromise between being well above all possible sources of interference from structural members of the ship and not being so far above the water so that the correction of the wind speed to 10m was large.

Since the wind sensors were mounted on a mast 22.5m above DWL, ship roll could induce sufficient relative motion to the sensors to cause erroneous readings; hence, the wind data was corrected for this using a roll sensor mounted midship. The roll sensor was a Robinson-Halpern Model 685B inclinometer.

3. Ocean temperature and salinity:

These quantities were measured with a Plessey Model 6600T thermosalinograph. Temperature (TS) is sensed with a PRT and conductivity with a thermistor-compensated induction conductivity cell. This data is then converted to salinity (CS) directly in the unit. The water was drawn in 7m below DWL and pumped to the sensor assembly on deck through insulated plastic tubing. The nominal flow rate was 300cc/sec. The water first passed through a filter before entering the thermosalinograph sensor housing.

4. Navigation

The primary navigation aid was two Northstar 7000 Loran-C systems. These have a nominal accuracy of 0.1 km in the Nantucket Shoals area due to the excellent Loran coverage there. The Loran-C time delays, calculated latitude (LAT) and longitude (LONG), and calculated ship course (CSE) and speed (SPEED) were provided by the Loran set. The course and speed were averaged over about 100 sec.

B. CALIBRATION

Most of the sensors were calibrated either in the laboratory or in situ. WS1 and WS2 were factory calibrated at the time of manufacture. The main factors which would affect the calibration are the bearings which are periodically checked for degradation. Intercomparison of WS1 and WS2 also verify they retain their accuracy. Four groups of calibrations were performed: 1) temperature (TA1, TDP1, TA2; laboratory), 2) wind direction (WD1, WD2; laboratory), 3) relative humidity (TDP2; laboratory), and 4) thermosalinograph (TS, CS; in situ).

1. Temperature calibration:

The temperature standard for the calibrations was a Dymec Model 2801A quartz thermometer with a least count of .0001°C. This quartz thermometer was calibrated against a standard quartz system over the range 0 to 40° C. Then the TA1, TDP1 and TA2 systems were calibrated over the range of 18 to 36° C and appropriate correction factors determined. Over the temperature range encountered in the experiment (<27°C) TA1, TA2 and TDP1 were all accurate to .05°C (Fig 2. 2).

2. Wind calibration

WS1 and WS2 were both factory calibrated to 0.5m/sec or 2% of air speed which ever is greater. WD1 and WD2 were laboratory calibrated. WD1 and WD2 errors are shown in Fig 2. 2. The maximum error is less than 2.5 degrees for both systems.



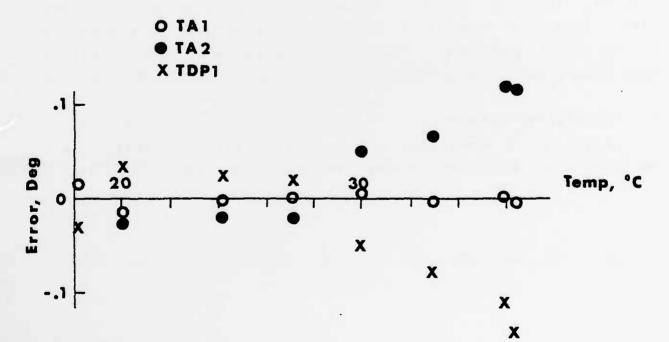


Fig. 2.2. Calibration data on WD1, WD2, TA1, TA2 and TDP1.

3. Relative Humidity Calibration

TDP2 was a relative humidity sensor. It was laboratory calibrated against saturated salt solutions which produce known relative humidities from 33% to 96.5%. The error was less than 2% over this range.

4. Thermosalinograph Calibration

The thermosalinograph measured temperature (TS) and salinity (CS) of 7m deep water. It was calibrated against a Neil Brown CTD (conductivity, temperature, depth) profiles in situ (Kaiser, 1983, describes the CTD instrument and accuracies), by selecting CTD casts with special characteristics. The calibration data could only be obtained when the CTD casts indicated homogenous water within 2 meters of the 7m depth, when the CTD down cast and up cast were the same; and when the thermosalinograph showed no temporal variation in the 7m water within 5 minutes of the cast. This left nine casts which could be used to determine the TS and CS calibrations. From these the root-mean-square errors are: TS, .065°C; CS, .031%.

5. Calibration Summary

Table 2. 2 summarizes the important data channels, their resolution and rms error or inaccurracy.

Table 2. 2. Summary of Calibrations and Errors

		rms error/
Channel	Resolution	innaccuracy
	6	
TA1	.001°C	.010°C
TDP1	.001	.034
TA2	.001	.031
TS	.001	.065
TDP2	.01%	2%
CS	.001%	0.31%
WS1	.05m/sec	Greater of .5m/sec
WS2	.05	or 2% of reading
WD1 .	1°	1.3°
· WD2	1°	1.3°
LAT	0.01'	0.1'
LONG	0.01'	0.1'
WS1 WS2 WD1 . WD2	.05m/sec .05 1° 1°	Greater of .5m/sec for 2% of reading 1.3° 1.3°

III. Database:

A. Description

The data was collected during two periods each of about Each channel was read once every two seconds. Several interruptions occurred due to the computer. Fia 3. 1 shows the operational periods of each sensor. The two second data (in original form: volts, frequency or digital) was logged directly onto digital magnetic tape. The data acquisition programs converted the raw data to digital form and passed the time of day and data to the processing system. Data processing proceeded according to guidelines established and maintained by the user. Every minute, data averages were output to disk files. Every 15 minutes, data averages, results of physical quantity calculations, and data quality assessments were output to both disk files and hard copy. A detailed discussion of the acquisition and processing system is given in Munch and Kaiser, 1983.

Some of the data channels (TA1, TDP1, TA2, WS1, WD1, TS and CS) were recorded on strip-chart recorders. For TS and CS, a portion of the strip-charts were read to fill data voids created by computer or instrument failures.

B. Contents of Files:

The contents of the 2 sec raw data tapes are the first 43 words of Table 3. 1. Tables 3. 1 and 3. 2 give the contents of the 1 minute averages file and the 15 minute averages file. The algorithms used to generate the variables and parameters are given in IV.

205				j						1									1				1						
204	-			+		-	+	1		-			+		-	+		-	1			 	+			 	+	1	
203	-			1			†			-			†			+		-	+			 -	†	+			+	+	
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193		1		1			1						-					 	† 			- 	†	1			†	1	
192			†				†	1						4		†			† 	1			†	1			†	1	
161							† 						† 																
90				-							-					-			-							-	-		
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	1 44	4	1001	TAS	7 6 6	1054	MSI	7	2	WS2	WOS	MON	S	ű	3	80	0	204	LAT	20	2 (3	SS	PDM		<u>.</u>	RPMZ	PIS	

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Fig. 3.1. Operational periods of all meteorological and ship parameter sensors. No line indicates no data.

Table 3. 1. Data Format for File SMIN1 (1-minute averages)

Words	Channel #	Channel	Description
0 1 2 3 4 6 8 10 12 14 16 18 22 24 25 33 32 44 46 48 50	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	TA1 TDP1 TA2 TDP2 WS1 WD1 WS2 WD2 TD CS TW ROLL Spare Spare HD RPM1 PI1 RPM2 PI2 PLOG LAT LONG SPEED COURSE	Hours Seconds 10's milliseconds Years Air Temperature 1 Dew Point 1 Air Temperature 2 Dew Point 2 Wind Speed 1, Starboard Wind Direction 1, Starboard Wind Speed 2, Port Wind Direction 2, Port Thermosalinograph Temperature Thermosalinograph Salinity Water Temperature Ship Roll For future use For future use Ship Heading RPM, Starboard Screw Pitch, Starboard Screw Pitch, Port Screw Pitch Log Latitude Longitude Ship Speed Ship Course

Table 3. 2. Data Format for File SMIN5 (15-minute averages)

Beginning Word

Word	Variable	Description	Units
0	I (1)	Time, hours from beginning of year	Hours
1	I (2)	Time, seconds from beginning of day	Seconds
2 3 4 5	I (3)	10's milliseconds from beginning of second	10 msec
3	I (4)	Year	Integer
4	LAT	Latitude	Deg.
5	RLAT	Latitude	Min.
7	LONG	Longitude	Deg.
8	RLONG	Longitude	Mn.
10	LRSPD	Ship speed calculated by Loran-C	Kts
12	PLOG	Ship speed from Pitot Log	Kts
14	HEAD	Ship heading	Deg.
16	CSE	Ship course calculated by Loran-C	Deg.
18	TA	Air temperature in physical units	°C ¯
20	TDP	Dew point temperature in physical units	°C
22	WS	Wind speed in physical units	m/sec
24	WD	Wind direction in physical units	Deg.
26	BLANK	For future use	
28	RLSPD	Ship roll speed	m/sec
30	RMSRL	RMS ship roll	Deg.
32	TW	Water temperature from towed thermistor	°C
34	TS	Water temperature from thermosalinograph	°C
36	SALIN	Water salinity from thermosalinograph	°/00 2
38	SIGT	Water sigma-T from TS and SALIN	gm/cm ³
40	TATW	TA-TW	C
42	TDPTW	TDP-TW	°C 2
44	H	Sensible water-to-air heat flux	watts/m2
46	Ε	Evaporative water-to-air heat flux	watts/m ²
48	TVATW	TVA-TVW	°C
50	TVA	Virtual air temperature	°C
52	TVW	Virtual air temperature when air is saturated at TW	°C
54	RH	Relative humidity	%
56	QWQA	QW-QA	gm/kgm
58	QW	Specific humidity of air	gm/kgm
60	QA	Specific humidity of air when saturated at TW	gm/kgm dyne/cm ²
62	TAU	Momentum stress on water	dyne/cm²
64	L	Monin-Obukhov length scale	m
66	ZO	Sea surface roughness height	cm
68	CD	Drag coefficient for momentum	
70	CH	Drag coefficient for sensible heat	
72	CE	 Drag coefficient for latent heat 	
74	USTAR	Friction velocity	cm/sec
76	TSTAR	TA	
78	QSTAR	QA	
80	PA	Atmospheric pressure	mbar
82	HW	Height of anemometer above DWL	meters
84	DT	Time interval between data scans	seconds

Table 3. 2 Data Format for File SMIN5 (15-min averages) (Cont)

Word	Variable	Description	Units
86	нт	Heights of air temperature & dew point sensors above DWL	meters
88	RBLN2	Blank	
90	VB	Current background variances - array	
130	RVAL	Current background variance thresholds - array	
170	FLG15	Total variance flags generated in last 15-minutes - array	
230	DAT15	15-minute raw data array	
278	STA	TA variance over 15-minutes	
280	STDP	TDP variance over 15-minutes	
282	SWS	WS variance over 15-minutes	
284	SWD	WD variance over 15-minutes	
286	SPLOG	PLOG variance over 15-minutes	
288	IBLK2	Blank	
289	OPTN1	System Execution Parameters algorithm selectors	5
293	RPTN2	System Execution Parameters calibrators	
301	STS	TS variance over 15-minutes	
303	IBLK5	Blank	

IV. Data Processing

A. Overview

The raw data was read once every two seconds. This data was averaged over 1 minute to eliminate variance due to ship motion (typically 6-12 sec. period). Then various quantities were calculated from these averages (correlations and variances) and these quantities were averaged over 15 minutes to minimize the variability of the lower atmospheric boundary layer. The appropriate boundary layer averaging interval is actually determined by the properties of the boundary layer existing during the measurement. The appropriate averaging period can vary from 100 to 2000 sec.

The wind data was corrected for ship roll since the wind sensors were on a 22.5m mast. Then the heading was combined with the wind direction. The wind velocity data was combined with the ship velocity data from the Loran-C to give true wind velocity at 22.5m. This wind velocity was then reduced to 10m elevation assuming a neutral atmosphere.

The dew point 2 (TDP2) sensor actually outputs relative humidity. This is converted to a vapor pressure and then to dew point.

The raw 2 sec data was wild point edited and then scanned for noise by comparing a running 60 sec variance to an average "background" variance. Any noisy records were flagged, and statistics on noise were compiled for each channel. The user selected the noise threshold for each channel and this could be changed during execution.

The one minute data, which represents atmospheric conditions averaged to remove ship motion contamination, is useful to examine variability on short time scales.

The 15 minute output is intended to provide the final characterization of the environment for all the scientists participating in the experiment.

B. Calculation of parameters

The parameters were caluclated from the one minute averages in Table 4. 1. An overbar denotes a one minute average

$$(=\frac{1}{30})^{30} \times \times_{i}^{5}$$
, where \times_{i}^{5} is a 2 second reading converted to

physical units).

From the one minute average variable values the various parameters are calculated and then averaged. The parameters and units are defined in Table 3. 2. The quantities which represent 15-minute averages are formed as

$$\overline{X} = \frac{1}{15} \sum_{j=1}^{15} f(x_j)$$

where \overline{x} is the one minute average. The functions f are defined in Table 4. 2; f would be the unity multiplier in the case of an unweighted average (e.g., TA, TDP); these are omitted from Table 4. 2. In Table 4. 2 the 15-minute average quantity is on the left and f (\overline{x}) on the right.

The parameterizations of CD, CE, CH, E and H are due to Smith (1980).

C. Special algorithms

Special algorithms were used to correct the wind speed and direction for ship course, speed, heading and roll; to calculate saturation vapor pressure from TDP; to calculate TDP from RH; to calculate σ_{T} .

1. Roll correction and TWIND

HW = height of wind sensor in m

DT = time interal between data scans in sec

ROLL = roll sensor in degrees - current scan

ROLLL = roll sensor in degrees - previous scan

WS - measured wind speed in m/sec

WD - measured wind direction in degrees

```
Roll velocity, VR:
    VR = (1.943 \cdot Hw \cdot (ROLL - ROLLL) / (DT \cdot 57.926)) \cdot 6.0
Across ship wind speed (WMX):
    WMX = WS \cdot sin (WD/57.296) - VR
Along ship wind speed (WMY):
    WMY = WS \cdot cos (WD/57.926)
Roll corrected wind speed (WS') & direction (WD'):
    WS' = [WMX^2 + WMY^2]^{1/2}
    WD' = arctan(WMY/WMX)
Ship motion correction to wind:
    SPEED = ship speed in kts
    COURSE = ship course in degrees
    HDG = ship heading in degrees
    DIR = wind direction in degrees (WD')
    SPD = wind speed in knots (WS')
    TWD = corrected wind direction in degrees
    TWS = corrected wind speed in knots
Subroutine TWIND*
ATMIND T=00003 IS ON CROODS! USING 00002 BLKS R=0000
000i
      FTN, L
5000
             SUBROUTINE TWIND(SPEED, COURSE, HDG, DIR, SPD, TWD, TWS)
             D=(HDG+DIR)*5.14159/180.0
0003
0004
             C=COURSE*3.14159/180.0
0005
             SVX=SPEED*COS(C)
0006
             SUY=SPEED*SIN(C)
             TWX=SPD*COS(D)-SVX
0007
8000
             TWY=SPD*SIN(D)-SVY
             TWS=SGRT(TWX*TWX+TWY*TWY)
0009
0010
             TWD=ATAN2(TWY, TWX) *180.0/3.14159
             IF(TWD.LT.0.0)TWD=TWD+360.0
Opii
0012
             RETURN
             ENU
0013
0014
             END'S
```

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2. Saturation vapor pressure from dew point or dew point from saturation vapor pressure

IPOLY = 1: DIN = Saturation vapor pressure in mbar
DOUT = Dew point in deg C

^{*}Dean Clamons, NRL Code 5003 developed this subroutine

IPOLY = 2: DIN = Dew point in deg C

DOUT = Saturation vapor pressure in mbar

The polynomials in SPOLY were obtained by fitting data from List
(1966).

ASPOLY T=00003 IS ON CR00033 USING 00005 BLKS R=0000

```
SUBROUTINE SPOLY(DIN, DOUT, IPOLY), 1982 Cruise E(t) and T(e)
0002
0003
     C
0004
           REAL*8 DIN
                                          Double precision input to subroutine
0005
           REAL*8 DOUT
                                           Double precision output from subroutine
0006
                                          Operational mode of subroutine
           INTEGER IPOLY
                                          Coefficients
0007
            REAL*8 D0, D1, D2, D3, D4, D5
0008
0009
                     Saturation vapor pressure from dew point
0010
     C
           IF (IPOLY.EQ.1) THEN
0011
0012
             D0=6.1183482DU
0013
             D1=0.42750748D0
0014
             D2=0.0169417D0
0015
             D3=0.0001191286D0
0016
             D4=0.00000618443D0
0017
              DGUT=D0+(D1*DIN)+(D2*D]N*DIN)+(D3*DIN**3)+(D4*DIN**4)
0018
            END IF
0019
0020
              T(e) Dew point from saturation vapor pressure
0021
0022
           IF (IPOLY.EQ.2) THEN
              D0=-12.304D0
0023
0024
             D1=2.42893D0
0025
              D2=-0.0626510D0
0026
             D3=0.000936792D0
0027
             D4=-0.00000689041D0
0028
             D5=1.93622D-8
0029
             0030
                (D5*DIN**5)
0031
                To correct for bad fit of T(e) polynomial to table
0032
0033
0034
             IF (DOUT.LT.16.0) THEN
0035
                DOUT=0.86+0.95*DOUT
0036
0037
                DOUT=DOUT+0.01*(DOUT-22.0)**2-0.31
0038
             END IF
0039
            END IF
0040
0041
     С
            RETURN
0042
0043
           END
```

3. To calculate dewpoint from relative humidity:

RH = relativity humidity in percent

R = mixing ratio over water in gm/gm

R = (RH/100) • (.62197 • E(TA)/(PA - E(TA))

E(TDP) = R • PA/(.62197 + R)

Use SPOLY with IPOLY = 1 to obtain E(TA) and E(TDP).

To calculate sea water sigma-T:

T = temperature in deg C

S = salinity in 0/00

 $\sigma_T = \text{sigma-T in gm/cm}^3$

 $\sigma_{T} = 29.42 - .270T - .0042(T-21)^{2} + (.7954 - .00162T) \cdot (S-34)$

This is a quadratic fit to the data in Stommel, 1965.

D. Background Variance Procedure

A running background variance check was implemented on 20 of the 24 data channels. In the check, a 30-point (60 sec) running background variance was divided by the long-term variance for the channel and the ratio is then compared to a threshold. If the threshold is exceeded, the channel is identified as noisy and a record of the violation is written to disk. The thresholds are initially set by the user and can be altered at any time by using the program SALTR to independently modify each of the data channel thresholds. (Munch and Kaiser, 1983). Total violations for every 15 minutes are recorded on disk and appear on the 15 minute data summary hardcopy. The current background variance and thresholds for each channel also appear on the printout.

The algorithm to perform the variance check was executed on each of the 20 channels of data. Thus, in actuality, during each 1 minute variance check, 20 variance ratios are calculated and compared with 20 independent threshold values and if necessary, the running background variance must be updated. For the first one hundred minutes the background variance is assumed to be a simple average of the variance. The algorithm to perform the variance check on only one channel is outlined below.

The running variance,

$$V_s = \frac{1}{30} \int_{i=1}^{30} (x_i - \overline{x})^2, x_i = 2$$
 -second data value

if N <100, the background variance

$$V_B = \frac{1}{N} \sum_{i=1}^{N} V_S$$

where N is the number of minutes (sets of 30 data points),

If
$$\frac{V_S}{V_B} > T$$
, $v = v + 1$,

where T is the channel threshold and v is the number of violations. For N > 100, $V_{\mbox{\footnotesize{B}}}$ is calculated as follows:

$$\frac{v_S}{v_B}$$
 < T, v_B = .99 v_B + .01 v_S ;

else $V_B = V_B$, v = v + 1.

Table 4. 1 One-minute Average Variables

Description	Air temperature, °C *Air dew point, °C	ED) *True wind direction, deg True wind speed at			Height of anemometer, m	273.15] $[1 + \frac{E(TDP)}{PA-E(TDP)}]/[1 + \frac{.62197}{PA} - \frac{E(TDP)}{E(TDP)}]$ -273.15 × 10^{-4} PA/TVA
Source	TAI or TAZ TDPI or RH(TDP2)	TWIND (WS, WD, HDG, CSE, SPEROLL COFFECTION AND HOG CSE SPEROLL COFFECTION AND HOG CSF SPEROLL CSF SPEROLL COFFECTION AND HOG CSF SPEROLL COFFETTION AND HO	WS 22.5/[1 = .076 ln(HW/10] TS SIGMA (TS, CS)*	\overline{E} (T)*	operator $(0.061 + 0.063 \overline{WS}) \times 10^{-3}$	[TA + 273.15] [1 + $\frac{E(TDP)}{PA-E(TDP)}$ 3.4838 x 10 ⁻⁴ PA/TVA
Variable	TA TDP	WD 822.5	WS TS SIGT	E(TA) E(TDP) E(TS)	HW CD	TVA

and roll correction ىيا TWIND, SIGMA, *The subroutines/functions RH, to wind are described in 4. C.

Average

Parameter RMS ROLL

 $(R0LL^2)^{1/2}$

100WS (CD)^{1/2}

 1.32×10^{-3}

RH

USTAR

E(TA)[PA-E(TA)]/E(TA)[PA-E(TDP)]

[TA+273.15] $[1 + \frac{E(TS)}{PA-E(TS)}]/[\frac{.62197E(TDP)}{-PA}]-273.15$

1046.4 [8.7 + .99 · (TS-TA) · WS]RHO

RHO[USTAR]²

H/[1046.4 RHO · (TS-TA) · WS]

1.515 x 109 · RHO · CE · WS[E(TS)-E(TDP)]/PA

.621 E(TS)/PA

3

OA

.621 E(TA)/PA

-.267 [TA + 273.15] · [USTAR] 3RHO/H

[USTAR]²/79,380

TVW

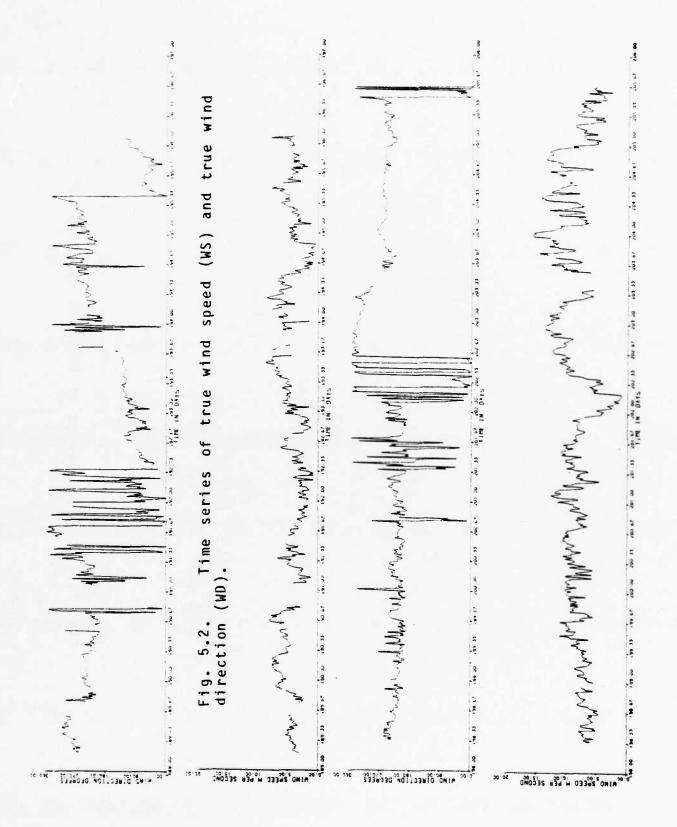
TAU

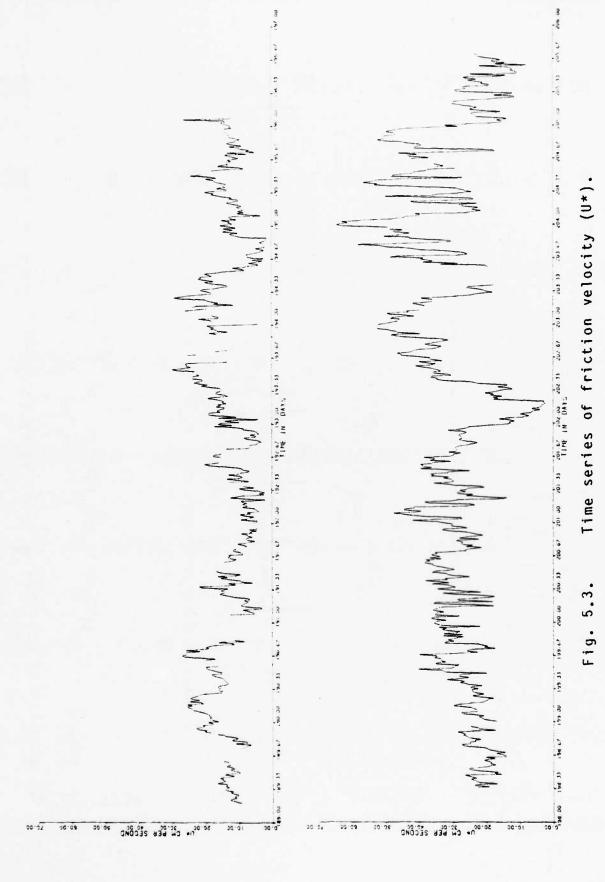
E

V. Time Series of Variables and Parameters

The basic data of importance to the phenomena (TA, TDP, TW, WS and WD) is displayed in Figs. 5.1 and 5.2 as time series for each half of the cruise. The important parameters (U*, TAU, TVA-TVW, H and E) are plotted in Figs. 5.3 to 5.6. WD and WS are true. The variables and parameters plotted are 15 minute averages. TVA-TVW is a measure of the stability of the lower atmosphere – the virtual temperature accounts for the effect of water vapor on the density of air. If TVA-TVW < 0 the lower atmosphere is convectively unstable. The calculations of U*, TAU, H and E are based on measurements over both stable and unstable conditions. The largest deviations of the calculated U*, TAU, H and E from the true conditions are likely to occur at very small U*, below about 10 cm/sec, when TVA-TVW < 0 .

(TA), dew point air temperature 7m depth (TS). TIME IN DATS Fig. 5.1. Time series of (TDP) and water temperature at TEMPERATURE DECREES CELSIUS 36.15 TEMPERATURE DECREES CELSIUS





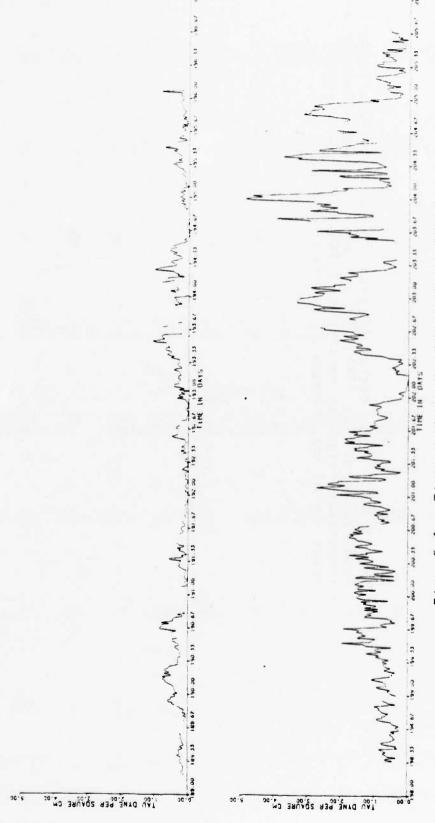
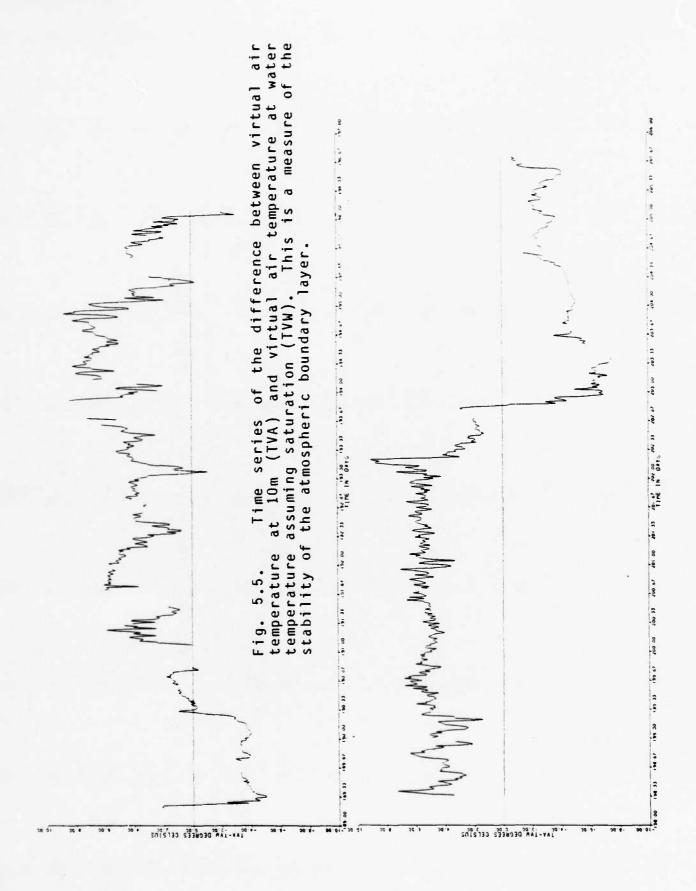
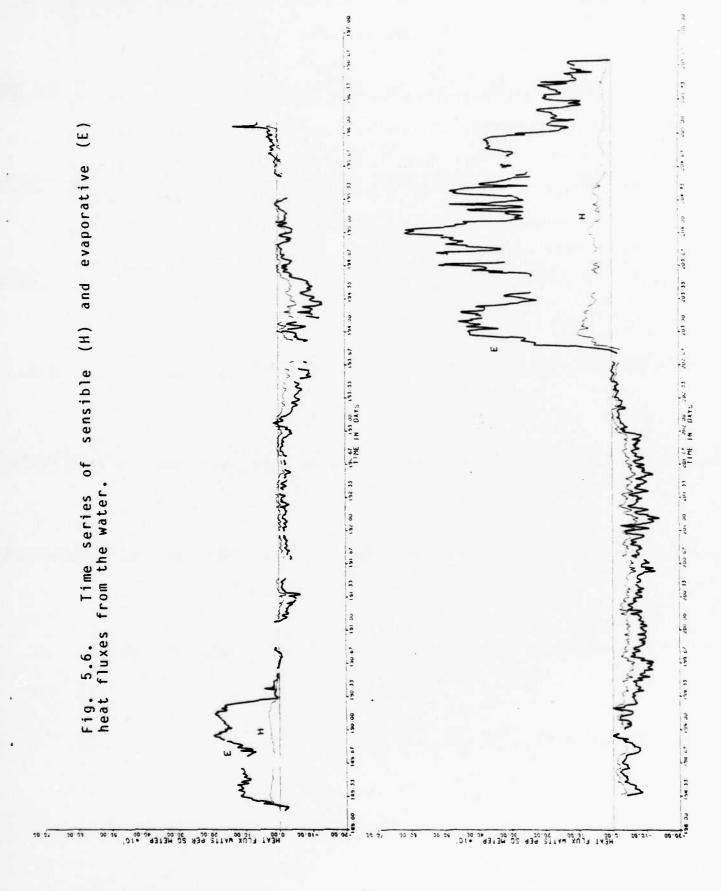


Fig. 5.4. Time series of wind stress (TAU).





ACKNOWLEDGEMENTS

This work was supported by the Naval Research Laboratory basic research program. Scientific and technical personnel who contributed to this work were W. Garrett, NRL Code 4350, senior scientist; Jack Ostrander, NRL Code 5004, navigator; Dean Clamons and Chuck McMath, NRL Code 5003, computer scientists and especially CAPT John W. Arens and the crew of the <u>USNS HAYES</u> who operated in extremely difficult conditions.

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 1, 1980). NRL Report 8659. Naval Research Laboratory,
 Washington, DC 20375 31p.

APPENDIX A: Physical Variable Summary

The basic physical variables which were measured during the experiment are tabulated in time here. The entries are 15-minute averages. The quantities are:

Quantity	Discription	Units
DTG,Z	Julian day/Greenwich time	day/hour,min.
TA	Air temperature	°C
TDP	Air dew point	°C
TS	Water temperature at -7m	°C
SAL	Water salinity at -7m	°/00
SIGT	$(\rho-1) \times 10^3$, ρ =water density	gm/cm^3
WS	True wind speed corrected for ship motion, heading and roll	m/sec
WD	True wind direction corrected for ship motion, heading and roll	deg
SHIPS	True ship speed	m/sec
CSE	True ship course	deg
HDG	Ship heading	deg
LAT	Latitude	deg, min
LONG	Longitude	deg,min

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19871129	50.75			34.56/		· :	7	¢ =	167	/07		Z :	\$ 3		? :
17071144	100			24.400		= 0 n (= 1	л с С 7	999		z :	20	4.50	3 :
1707137				24.506		- •	N 0 0	e :	5. P	547		2 :	40		3 :
17071214		٠		04.670		u i	100	4. V (5.5	.547		S	20	75. 75	3
178/1669		٠		4		ς . Σ	20.5	÷ (352	2.5		2 :	69		3
4451/171				35.400		e c		N C	200	55.9	38 41	4 : 5 :	9 .	-	2
4521/041	27.78	21.74				or i	661	 	.354	45.4		190 ×	7.0	7	3
170/1314				35, 3.58		9:3	100	ا أدا	554	35.5	-	× ×	7.		3
17071529					24.47	بارد د در	5.0.5	- :	4 :	/81			*	* **	+
170/1445	23.50		201.300			S .	Y 1	= 0 	69.	194		Z :	2.5		3 :
100/12/2					24.204	? \ 0 U	ת ה טנ	h i	/01	100		200	2 2		3 :
19071520						c -	000	n =	1 2	1 20		2 2	2 2		2 3 6 3
1911/1544					24 101		200	2	707	0		N 6.7	200		
19071559		22.08	22.122	35.244	24.386	0.1	66	. 4	2	96	30 58	20 X	20%	7	2 =
190/1614	23.54				24.363	7.8	202	s.	99	1.00		77 N	7.	26	3
194/1629			22.156		24.377	7.8	202	₽.	61	1.03		81 N	60	59.74	3
1911/1644			•		24.370	7.8	23.8	9.	56	146		N 06	69	29.7	3
6591/061					24.375	9·9	٠ (١) (١)	Ľ.	4	243	_	× 69	69	29.7	3 I
178/1/14			•		24.364	2.9	25.3	ن .	66	179	_	71 N	69	6.6.	3
1907/17091					24.401	9.0	137	₹ ·	127	539		SHS	69	59 5	3
1911/1744					64.369	6.1	23.0	4	120	225	-	2 09	6.3	59.4	3
45/1/071		74.55			24.541	5.5	2.54		1.38	506		22	69	29.1	3
19071014	50.00	20.33	100 A 20		04.546	= ? • L	क ह ए र	٠. د	147	328	95 95 95	Z :	4.5	~. ~. 	3:
100/10/1					200 40) c		· ·				2 :	20		3 :
19071859		24 25	•	3 -	24.674 24.08H	o 4		> 0	545	166		76 N	200	29.	3 -
19071914	22,22	21.54	22.260	35, 181	24.300	, m	7	1 147	1.54	0.5	: c.	2 4 4 2 2 2	2 5		2 3
198/1929		21.63		35,190	24.307	3.0	-	.	160	568	36	: z	2	-	; 3
190/1944	22.39	21.47	22.239	35.176	24,382	3.9	2.5	3.0	90	24	39 2.	7B N	69	6 65	3
191/0154		19.55	20.422	34.496	24.283	4.4	516	5.1	4	1.5	39 59.	N 26	69	40 . 0	2

106	15	SAI	SIGT	S	(17)	SHIPS	13.7	9311		Œ	
Cheg	degt:	166	u/rn*43	3.357W	bop	305/W	hap	hap	b.əp		Mins
7.21				1.9	245	5.	1.3	1.5	4	6.	\$
8. 95				eu	204	ه. چ	~	5.	=	4	1.3
1.78	17. H4B	33, 125	24.1179	4	950	5	1.5	5	-	^	100
1 54			24 665					<u> </u>	3 3	, (
1 4 4	15.363			ο -	1.75	= A	767	1 N	2 3	_ ~	7 11 13
7.89		32.0147		-	35	. 4	328	3.42	4.0		28
			24 448	0.	133	4 5	37.6	196	=	17	7
	15.099			3.3	0.00	÷	3.3	5	40	19	88
7.75	15.797	32, 166		0. M	573	ر م	3.4	.\$5	7	21.	2
٠	14.694			o c.	217	- ⊈.	38	35	40	53	46
5.75	14.352			2.7	243	5 1	.34	3.5	3.5	56	0.3
7.70	14.764			ت ور	B	ان -	34	35	46	3.	2
. E2				. e	<u>.</u>	3.4	è.	3.5	-	200	2 0
6.65	12, 421		24 175	ر ا	234	# · E	3.0	90	4 =	3	25
	•		24.237	-e :	239	4 6	(N)	£ :	4	3.5	90
4= 0	11.671		24 576		7			? ?	₹	ज *?	4
91.00		36.071	100 A 100 B	e •	- 1	æ . ∽ (<u>.</u>	3	9 :	36	S
10.00	44 6112	450 440	24 544 24 454	+ U		7. S	9.5	53	= =	ž :	90
7 7 7	111 606	140 15	24 465	0 <	0.00			2 0			
. T. S.	****	***	****	4		- 0.	1	= =	4	5	4.3
5.24	11.080	32.067	24.513	<u>۔</u> س	2.46	~	=	14.7 14.5 14.5	4	4.3	5
5.80	11,019	32.119	24.564	4.6	244	1.9	5.2	H	=	44	20
3.92	11.112	32.152	24.573	4.4	243	1 6	BE	1 3.1	40	44	0.2
5.02	11.053	32.153	24,584	6.3	267	9 -	53	509	40	44	1.3
4.86	11 826	32.127	24.569	6.0	575	1.6	9	20%	48	44	12
5.5B	11 076	36.1174		יים פיים	315	٠ . . ـ .	20 N	ص : د د	= ;	÷.	4
	11 025	30.411	24.013		247	5 n	9 2 3	c :	40	4.5	N C
	11, 466	32.161		7 F	626	. 4	953	200	- 4		000
-	11.869	32.450	24.581	*:	351	2	3.0	154	4		6.0
	11 463	32.424		3.4	£52		160	7.1	=	4.5	46
•	11.161			4.4	275	ત. આ	25	5.3	9	4.5	3.4
N 0	11.244	31.553	24. (182		= ?	ni s	7.7	22	= :	4	5.5
	11 086			ין די	0 1	0 E	100	0 2 3			
	11, 104	31.582			340		287	311	4		613
	11.057		24,413	3.3	2015	2.7	3.5	=	4	40	80
	11.049			4.9	2117		191	236	-	46	69
	10.946	32. 444	24.556	ιυ 51	ಣ		272	5.6	4	5.	_
	10.893			is:	38.0	2	13	124	=	3	Z
•	18.924	31.925	24.431	***	***	υ, 	= v	5.5	4	=	25
	18.31.5	•		***	**	ص - در	166	1.74	=	<u>.</u>	5
3.63	11.914	21.973	24.468	*	**	দ ^ব	247	400	= :	3 3	~ ~ :
	10.7.01			****	***	4	000	100	-	44	
V CV	100 19	26 1.00	2000 20	de de de de	4 4						

1 Civil

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19170289 19170224 19170239 19170254 19170389

19170424

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19171342

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19170609 19170639 19170639 19170718 19170255 19170255

1917825 19170810 19178825 1917885 1917885 1917895 1917895 1917895

19174955

19171055

91/11/40

9171825

19171155

91/1211 91/1225 91/1257 91/1241 91/1312 19171327

191/11411

1917/1125

MINUTE AVERAGES: DATA

2,910	C.	106	LS	SAL	STGT	56	MD	SHIPS	CSE	HDE		Œ			LONG		
	degC	degC	gbap	ppt	g/ca**3	M/50C	5.30	m/sec	deg	bap	bap	mins	15	bap	Σ	Mills.	
91/1412	14.28	14.85	****	*****	*****	****	***	4.7	724	218	40	46.60	z			9 i W	
191/1432	14.30	14.43	****	*****	*****	ις: (1)	33.4	1. (29.3	202	40	45.9	2				
91/1447	15.14	15.10	*****	*****	****	4.6	326	Ξ.	346	138	40	46 3.	z	69	-	_	
191/1502	15.25	14.98	****	****	****	4.2	3.36	1 .5	72	48	41	46.70	z				
191/1517	14.67	14.09	*****	****	****	о. М	313	3.1	70%	140	9	46.75	z				
19171532	15.04	14.50	****	***	****	9.6	320	- i	241	S S S	41	46.2	z				
91/1547	15.42	14.74	****	****	***	4	3.56	in i	10 to	23.5	2 3	45.5	z:	69			
2001/14	10.67	14.00	****	****	***	n :	100	n c	2.5	£ 6	= 1	2	2 ;		9.		
7191717	16.06	15 41	*****	****	****	4 7	343	/ e	2 Z	400	4 4	45.8	z	40	200	3 3	
01/1647		10 61	****	****	***	7 7	7.05		07.0	000	2 4	40 40	2 2				
61/1203	ė «	17.01	11 870	*****	*****	۲ را د د	240	, e	226	700	= =	40.40	2 2				
91/1717		15 18	11 (31		24 585	. 4	755	. 4	15.4	191	. 4	AG 7	2 2				
19171732	16.40	15.02	11,088	32, 135	24.563	4	352	3.7	200	(N)	4	47. 2	: z				
191/1747		15.02	11.053		24.561	3.7	1.1	4.4	105	44	40	46.66	z				
191/1802		14.87	11.167		24.559	***	***	4.6	20.1	245	40	47.5	2				
191/1817	16.39		11.091		24.578	3.0	20	4.5	105	112	40	49.30	z				
191/1832	16.72	15.31	11.005	32.166	24.588	2.7	1.4	6.	179	255	48	51.4.	z				
91/1847	16.33		11.170	32.154	24.563	# K	9	4.5	184	190	4 ((50.5	z				
191/1902	16.44		11.052	32,138	24.573	3.6	ın	4.4	175	170	11	48.39	2	69		M 21.	
191/1917	16.42	14.78	11.181	32,139	24.550	5.9	317	4.6	64	153	40	47.7.	z	69	74		
191/1932	16.48		11.102	32, 154		ທ ແ	36	4. ((264	192	9 ii	46.94	2	69		3 CA	
191/1947	16.50		11.117	32.186		4.9	56	4 .	7.8	139	41	50.9	Z ×	69			
191/2002		14.65	11.151	32.169	24.579	2.7	.34	4 0	234	200	9.6	51 47	2				
191/2017		15.03	11.111	32.154		2.0	Ξ	4.9	101	191	411	49.12	z				
191/2032	16.46	14.98	11.003	32.132		7.7	347	4.6	150	134	411	47.11	z				
191/2047		14.94	11.290	32.134	24.525	2.5	294	4 .	96	144	411	47.04	z	6.9	25.	M //	
191/2102	16.67	14.89	11.232	32.144		o.	5.	æ :e	299	255	7		z				
191/2117	16.51	14.76	11.246	32.181		9 1	رن 4	3.	37	29	7	49.37	z				
19172132	16.28	14.65	11.180	32.157	24.564		64	e	266	100	7	511.3	z				
91/2147	16.45	14.81	11.187	32.151	24.558	ou o	47	in i	181	404	4	46.1	z	69	4		
2022/14	10.51	14.56	11.121	20.131	64.994	. v	<u> </u>	= t	171	ת מ מ	= : -	2.5	z :	2	- ·		
191/2532	16.36	14.34	11.510	32.138	24 492	\ r - c	2 M	4 لا لأ ج	276	3,612	÷ ÷	4 to 4 to 7 to 7 to 7 to 7 to 7 to 7 to	22	69		3 3	
191/2247		14.85	11.203	32.177		1.6	261	3	137	1,1	4 (46.9	z	69	. 4.5		
191/2305	****	-	11.248	32.128		***	***	4.1	278	249	40	48.39	z	69	29.	3	
191/2320	16.56	15.30	11.158	32.154		***	***	5.5	173	171	4 ((46.45	z	69	24	3	
191/2335			11.096	32.140	24.566	***	***	4.7	174	150	46	44.(()	z	69		3	
91/5355	16.62		11.510	32.141	24.490	2.0	288	4.3	161	114	4	43.00	z	69	21.	3	
92/0010	16.62		11.461	32.151	24.507	ب بي	6.1	4.1	279	311	4(43.5	z	69	٠.	3 E	
92/0025	16.37	14.75	11.007	32.200	24.629	1.6	6.5	4	319	336	4 (44.5	z	69		3 + 1	
192/0040	15.96	14.37	11.280	32.157	24.546	1.7	63	4.5	325	313	4.0	46. 3.	z	69	. 5%	3	
95/0022	16.01	14.43	11.247	32.122	24.525	3.3	2	3.9	105	1.54	4(46.10	z	69	25.5	3 =	
92/0110		14.69	11.191	32.208	24.682	ري خ	~	4.6	171	177	4=	43.96	z	69	5.5	3	
92/0125	15.79	14.73	11.109	32.143	24.566	ر د د	63	4 ·	165	147	7	42.1	z	69	5	33 : Vg :	
17270140		14.75	11.558	36.157	24.531	= : N 1	121	N. I	997	116	-	41 4	2 :	66		3	
2510/27	16.02	14.62	11.385	32.147	24.53	= < -	0 2 0	4 .	263	294	4	41.6	z	69		3 :	
1767 0610		14.07	11.166	741.20	24.500	₹.	11	4.0	6.6	OHI	#	9.7.0	Z	÷	92	2	

15 MINUTE AVERAGES: DATA

DTG, 2	1A degC	1DP deaf	1S deqC	SAL ppt	S1GT 9/c###3	MS M/sec	erb drd	SHIPS	ESE deg	990 ded	ieg	1.61 8108	5	DNU 1	NAC m rus	
192/0225	15.38	14.73	11.182	32.207	24.602	×	7.7	4.7	195	254	40	44.54 6	9	26 4	1 4 5	-
192/0240	15.51	14.71	11.312	32, 171	24.550	2. 5.	13.3	4.1	26.0	37.6	40	45.94 6	69 7	12 6	~	3
19270255	15.65	14.66	11.186	32.196	24.593	٦.	5.63	4	150	103	40	44.97 N	69 }		3	-
192/0310	15.79	14.64	11.097	****	****	1.7	34.6		150	157	9	42.75 K	9	-	69	_
19270325	16.05	14.56	11.318	****	****	4.9	3.04	4 . 3	150	135	4	41.8D K	Č.		4 .).)	_
192/0340	16.02	14 42	11.253	****	****	e.	6.0	4	29.0	320	4 (1	41.75 6	50 P		1 13:1	~
19270355	15.65	14.33	11.260	****	****	n:	60	4 :	56.4	201	=	43.56 N	ن پ	-	69	-3
1927.4410	15.87	14.63	11.149	****	***	Q 1	11	ا س	161	ر ا ا	40	45.73	· ·	-		₹
5240/261	15.11	14.46	11.218	****	****	0 4 N 5	* 0 * 4 * 4	ə د د د	326	×1.5	9 9	47 92 4	٠. د د	700	Z :	٦.
193/0440		14.30	4.0 00%	*****	*****	- c	0.0	ن د د د	600		4 6	47.07	c 3		= ;	? -
19270510	14.70	14.16	11 667	*****	*****		. 0	÷ 4	2/1	7 7 5		47.00 6	2 4		3 3	2 7
192/0525		13.85	11.056	*****	****	; PC	0	 	277	244	4	46 66 N			· 5	
19970540	14.09	13.99	11.018	****	****		29.4	4 61	120	131	40		60		9	3
192/0555	14.59	14.48	18.974	*****	*****	9.8	1 ((4)	4 6	88	29	40	47.59 N	3	-	63	_
192/0610		11.38	11.135	****	****	4.3	1.13	5.0	95	64	3		9		7.3	3
19270625		14.82	11.326	****	****	3.6	18	υ. Ω	117	193	9 V		2		0 3 6	7
192/0640		14.22	11.228	****	****	3.2	130	3.1	563	53.4	40	50.13 1	69		=======================================	3
192/0655		14.48	11.247	****	****	э .	543	4 4	139	145	40		2		17.	3
192/0710		14.84	11.245	***	***	1.5	563	3.4	147	1.63	÷	47.63 6	٥ -		7.53	3
19270725		14.89	11.272	*****	*****	Ξ	317	3.8	175	181	40		9		111	_
195/0740		1.5.97	11.223	****	****	٠	24.3	€ :	178	1.1.1	90		ā.		- 2	3
192/0/55			11.169	****	****	9.1	2.	3.6	17.3	17.3	7	42.87	ت ب		7.7	-
0108/261	13, 45	13.36	11.078	52.174	24.596	3.0	.304	2	19.3	21.0	-	40.50	ري. د د		T :	<u>.</u>
27/10/25	13.76		11.110	32.167	24.586	4 :	45.	os t	172	143	4	411.03	٠ -		2	<u>.</u>
1927/0840	12.33		11.186	36.171	24.558	= ·	5.52		74	e .	= :	40.50	ç :		•	2 .
192/0010		13.77	11.027	120 178			n 3	4.	200	151	= 0	40 47 6	2 4		4.5	
192/0926		12.71	11.083	32, 178	24. 592	***	***	9 -	200	184		40 50 N	204	0 0	- 3	
192/0941	12.71		11.021	32.148	24.586	***	**	4	354	9	=		ت ب			3
192/0956		12.62	11.138	32.146	24.563	4.4	5.0	3 .	566	72	40		5		73 4	-
192/1011	12.59		11.150	32.147	24.561	53 57	46	٥.	192	194	4		ر د		E :	3
192/1026	12.72	12.62	11.104	32.144	24.568	හ : ල	32	- :	2.30	583	-	42.60 h	69		5.	٦.
19271056	4 2 4 5	13.47	11.685	30 124	74.04.	0 <	6.0	N +	745	15.	= =	45.75	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		9 3	· -
192/1111		12 35	11 891	691 68	065 66	· ·	45	2 0.	446	100	7				200	
192/1126		12.4B	11.095	32.202	24.615	3 FC	6.5		276	100	= =	46.46 6	200		1 4 6	
192/1141		12.95	11.091	32.170	24.597	4	2	= @	260	213	9	46.49	2		3	7
192/1156	14.20	14.05	11.109	32.171	24,588	3.5	6%	1 0	1-16	54	4	46.57 N	69	he 6	111	-
19271211	14.70	14.52	11.122	32, 185	24,596	53	Ξ	٠.	120	59	9.0	46.76	64 7		- 91-	3
19271226	14.61	14.40	*****	*****	****	æ. €.	83	£ . D	36	65	***	* ****	***		* **	
192/1241	14.67	14.39	11.116	32.1142	24,486	is N	7.5	ر ا ا	+ 19	65	4.0	47.67 6	69	-	411	7
19271256	14.81	14.31	11.134	31.973	24.429	. t	22	64 65	œ œ	ф Э	48	40.22 N	ic T	-	30.	_
192/1311	19.67	13.95	11.117	31.961	24. 423	י נים ו ביי	7.6	₹	ۍ د د	59	9	48.01	<u>.</u>		06	7
1927.1326	14.67	13.50	11.013	42 161	24.476	45 4 45 6	E 6	o^ o 4 ∪	89	in u	4 6	49.41 P	69	200		
19271356		13 50	10 768	BCE CE			u d		0	77		77 05		96		
192/1411		13.02	10.706	32.246	24.720	. 4	0.00	1.7	. r	99	9 0	51.26	: ·c		. Y.	, 7
									,	:	:			:		

15 MINUTE AVERAGES: DATA

2,510	14	1 DP	18	SAL	1918	145	940	SHIPS	CSE	HÖE	_	16.1			DNC	10	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	dege	deg);	dode	ppt	0/CM*#3	M/86-C	Christ	3.95/W	deg	deg	deg	Mins	9 1	bap	ε	MIDS	
1927/1426		12.58	111 688		24.714	2 %	92	K =	54	99	4	51.6	Z	69			
192/1441	(3.67	12.37	10.667		24.666	ev Les	2		S.	59	40	51.16	= \	69			_
192/1558		12.59	10.037		24.666	<u>.</u>	6.6	Œ.	192	179	411	11.4	z	69	11		
192/1613		12.65	18.907		24 646	5.6	 -	`.	19.5	Ē	=	0.10	2	69			_
192/1628		12.67	10.987	32.358	24 770	ic i	£ 0 .	ا بی	1117	180	4	7	Z:	69		74 E	
192/1643	٠	18.71	11.857		24.674	= 0 •	1 1 2	.^ :	186	131			z :	2			
19271658	•	12.76	10.967		24.702	4 4		s t			2 2	9 6	Z	2			
19271726		1.5.1.5	11.327		24.556		1.5.5	<i>r</i> .	E 1	T. C.	=	20.00	2 :	4.7	<u> </u>		
192/1741	14.39	***	11.027	32.268	24.678	***	**	جر ز	193	in it	2	S : 0	2 2	4	<u> </u>		
19271756		16.3.41	10.997		24.688	4 6	25.7	7/2	N - N		3 2	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	2 :	4			_
192/1811		13.94	1.1.097	32.146	24.572	e e	106	<u>د</u> د د	200	(S)	7	2 ·	Z :	200	<u>~</u>		
192/1826		13.78	11.077		•	ج ان	11.5	> :	3.5%		2 2	-	Z :	60	= :		_
192711141	10.00	13.76	10.777	52.183	24.621	.	- 1		1111	14.	4 11		2 :	2			
192/1856		1.5.46	1.8.967		24.668	Q .	117	N, I	26.5	266	2	49.96	<u>.</u>	6.7	2	1 %	_
192/1911		12.94	10.997	32.104	24.618	· ·	1114	ء ج <u>ي</u>	267	292	= :	•	2	69	_	=	
9251726		1.5.05	11.007		24.509			: د	56.5	5.54	4 2 2		= :	\$:	5		
192/1941		13.94	11.027		24.593	ry i	14	ا. د	6.6	124	=======================================	•	Z:	69	<u>.</u>		
176/1756		1.5. 1.5	11.0.57	32. 19H	٠	ر د د	N .		1.54	1 : C	4 18	49. HZ	= :	40	> :	`	
172/2011	•	13.77	11.517		24.550	= =	2	` :	1,5	16	40.	47.6	z:	9	= :	= '	
192/21/26	٠	13.78	11.417			2.7	67		1.31	286	-	40.4	2	4.7	=		
192/2041		13.26	11.217			= *	99		132	248	40	19 19	2	69	==	3	
192721156			11.057			4	6.5	Œ	1.5%	27.55	43		=	4.5	17	=	_
192/2111	•		11.137	32.250		3 .	5	٥.	158	116	40 7		2	69	1.7	3 = 3	_
19272126			11.157	32.228		ري د .	7.5	۲.	20	iji G	4		= ~	60	16		_
192/2141	*	14.51	11.237	32.203		1.5	3	**	123	7 7	4		¥	69	16		
192/2156			11.427	32,358	24.674	1	3.	-	ã.	Ē	=	17.66	2	69	-		_
192/2211		14.90	11.507	32.5911	•	3 6	14	+	123	1111	411		Z	69	14 (_	
192/2226			11.417	32.651	24.984	٠. د	65	.3	127	<u> </u>	=		7	69	14	5	
192/2241		15.63	11.977	****	****	3.1	E 6	1.1	159	112	4)	46.59	Z	69	13.		_
192/2256	15.47	15.53	11.557	****	***	æ	117	3.1	283	315	=	47. 11	z a	69	1.7		_
192/2311		14.87	11.047	32.028	24.468	3. G	116	65 i	018	318	43	47.9	Z :	69	16		_
19272326		14.50	11.117	31.948	24.415	o :		خ. <u>ء</u> (252	198	9 9	46	2 :	\$:	2		_
176/6341	14.76	14.65	11.18/	75 005	24.314	4 F	011		181	176	200	49.69	z:	% °	2:	3	
193/0811		14 25	11 167	*****	****	: = : u	000	, k	4.4		2 2		2 2	204	\ U	. 7	
(93/0826		14.01	11.337	****	****	. 4	119	· 10	103	6.4	=	49. B1	: 2	69	. M		_
19370041		13.96	11.327	****	****	4.7	1114	i iv	124	613	4		z	69	25	_	
193/01/56	14.30		11.607	****	****	4.6	114	4.9	88	05	100	50.01	7 7	69	٥		_
193/0111		14.04	13.207	****	****	£.5	ŝ	3.1	113	104	40	49.84	2	69	2		_
193711126	٠	14.10	14.057	****	****	بن س	66	. E	105	35	9	49.08	Z	60	ç	7	
19.370141		13.91	14.287	****	****	3.7	S	4 2	95	66	40	6.61	Z	69	2		
193/0156		13.63	-	****	****	4.0	69)	£	150	140	○	16.71	z S	63	ಎ		_
193/0211		13.21		****	****	6.0	96	4.9	IV.	<u>-</u>	48	51 1)	z	69	c.	 ?	
193/0226	12.89	12.75	•	***	***	€. 8	611	ر د	<u>:</u>	5	4.0	1.5 46	z	90	_		_
193/0241		12.55	11. 477	****	****	9 (110	-0 C	1.32	901	2 :	14.90	z:	6.9	-	9	_
175/8636		15.61		· 经转换经济	· · · · · · · · · · · · · · · · · · ·	 	16.3	4 i	2/2	27.11	= :	5.00	Z:	30		= :	_
193/0311	13.70	19.61	12.957	****	***	λ. r. 4. c.	111	10 ·	269	272	200	4	z:	69	٠. ر د د	عد . آي (
17.57 0560		15.75		***	***	2.6	52	٠. ب ١	MAZ	263	. #6	∃.	z ~	2.0	=		_

15 MINUTE AVERAGES: GALA

2,310	1A deqC	TOF	1S deq£	SAL	STG1	WS A/Set	QM (lea	SHIPS	TS.F.	39H	- 5	3102		1	Charles Paris	ے ۔
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19370341	14 09	14.86	11.887	*****	****	4.8	1.03	٦. 4	260	173	40 %	16 4	2		1.6 0	3
193/0356	1.3.78	13.74	10.947	32.243	24 673	4.7	1117	*:	7113	388	40 %	20 5	=		1 557	3
19.3/11411	13 76	13.78	10 947	32.278	24.743	r.	118		230	1.1.5	40 %	1. 3.5	z		4 40	3
19370426		14 17	10.917	32, 223	24 663	e e	127	1.6	17:	176	46	4.34	2			3
19.3.0441		14.29	10.937	32.200	24.640	۰ کتا - می	126	-	51.5	514	4 5	2 30	z		E	3
3-t0/261		4.75	77.77	32. 1116	21.6.51	9 :		~ :	176	127		4 45	=			3
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19578541		14. Cit.	18.957		15 4 TEN	- د د ب		z :		2	4 ≃ Հ.		z			3
ASSULATION 1			10.707	200		e .	: -		200		= :		= :		\$:	2 :
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19370711		10.50	111 917	32 848	24 550	טי	10.7		266				: :			? 3
193/0726		15 69	10 567	32.106	24 560	ى ئى:	1.51	- f.	111		. U		: =			3 2
193/8741		16 04	11.067	32.162	24.589	4	1.33		300	289	40 %		z			3
193/0756		15 52	11.117	32,154	24.573	را -	126	-	25.7	230	7 74		z			=
19370811		15.28	14.987	32.073	24.534	<u>د</u>	122	1.1	213	600	40 5		z			3
95907861	14.86	15.24	11 017	32, 020	24.494	٦. ٥	- N	e: +	21.4	248	9.0		z			73
19370841	15.02	15.37	11.007	32.065	24.524	5.1	1.25	1 1	242	27.0	40 4		z			3
19.370056	- 1	15.02	11.047	32,115	24.596	9 9	124	_	245	643	48 4		2			3
19374911		15.85	11.127	****	****	4 4	121	9.	117	6.1	40 4	11 134	Z	-		3
193/8926		15.39	11.187	****	米米米米米	1 9	122	2	1.116	6.1	10 4		.2			2
193,19941		15.16	11.187	****	****	0 3	156	9	111	6.1	40 4		z			3
193/10956		15 34	11.147	****	米泽安州济安	K.	135		110	09	4 11 4		2			3
19371011		15.51	11.177	****	****	14 3	1.3:	9	116	23	7 ₩		Z			3
19.5/1426		14.84	11.067	52.011	24. 47.3	6.5	1.30	~	111	3.3			2			:
19.5/1041		14.4.5	11.017	52.027	24.493	9 :	50	ci i	293	4		46.28	z			3
19371056	14.00	200	11.017	36.067	24.476	7.5	187	÷ (6/2	- 7	4 0 4		2:			Ŧ :
19371126	14.55	14.66	10.07/	32 (15.3	24 426	; ×	126	r. 5	11/11	ŋ -	3 4 4	46 32	2 2	7 0 3	19. 75	3 3
193/1141		14.39	11.067	32.000	24.463	2 9	124	: ``	277	0.0	4 8 4	8 37	z			3
193/1156	14 45	14.11	11.007	32.046	24 509	7.11	123	6	2115	15	400	B 46	2	_		3
19371211	13.56	13 66	10.967	32.491	24,552	****	***	1	265	9.9	4.8.4	8.63	z	-		3
193/1356		14 45	10.947	32.478	24,539	* · · · · · · · · · · · · · · · · · · ·	***	0.1	3.63	7	40 4		z			3
193/1241		14.90	10.927	32.047	24, 525	7.1	126	1.0	123	9.1	40 4	98 0	z			3
19.5/12'66		15.33	10.937	35. 040	24.517	6.4		- در	٠. در	2	96		2			2
173/1311		15.64	10.917	32.062	24.524	Z .	1.3.3	1 0	140	71	46 4	40.25	z	61 69		3
193/13:46		15.33	10.927	32. #50	24.527	=	129	Ξ,	202	25	411 4	1 44	2			3
193/1341		15.79	10.90%	32.143	24.572	7.4	129	-	308	11	4 11 4	0.10	z			3
19.471.556		15.77	10.927	32.170	24. 627		ر در	~	310	4	4 114	19 8	2	-		3
17.5/1411		15 77	10.897	32.224	24.668	7.7	155	-	50	41	4=4		z	69 3	=======================================	3
193/1126		15.70	10.907	52 250	24.606	0 .	4:3	~ ·	17	4.3	48	9 62	.2	64 69	4 - 1	3
175/1441	15.55	15.76	10 877	32.246	24.689	200	€. •	۳ . م	74 5 TO 0	4. G	4 6 6 7	50 45	z	بر م م	200	3 :
19771511		3.6.66	40 007	700 000	24 723			.	0.4.			20.7	2 :	4 0 0		1
1621/671	15 65	10.32	10.707	36.276	24. /de	4:	137	ں <u>ج</u>	15.5	151	# D 4	* · ·	zi		3.5	3 :
37.77 110.34		0.00	11.677	34.430	107.62	11	14.5	n	2.0	(F)	2	33	2	1 40	-	2

15 MINUTE AUFRAGES: DATA

2,310	3	100	1.5	SAL	STEF	23	02	SHIPS	F.5E	HING		2			_	FING	9	
	deac	degC	deage	ppt	(1/c m* #3	n'sec.	bap	M/Sec	ded	deg	der	ε	MIRS	1	ged	Ξ	MIDS.	į
93/1647	18.00	15.80	11,257			0 /	155		328	100	48	35	89	z	69		09	3
19371732	85 HT	15 67	11.157			5	27.5	9	1.0.3	1.42	40	46	B/	z	63		1.	3
193/1747	18.55	15 35	****	-	*	4.7	190	4	69	143	9.6	20	8.3	z	(1)	1.7	= 6	3
93/1822	18.96	15.51	11 467			<u>-</u>	286	8.	2	153	3	28	11	Z.	44		19	3
193/1851		15 30	11.487	(0)		ey i	5.03	<u>.</u>	4.7	163	-	2.	5.3	z	66		5.	3
19371951		15.91	11.597			0 :	/= :	s.	S .	æ !	= :	2	= :	= :	60		*	3 ;
19372041	20.00	16.75	11.227			= 0 in <	20 v	- 1	161	21.5	4 4		6.3	z	200		ر ا ا	3 :
93/6/8/		10.04	11.477			c <	200	- 0	177				9 5	2 2	200			3 :
02/01/0		10.77	11.14/			σ. = Ω. ¬	0 0	\ .	000	0 0	= =	/4/	2 2	z	0			3 -
02/2243		17.03	4.0 45.0			= 3	17.5		140	577	= 0		2 9	2 2	200			3 :
61/2220		27 40	12 140				- U	7 U	200	† «	= =		60	2 3	0 0		1	3 =
93/2243	18.53	17 53	14 250			. u	288	יט ני	2 8	i i	. 4	7.7	200	2 2	0 0			3 7
Bacc/161		17 KB	14 982	•		: U	200	4	2	2 0		40	7	: 2			0	: 3
93/2313	18.63	17.87	14.429			1 5	1.7	0.	105	± 20	7	44	64	: =	66	4		. 3
19372328		18.07	14.560			<u>د</u> د	173	(C)	84	H	*	44	23	z	20.0		19	. 3
193/2343	18.92	18.31	15.488			6.3	348	3.9	56	0.6	48	4	5.6	z	#		13	3
193/2358		18.6A	15.298			3 6	25.1	9.	163	1.67	40	4	54	2	99		3	3
194/0013		19.85	16.243			5	2.42	9.5	194	284	7	41	7.3	z	89	4	4.5	3
194/0035		19.25	17 447			5.9	222	-9	556	254	-6	39	96	¥	6.9		Ξ	3
194/0050	19.61	19.39	15.977			£.	193	5.	278	278	4	39.	83	z	69		9.3	3
50107461	18.99	18.82	14.345			ر ا ا	273	3.7	266	3.5	40	.89	#2 12	z	69		-	=
194/0120		19.01	14.658			6.8	522	5.5	166	145	48	36	04 04	z	69		30	3
194/0135	19.51	19.37	16.746			64 Un	193	ري دي	182	163	46	36.	6B	z	63		2.9	2
194/0150	19.38	19.26	17.643			က (ကို (510	1.7	280	592	40	35	0,	z.	ر د		2	3
194/0205	19.17	19.09	16.684			5.7	.50 1	ص ن	567	5/2	10		96	2	20		 I	3
194/0220	19.21	19.15	15.866			ce :	244	ا د د	271	276	~		96	z	69		e 1	3
2520746	1H. 52	18.29	14.7HB			e :	191	4.7	3	7.3	~	37	<u></u>	z	\$		Œ,	3
94/0323	17.72	17.72	11.609			2.8	226	տ : c. :	237	ณ (ณ (ณ (9	3.0	26	z:	60	14	0	3
547.03.58	17.38	17.45	11.360			× .	6	ه برد د نه	KZH	D .	4		=	z:	6.7		-	3 ;
94/0416	16.73	16.84	11.634			- r	0 0 0 0 0 0	= 5 N N	⊋ 0 12 0 13 0	513	2 0	2 0	> 1	2 2	× 0		7 0	3 -
94/0431	16.72	16 83	11 000			9 0	1 10 0		2000	400	- 4		0 0	2 7	100			3 =
194/0446		17.24	11.195	32.269	24.648	0 (O) (O)	23.3	. 0.	1 0.1 2 0.1 2 0.1	242	4	. 6	E .	2 2	0.00		: =	3 3
194/0501	17.93	18.02	11,182			5.7	248	8	262	309	4	39	86	z	69	5		3
194/0516		1H. 39	11.203			ស ភ	27.5	63	331	345	9		136	2	69		.54	3
194/0531		18.19	11.174			ۍ	215	61 64	345	345	4		89	z	63	.98	æ	3
94/0246	17:30	17.32	11.169			6.1	212	त्यः स्य	348	345	48	45	86	z	69		I	3
194/0601		15.93	11.169			6.3	221	٠. ده	351	344	4	44.	98	z	50	22	37	=
94/0616		16.65	11.186			# #	539	1.7	346	328	₩	44	63	z	69	27	61	3
174/0631		17.30	11.201			9.6	244	1.6	344	356	40	45	7.0	z	69	22	=	3
194/0647		17.38	11.220			=	0.0	9.1	345	356	=	46.	<u>~</u>	z	69	. HE	2	3
20/0/64		18.11	11.227			2.5	244	٠. د د	348	21.5	4	4.	3	z	69	=	ক ক	3
/1/0/6/	Y 0 0 0	18.47	11.050			9 1	2.47	1.3	328	# A !!	2	47	=	3 .	20		3	3
174/0/32	•	18.14	11.655			I C	2.5 2.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3	o-, :	558	29.5	₹ :	5 5	2	z:	69	0. 0 0. 1	4	3
2000/60	27.72	17.04	11.649) (1)	127	> :	.58		= :	4	4	2 :	2	À		3
200770	20.71	17.57	11.668	32.134		rų i	2.38	<u>٠</u> !	368	E (45	48	14	z	69	9	4	3
Ē	17.61	17.76	11.224	54.125		6.7	7.47	₽.	276	27.4	4	ξ.	3.	z	20	3.1	1	3

VI Va
AUF,RAFIES
MINCIE
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D(6, Z	TA	TOP	TS	SAL. PPt	SIGT q/cm*#3	W/Sec	0 to 10	50)PS	7.5.F.	HD);	bap	3 2	5.T mins	ર્સ	i ,	HIPE MILL	2.
-	!				1 1 1 1 1 1 1		20 May 100 May 100 May	-	*** mas vos 1441 des -		1	:	:	:	÷	:	2
19470832	17.92	17.81	11.250	32.117	24.520	6.5	247		565	279	40	49 (11 11	£			3
194/0647	17.66	17.55	11.287	32.099	24.459	t J	206	^	284	628	9		× 2	£		-	Z
194/0902	17.48	17.37	11.330	31.7511	24,219	<u>۔</u> بی	215	Ξ	278	500	4		N 0:	3		16	3
194/11917		17.36	11,349	31.212	23.790	*	₩. Y.	4	27.3	613	=		X	\$?
19970932		17.52	11.516	31.150	23 719	4 5	240	٤	27.1	20.3	40		9,	સ		=	<u> </u>
19478947		17.07	11.390	31.151	23.744	er.	243	9.	2:14.5	300	40		200	9			3
1907/1002		17.49	11.361	34 200	23 793	0.0	5 14	^	275	301	40		36 H	•		_	3
194/1017		17.59	11.302	31.244	23.812	6.5	5.20	<u>``</u>	27.3	306	3		÷ :	·\$			3
194/1032	1	17.47	11.307	31.272	23 1138	2.6	0 5 6	Y	313	16.3	40	49.	Z	\$		Ė	3
194711947	17.43	12.31	11.412	31.277	23, 837	6.3	246	9.	307	<u>2</u>	9		2 2 2	Ç		-	3
194/1102	~	17.44	11.459	31,234	23.795	(1.9	243	4	279	366	4		ا ا	Ğ.		0.5	3
194/1117		16.99	11,402	31,229	23.767	6 0	65%	۲.	200	327	4		2 =	Ţ			?
194/1132	1	17.10	11.503	31.106	23.680	6.7	265	4	200	333	40		7 TS	÷			3
17471147			11.499		23 652	න ග	272	بر	186	170	40		2 9	S			.?
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174/1217			11.500		23.902	6 .5	5/2	in.	0.1 0.1 0.1	3.87	40		2	3			3
194/1232			11.429		24.403	5	567	î.	23)	376	÷		2 9	Ü			3
194/1247			11.420			4.9	10 c.	9.	247	800	40		=	<u>.</u>			.3
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194/1332			11.561		24.346	es :	233	-	4	6.0	40		z :	ર			3
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194/1702			11.408		24,450	5.7	261	3.1	F,3	56	=		50	4 0			3
194/1717			11.377		24 509	ev ev	540	2.6	7.5	86	÷		× 5	·£			2
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19471002			11.390		24.528	> .	295	Œ.	129	190	0.7		2 0 2	હ		-	3
194/1817			11.356		24.538	1.3	200	1.3	190	201	40		7	٤		3	=
19471832			11,308		24,533	#. #.	568	4.9	190	499	9		36 ((હ			3
174/1847			11.257		24,519	©	267		36	139	6		3	4.			2
194/1902			11.291		24.512	≆.	500		43	179	40		Z	Ç		4	3
17471917	Ξ (11.319	32.118	24.508	<u>9-</u>	22.	3	J. G	16.4	40		S .	2		6.4	3
174/1736	17.61		31.315	32.119	24,509	6.	(C) (3 .0	22	157	4	45	ក្ ខេះ	· 2		ĵ.	3
404/2002	2		11.307	36, 166	21.0 4.0	0 '	100	> 1	4	150	9	7	2	φ.		- :	3 :
19475006	46. 40		11.505	37.176	24,516	~? 	236	- r	S :	200	4	45	Z :	\$	15.	\$:	3
174/6017			11,6/0	36,360	24.517	P.		N .	217	922	=	1	=	e	5	2	2

15 MINULE AUTRICES: DATA

016,2	<u><</u>	101	5-1	SAI.	5167	50	(IN)	SHIPS	PAE	110G	107		_	(DMC	
1	degC	degC	gbap	Ppt	0/c.m*#3	N. Co.	give)	345/W	dec	ded	deg mins	5	Бар	SOLM	2. 1
9472032	18.81	15.20	11.877				295	8. 4	225	230	40 47.50	z			3
194/2047	19.54	15.81	14.115		٠.	÷Ĉ	317	4	4 2.5	686	46 45 99	z			3
94/2102		15.83	14.060		٠.	٠ <u>.</u>	347	4 5	2.24	23.30	40 44 43	74 5			3
4		15.90	14.629		٠.	o, ~:	283	4 2	1.4	19	411 44. 47	z			3
194/2132		15.92	14.413		Ξ.	3.6	215	4	3.	5.63	40 46 27	Ξ			3
194/2147		18.90	12.820			7	517	6.	3.7	4	411 47.98	=			2
		15.53	11.719			e e	200	5.5	143	194	40 49.44	z			3
		91 51	11.872			٠. ا	5	9.	(85)	5.60	40 50.00	=			=
194/2232	19.45	15.43	11.773			4 . F	23.8	1.6	1411	243	40 49 77	Z			3
-		15.66	12.622		- 1	\$. \$	234	હ	(13.3	193	48 47 65	2			3
194/2302	•	15.70	14.362		Ξ.	3.9	240	3.4	140	194	40 45 44	z			3
۲.		15.54	15.099			2	N. N.	4. 4	179	1161	48 43 95	z			3
194/2332	٠.	15.32	14.37B			3 2	27.5	r. Cr	1113	106	40 41.39	Z			3
194/2347		15.26	12.553			4	231	6. 6.	18.	()()	48 39.76	3			3
2000/561	17.86	15.31	11.739		٠.	λ. -	2.33	7.1 4.	110	1110	40 37.49	Z			3
195/0017	•	15.60	11.520			÷ .	۲. ک	. t	191	235	40 .55 35	z			.?
		15.73	11.274			9.0	27.3	7.5	158	1411	411 .54.69	2			3
195/8847		15.61	11.365			4.4	233	7	3 8 6	9))	40 33 03	2			.7
2010/561		15.85	12.109	٠.	٠,	4.2	234	4.9	116	113	40 35 90	I			3
195/0112	•	15.84	13.725			= ७	247	3.	1.45	147		2			3
195/0132	17.36	15.80	14.318		-	3.6	249	3.3	656	7.3	40 32.28	2			3
195/0147		15.78	15,393			4.3	247	4.6	63	63	33.28	z			3
195/0202	17.02	15.69	13.736	٠.		T T	246	4.5	22	6.3	411 34.37	Z			_
155/11217		15.39	12.405		٠.	4.6	652	ر ا	175	1614	98.59	z			
19570232		15.24	14.062	٠.	٠.	C4.	303	r. ca	565	277	٠	z	-		
195/0248	15. HO	14.78	12,279			3. 3.	2411	4.4	209	203		2			
195/0303	15.57	14.75	11.874			3 6	27.0	C.	316	5/		Z	_		_
(95/0318		14.58	11.739			o. N	7.53	4 .s	5/	=		z			
95/0333		14.70	11.568		٠.	53	240	3	5.5			Z	_		_
195,10348		14.39	11.512	•	٠.	.5. 0	25.7	, ,	249	133		2			_
95/0403	14.95	14.36	11.485		-	(1) (1)	75.2	٠.	269	2.	40 39.51	z			_
0150/0410	10.16	14.00	11.367			ا ت ن	200	י ד	# N	S 2		z :			
95/044B		44.03	11.63/			e 0 7	197	- 0	273	S F		2 3	-		
195/0503		13.91	11.175			· **	252	5.7	16	1 00	40 42 00	Z			3
0150/551		12.95	11.207			-	192	. r.	46	7.3	411 4.3 11.1	2			
195/0533	15.91	12.39	11.224		٠.	4 5	261	5.	33	96	411 43 29	z	_		_
1957115411		11.73	11.231		٠.		586	2	5.6	96	48 43.27	z			
3	12.65	12.12			٠.	3.4	251	C.	1.6	5.6	40 43.24	z	-		_
*	•	12.14	•		٠.	54	520	ત્ય ભ	5	5.5	48 38 36	=			
195/0633		12.19		٠.		4	264	2.3	06	66	40 43.35	z			_
195711648		(2.29				4	26.3	6. 4	64	1.1	48 43.43	2			
195,707.03		13.45	*	Ξ.	᠆.	= :s:	575	4.	2	14	411 43.56	z			
195/0718		13.64		٠.	٠.	ល	569	3.1	31315	5.7	40 44.70	z			
195/0/33	13,84	13.40	12.942	32.174	24.239	in i	263	44 4 44 4	347	45. 45.	40 46.20	z	69	15.77	3
26/0/0/1		10,00				ר ה ה	000	T :	100	900	46 47 40	2 :			3 :
95/0003		13.41	11.748			n :	200	= C	243	334	40 46 36	z	6%	= = =	3 :
17 1/ 10/12/14	٠	14.41	131.11			7.1	÷ / :	\		5.34	41 47.10	2	0.4		3

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13.77 13.73 14.4444 14.4444 14.4444 14.7 15.7 14.6 15.7 14.6 15.8 14.6 14.6 14.4 14.	2,910	400	1DP deqC	15 degC	SAL	STET g/cn*#3	WS m/sec	ded	SHIPS	CSE	бар	ged (LAT mins) T	LCOME	iwG mins
14 15 15 15 15 15 15 15	133		13.77	*****	安安安安安安	******	40	970	4-	346	334	40 4	9.96 H	69	17.6	32
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15.32 112.35 11.172 32.415 24.549 4.6 70 5.83 54.40 50.01 69.19 15.37 11.36 11.184 32.216 24.513 3.0 66 1.3 69.1 40.4 39.0 N 69.19 15.11 16.4 11.4 32.216 32.216 24.549 5.3 7.0 12.0 16.6 11.20 24.549 5.3 7.0 12.0 16.6 11.20 24.549 5.3 7.0 12.0 16.6 14.0 26.0 19.	320			*****	- 4	*****	6.3	7.0	.3	318	623		-	69		_
15.17 11.36 11.169 32.219 24.513 3.0 61 1.3 124	333			11.172	32,135	24.549	4.6	1/1	S.	5.85	24			64		
15.16.3 11.84 32.143 24.549 5.3 7.4 154 154 11.449 35.140 16.7 14.49 35.14 16.7 14.49 35.14 16.7 14.49 35.14 17.7 14.69 19.7 18.69 19.7 18.69 19.7 18.69 19.7 18.69 19.7 18.69 19.7 18.69 19.7 18.69 19.7 18.69 19.7 18.69 19.7 19.7 18.69 19.7 19.7 18.69 19.7	350		11.36	11.169	32,210		3.0	19	1.3	121	67			69		
15.31 10.65 11.242 32.150 24.549 5.3 79 1.4 210 166 410 401.77 N . 69 19 15.51 10.65 11.242 32.172 24.548 4.9 1.5 21 6.5 410 401.27 N . 69 19 15.50 10.03 11.202 32.373 24.724 4.3 74 1.5 25 1.0 2581 11.7 40 49.748 N . 69 20 15.63 10.03 11.202 32.373 24.724 4.5 73 1 . 65 20 40 40 40 40 40 40 40 40 40 40 40 40 40	405	15.13	18.64	11.181	32.143		3.4	6.13	1.7	4 2 6	124			69		
15.50 10.81 (11.22) 32.372 24.548 4 9 74 1.5 216 163 40 40 10 12 H 69 19 15 16 10 10.81 (11.22) 32.372 24.548 4 9 74 1.5 29 3 10 40 40 12 H 69 19 15 60 10 81 (11.22) 32.382 32.3 24 224 4 1 3 10 253 10 7 40 47 48 H 69 20 15 64 10 67 (11.24) 32.384 24.728 4 .5 71 18 252 24 24 40 47 48 H 69 20 15 64 10 57 (11.24) 32.384 24.747 3 .9 72 1.1 294 21 40 47 43 H 69 20 15 72 10 64 11.216 32.359 24.747 3 .9 72 1.1 294 21 24 40 47 43 H 69 20 15 79 10 64 11.216 32.359 24.747 3 .9 72 1.1 294 21 24 40 47 43 H 69 20 15 79 10 64 11.216 32.359 24.747 3 .9 72 1.1 294 21 24 40 47 43 H 69 20 15 79 10 64 11.216 32.359 24.699 3 .4 62 1.5 283 24 40 47 24 H 69 20 15 79 10 64 11.216 32.359 24.699 3 .4 62 1.5 283 24 64 10 20 11.296 32.352 24.699 3 .4 62 10 24 216 24 27 24 10 20 11.296 32.322 24.699 3 .4 62 10 24 27 24 10 40 27 24 H 69 20 11.296 21 11.296 32.322 24.699 4 .5 60 10 20 11.294 32.342 24.699 4 .5 60 10 20 11.294 32.342 24.699 4 .5 60 10 20 11.294 32.342 24.699 1 .5 60 10 2 11.294 32.342 24.699 4 .5 60 10 20 11.294 32.342 24.699 4 .5 60 10 20 11.294 32.342 24.699 4 .5 60 10 20 11.294 32.342 24.699 1 .5 60 10 2 11.294 32.342 24.699 1 .5 60 10 2 11.294 32.342 24.699 1 .5 60 10 2 11.294 32.342 24.699 1 .5 60 10 2 11.294 32.342 24.699 1 .5 60 10 2 11.294 32.342 24.699 1 .5 60 10 2 11.294 32.342 24.699 1 .5 60 10 2 11.294 32.342 24.899 3 .5 60 10 2 11.294 32.342 24.899 3 .5 60 10 2 11.294 32.342 24.999 1 .5 60 10 2 11.294 32.342 24.999 1 .5 60 10 2 11.294 32.342 24.999 1 .5 60 10 2 11.294 32.342 24.999 1 .5 60 10 2 11.294 32.342 24.999 1 .5 60 10 2 11.294 32.342 24.999 1 .5 60 10 2 10 2 10 2 10 2 10 2 10 2 10 2 1	42.0	15.31	10.65	11.232	32.150	24.549	بر در	78	-	532	166		3.77 N	69		3 6
15.63 10.67 11.3 7.54 9.2 4.1.3 7.54 9.2 4.1.3 7.54 9.2 4.1.3 7.54 9.2 4.1.3 7.54 9.2 4.1.3 7.54 9.2 4.1.3 7.54 9.2 4.1.3 7.54 9.2 4.1.3 7.54 9.2 4.1.4 9.2 4.1.4 9.2 4.1.4 9.2 4.1.4 4.2 9.2 4.1.4 4.2 9.2 4.2 9.2	435		30.70	11.217		24.568	4 .	14	ر ا	916	163			9		= :
15.63 10.67 11.244 32.384 24.728 4.5 71 8 26.2 90 40.47.93 N 69.21.9 15.63 10.67 11.244 32.384 24.728 4.5 73 72 27.6 40.4 70.73 N 69.2 72.7 72 72 72 40.4 72.7 72 72 72 74 73 72 72 72 74 74 72 72 72 74	1 2 D		10.61	11.300		24 628	4 . A	6 N	~ ~	4 57 6 4 7 7 6	N 2 4			400		2. 44
##### ##### # #### # # #### # # # # #	520	15.63	10.67	1.244		24.728	4	2.	.	10	06			5.5		6.5.13
15. 43 10. 57 11. 211 32. 357 24. 745 4.4 69 .9 329 22 40 47 63 N 69 22 15.5 3 10. 64 11. 216 32. 359 24. 717 3.9 72 1.1 294 21 40 49. 23 N 69 22 15.7 10. 64 11. 216 32. 339 24. 680 3.4 62 1.5 283 203 40 48. 49 13 N 69 23 N 69 23 N 69 24 15. 7 10. 66 11. 216 32. 339 24. 680 4.1 50 24 682 4.7 10. 66 11. 216 32. 332 24. 680 4.7 40 2.4 24 682 4.7 40 49. 22 16. 640 47. 24 N 69 24 14. 64 10. 15 11. 246 32. 342 24. 687 4.7 40 2.8 N 69 24 14. 64 10. 15 11. 246 32. 342 24. 687 4.7 40 2.8 N 69 24 14. 64 10. 07 11. 244 32. 24. 689 4.5 40 4.9 83 67 40 49. 55 N 69 19 15. 07 11. 241 32. 236 24. 690 4.5 40 4.9 83 67 40 49. 93 N 69 19 15. 07 10. 62 11. 149 32. 235 24. 690 4.5 40 4.0 89 30 N 69 19 15. 64 10. 94 12. 667 33. 198 24. 760 2.0 6.9 4.0 69 10. 94 12. 667 33. 198 24. 760 2.0 6.9 4.0 69 10. 94 12. 667 33. 198 24. 760 2.0 6.9 4.0 69 10. 10. 94 12. 667 33. 198 24. 933 3.4 47 4.0 89 10. 10. 94 12. 677 33. 117 25. 10. 81 3.3 55 4.0 89 10. 10. 51 13. 399 33. 10. 81 13. 368 24. 933 3.4 47 4.0 89 10. 10. 51 13. 399 33. 10. 81 13. 368 24. 933 3.4 4.7 4.0 89 10. 10. 10. 10. 10. 10. 10. 10. 10. 10.	533	*****	****	10.804		24.831	4	7.3	2	27.4	216			6.9		3
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19071709		14.29	11.530		24.257	4	516	4.4	1.39	137	2.5	7 6 F		3.	
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15 MINUTE AVERAGES: DATA

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15 HIRBIC AVERAGES: DATA

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15 MINITE AVERAGES: DATA

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HINDLE AVERAGES: DATA

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20071640	17.46	16.16			24.591	10.1	211	2.3	263	27.3	40		1 11	69		3 	
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15 MIND'TE AVERAGES: DATA

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201/0842	15.73	14.45	11.373			6.8	5.	1	217	3.3.3	40	٠.	98 N	6.7		3	3
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28171258		15.28	11.471			1.0	271	<u>ۍ</u>	.545	37.2	41		4	69		. 56	3
201/1313	16.85	15.45	11.531			10.3	2	9.1	239	29B	46	5.	200	69		20	3
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51417105		14.97	11.389			10.3	= (4:	?		9	ŗ	2	9	10	2	3
201/1468	•	15.55	11.555			 		æ :	1 2 3	143	= :	5	Z	60	-	3	3 :
20171443	17.24	15.71	11.629	32.856		9	249	-	2.3	100	@ T	5.5	Z	63)	4	3	3

15 MINUTE AVERAGES: DATA

2011/15/23 16 55 9 19 11 15/25 3 28 19 10 5 5 10 11 1 1 1 1 1 1 1 1 1 1 1 1 1	Z, 516	TA desgC	3frap	15 Jeop	SAL.	S16T q/cm##3	MS m/sec	03 1	SHIPS M/Sec	CSF.	Gep 99H	e (beg)	LAT mins		lean -	1.08G	un.
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1, 14, 25, 14, 15, 15, 25, 37, 15, 15, 15, 15, 11, 10, 10, 11, 140, 197, 197, 197, 197, 197, 197, 197, 197	1/1513		15 66	11 213		24.907	1 8 1	241	?¥ -	36	96	24	56 47	z	69	3. 39	3
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(6) (1) <td>1/1613</td> <td></td> <td>14 67</td> <td>11 369</td> <td></td> <td>24.827</td> <td>6 2</td> <td>350</td> <td>) (C.</td> <td>3.6.3</td> <td>7</td> <td>90</td> <td>58 71</td> <td>z</td> <td>6.9</td> <td>3 1 5</td> <td>3</td>	1/1613		14 67	11 369		24.827	6 2	350) (C.	3.6.3	7	90	58 71	z	6.9	3 1 5	3
6.6 6.7 6.8 6.6 6.7 8.1 6.9 6.8 6.9 <td>20171628</td> <td></td> <td>14 69</td> <td>11.400</td> <td></td> <td>21.599</td> <td>8 H</td> <td>652</td> <td>9.</td> <td>239</td> <td>265</td> <td>2</td> <td>59.38</td> <td>z</td> <td>6.6</td> <td>5 1.3</td> <td>3</td>	20171628		14 69	11.400		21.599	8 H	652	9.	239	265	2	59.38	z	6.6	5 1.3	3
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16.67 15.29 11.445 32.304 24.629 B.4 197 7 90 80 40 50.19 H 69 19 16.40 15.62 11.443 32.244 24.640 8 3 196 8 103 40 40 50.19 H 69 19 16.40 15.02 11.443 32.243 24.641 9.8 251 1.7 260 203 40 49.90 N 69 19 15.29 14.455 32.340 24.641 9.2 260 1.0 162 40 49.90 N 69 19 16.37 14.625 32.340 24.641 9.2 260 1.0 162 19 40 49.90 N 99 19 16.37 14.625 32.243 24.641 9.2 261 1.0 162 19 40 40 40 40 40 40 40 40 40 <td< td=""><td>201/2044</td><td>9</td><td>14.64</td><td>11.424</td><td></td><td>24.652</td><td>8.2</td><td>204</td><td>7</td><td>63</td><td>91</td><td>48</td><td></td><td>z</td><td>_</td><td></td><td>3</td></td<>	201/2044	9	14.64	11.424		24.652	8.2	204	7	63	91	48		z	_		3
16.40 15.02 11.431 32.274 24.608 8.3 196 6 103 80 40 50.10 69 18 16.91 15.27 11.443 32.213 24.644 8.1 191 12 40 89 69 18 15.26 11.425 32.213 24.644 8.1 191 12 40 49 90 8 18 196 19 <td>201/2059</td> <td>9</td> <td>15.29</td> <td>11.445</td> <td></td> <td></td> <td>B. 4</td> <td>147</td> <td>7</td> <td>6.6</td> <td>80</td> <td>=</td> <td>50.19</td> <td>*</td> <td>_</td> <td></td> <td>3</td>	201/2059	9	15.29	11.445			B. 4	147	7	6.6	80	=	50.19	*	_		3
16. 91 15.57 11.443 32.213 24.559 8 9 251 1 7 26 264 40 49.74 69 19 15. 26 15. 54 11.445 32.326 24.646 9.2 260 1.0 462 40 49.68 8 19 19 19 19 19 19 16 16 9.2 260 1.0 462 40 49.68 8 19 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 17 16 16 16 17 16 16 17 16 16 17 16 16 17 16 16 17 16 16 16 17 16 16 17 16 16 16 16 16 17 16 16 16 17 16 16 17 16	1/2114	9	15.02	11.431			8.3	196	8	103	80	40	50.10	z		<i>3</i> 9 €	3
17.26 15.94 11.445 32.350 24.641 7.8 251 1 261 20.3 40 49.68 N 69.19 15.29 14.45 32.318 24.644 6.1 191 .2 40 49.90 N 69.19 15.29 14.45 32.343 24.646 9.2 260 1.1 167 176 8xx xxxxxxxx xxxxxxxx xxxxxxxx xxxxxxxx xxxxxxxx xxxxxxxx xxxxxxxxx xxxxxxxxx xxxxxxxxx xxxxxxxxx xxxxxxxxxx xxxxxxxxxx xxxxxxxxxx xxxxxxxxxxxxxxxxx xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx	1/2129	9	15.57	11.443			8	230	1 8	200	244	46	44.74	z			2
15.70 14.55 11.455 36.318 24.644 6.1 191 .2 47 82 40 49 90 N 69 19. 16.37 15.07 11.425 32.343 24.646 9.2 260 1.0 162 140 *** **** **** **** **** **** **** *	1/2144	1	15.94	11.445		24.641	8.7	550	1 7	560	203	40	49.68	z			3
17.28 16.07 17.02 17.03 <th< td=""><td>176157</td><td>, v</td><td>14.55</td><td>11.465</td><td></td><td>24.644</td><td>. o</td><td>171</td><td>N e</td><td>7</td><td>N o</td><td></td><td>49 98</td><td>2 i</td><td></td><td></td><td>3 4</td></th<>	176157	, v	14.55	11.465		24.644	. o	171	N e	7	N o		49 98	2 i			3 4
17.32 16.07 11.446 32.308 24.631 7.9 221 1.0 129 104 40 49.97 N 69.20 129 104 40 40.97 N 69.20 129 10.0 11.441 32.267 24.603 6.8 231 171 40 50.07 N 69.20 16.90 16.90 14.29 12.267 24.603 6.8 231 173 40 50.07 N 69.20 16.90 16.90 14.72 11.27 32.267 29.9 48 56 20.07 N 69.20 16.90 14.60 20.00 14.60	1/2229		15.62	11 409		24 666	y M	2000	-	100	176		*****	* *		***	*
17.28 16.07 11.441 32.287 24.617 7.7 21.7 .6 21.1 17.1 40 50.07 N 69 16.97 15.77 11.429 32.267 24.603 6.8 21.1 5 32.8 11.4 40 50.07 N 69 16.91 15.70 11.429 32.267 24.643 4.5 29.7 1.3 40 50.23 N 69 16.91 14.75 11.274 32.274 24.641 4.5 29.7 2.9 48 50 40 51.0 89 1.0 <td>201/2244</td> <td>1</td> <td>16.07</td> <td>11.446</td> <td></td> <td>24.631</td> <td>2.9</td> <td>122</td> <td>. 0</td> <td>129</td> <td>104</td> <td></td> <td>49.97</td> <td>f f 22</td> <td></td> <td>0.74</td> <td>- 3</td>	201/2244	1	16.07	11.446		24.631	2.9	122	. 0	129	104		49.97	f f 22		0.74	- 3
16.99 15.77 11.429 32.267 24.603 6.8 211 .5 328 114 40 58.23 N 69 16.91 15.70 11.424 32.251 24.641 4 25.7 13 48 58 N 69 16.91 14.75 11.274 32.276 24.641 4 26 3.1 28 50 48 58 N 69 16.13 14.07 32.27 24.645 4.2 27 28 50 48 59 N 69 16.13 14.07 32.262 24.663 4.2 27 22 27 40 51 89 16 40 51 89 16 40 51 89 16 40 51 89 16 40 51 16 40 52 30 89 16 40 52 30 89 16 40 52 30 40	1/2259	~	16.07	11.441			1.7	212	9.	211	171	9	50.07	z	69 2	0.76	3
16.91 15.70 11.424 32.851 24.591 6.8 225 7 197 113 48.58.38 6.9 16.00 14.75 11.274 32.278 24.641 4.5 257 2.9 48 58 40.51.50 N 69 16.13 14.27 32.27 2.4 6.2 4.3 24.6 3.1 22 57 40.54.30 N 69 16.13 14.51 11.158 32.202 24.663 3.9 282 27 50 40.51.20 N 69 15.83 14.51 13.7 24.619 4.4 247 4.1 35 93 40.57.28 N 69 16.01 14.51 14.4 24.7 4.1 35 93 40.57.28 N 69 16.01 14.53 14.7 4.4 24.7 4.1 35 24.8 52.3 N 69 16.01 14.53 14.5 14.4	1/2314	6.	15.77	11.429			9.9	211	S.	328	114	40	58.23	z		0 93	3
16.00 14.75 11.274 32.276 24.641 4.5 257 2.9 48 56 40 51.50 N 15.56 14.01 32.262 24.645 4.3 246 3.1 22 50 40 52.96 N 16.13 14.02 32.262 24.645 4.4 245 3.2 27 55.78 N 15.11 13.79 11.102 32.202 24.643 4.4 217 4.1 35 93 40 55.78 N 16.13 14.51 11.102 32.204 24.636 4.4 217 4.1 35 93 40 57.37 N 16.10 14.51 11.106 32.204 24.636 4.5 20 2.0 337 29 40 59.73 N 16.10 14.52 11.106 32.065 24.490 4.5 20 2.0 337 29 40 59.75 N 17.45 16.00 14.65 11.206 32.065 24.490 4.5 20 25 293 269 41 53 N 15.86 14.46 10.694 32.065 24.596 2.6 28	1/2329	9	15.70	11.424		24.591	9 9	225	. 2	197	1.1.3	48	58.53	2		96 0	3
15.56 14.51 11.17.3 35.262 24.65 4.3 246 3.1 22 50 40 52.76 N 16.13 14.02 11.073 32.262 24.665 4.4 245 3.2 27 55.78 N 15.11 13.79 11.102 32.202 24.665 4.4 217 4.1 35 93 40 55.737 N 16.13 14.51 11.102 32.202 24.636 4.4 217 4.1 35 93 40 55.737 N 16.13 14.51 11.107 32.202 24.636 4.5 20 2.0 317 29 40 50.74 N 50.74 N 16.00 14.52 11.106 32.065 24.490 4.5 20 2.0 317 29 40 59 27 N 17.45 16.00 14.60 32.065 24.479 3.1 214 2.5 293 269 41 11 N 15.86 14.46 10.958 32.065 24.574 3.1 24 3.3 41 62 N 16.22 14.86 11.398 31.836 24.274 3.4	1/2344	é:	14.75	11.274		24.641	4 . N ,	252	61 ·	46	<u>ت</u> ا	0 :	51.50	z	2 69	0.64	3
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15.11 13.77 11.150 32.202 24.619 4.4 217 4.1 35 93 40 55.78 N 16.13 14.51 11.102 32.224 24.619 4.4 217 4.1 35 93 40 55.78 N 16.10 14.51 11.10 2.6 22.6 24.49 4.4 217 4.1 35 29 40 59.73 N 17.45 16.00 11.206 32.054 24.49 4.9 2.6 2.0 337 299 40 59.57 N 17.46 16.07 10.694 32.065 24.496 2.6 2.6 251 1.5 291 256 41 11.N 15.86 14.46 10.958 32.065 24.521 3.1 244 3.3 76 91 41 62.N 16.22 14.82 11.398 31.836 24.274 3.4 257 3.0 115 135 135 41 62.N 16.99 15.69 11.358 31.836 24.274 3.4 257 3.0 115 135 135 41 16.N 16.99 15.67 11.463	6100/2	ر ه	14.07	11.673		24.665	क किं	0.0 4.0 2.0 3.0	N 4	200	ហ្គ ។ ហ	0 4	54.30	z:	69	- C	3 :
15.65 14.51 11.102 36.207 74.617 4.4 217 4.1 35 93 40.57.37 N 16.13 14.70 11.070 32.224 24.636 5.3 210 2.0 316 287 40.57.37 N 16.10 14.20 32.054 24.479 4.5 289 2.0 317 279 40.57.7 N 17.46 16.07 10.694 32.065 24.479 3.1 24 2.5 293 269 41 11 N 17.46 16.07 10.694 32.065 24.521 3.1 24 3.3 76 91 41 62 N 16.22 14.86 10.958 32.050 24.521 3.1 24 3.3 76 91 41 62 N 16.22 14.86 11.398 31.836 24.274 3.4 257 3.0 115 135 41 186 N 16.99 15.67 11.463 32.148 24.584 2.3 80 2.5 153 161 40.597 80	120072	ŕ	13.77	11.156		64.603		N.	= .	¥.	64	2	55.78	z	20	1 67	3
14.70 14.70 14.10 32.164 24.49 4.5 210 2.6 310 287 40 59.57 N 16.00 14.26 32.065 24.49 4.5 289 2.6 317 279 41 11 N 17.46 16.07 10.694 32.065 24.499 4.5 281 1.5 221 236 41 11 N 15.86 14.46 10.958 32.050 24.521 3.1 244 3.3 76 91 41 62 N 16.22 14.86 11.398 31.836 24.274 3.4 257 3.0 115 135 41 .66 N 16.22 14.86 11.358 31.836 24.274 3.4 257 3.0 115 135 41 .66 N 16.29 15.69 11.346 24.274 3.4 272 2.8 153 161 40 59.75 N 16.70 15.67 11.463 32.148 24.584 2.3 80 2.5 153 152 40 59.62 N	040072	, v	14.51	11.102		24.617	4 F	212	4.0	3.5	1	9 4	57.37	z	69	90.9	3
10.10 14.65 11.176 52.065 24.470 4.5 207 2.0 517 279 40 59.57 N 17.45 16.07 10.694 32.065 24.479 3.1 214 2.5 293 269 41 11.N 11.N 15.86 14.46 10.958 32.050 24.521 3.1 244 3.3 76 91 41 62 N 16.22 14.82 11.398 31.836 24.274 3.4 257 3.0 115 135 41 66 N 16.99 15.58 11.335 31.836 24.274 3.4 257 3.0 115 135 41 66 N 17.07 15.67 11.463 32.148 24.584 2.3 80 2.5 153 152 40 59.62 N	2 / 0 4 4 5			44 407		0.4.40	9.4	0 1 0	0 e	010	/80		- / · OC	2 :	70		3
12.46 16.07 10.694 32.065 24.596 2.6 251 1.5 221 236 41 53.8 15.86 14.46 10.958 32.050 24.521 3.1 244 3.3 76 91 41 62.8 16.22 14.82 11.398 31.836 24.274 3.4 257 3.0 115 135 41 .86.8 16.99 15.58 11.335 31.836 24.288 2.4 272 2.8 152 161 40 59.75 N 17.07 15.67 11.463 32.148 24.584 2.3 80 2.5 153 152 40 58.62 N	2/0130		16.08	11 206		24.479	t W	200	e u n	203	6/2	4 4 5 4	57.57	z 2	7 69		3 3
15.86 14.46 10.958 32.050 24.521 3.1 244 3.3 76 91 41 62 N 16.22 14.82 11.398 31.836 24.274 3.4 257 3.0 115 135 41 .86 N 16.99 15.58 11.335 31.839 24.288 2.4 272 2.8 152 161 40.59.75 N 17.07 15.67 11.463 32.148 24.584 2.3 80 2.5 153 152 40.58.62 N	2/0145		16.07	10.694		24.596	9	251	, -	555	236	41	5	: 2	60	9 4	3
5 16.22 14.82 11.398 31.836 24.274 3.4 257 3.0 115 135 41 .86 N 0 16.99 15.58 11.335 31.839 24.288 2.4 272 2.8 152 161 40.59.75 N 5 17.07 15.67 11.463 32.148 24.584 2.3 80 2.5 153 152 40.58.62 N	202/0200	15.86	14.46	10.958		24.521	3.1	244	5.	26	9.1	11	.62	z	69	H	3
16.99 15.58 11.335 31.839 24.288 2.4 272 2.8 152 161 40.59.75 N 17.07 15.67 11.463 32.148 24.584 2.3 80 2.5 153 152 40.58.62 N	2/0215	16.22	14.85	11.398		24.274	4.4	252	3.6	115	135	41	.86	z	1 69	6 32	3
17.07 15.67 11.463 32.148 24.584 2.3 60 2.5 153 152 40	12/0230		15.58	11.335	Œ	24.288	4.5	272	æ ?!	152	161	40	58.75	z	69 1	5 .56	3
	5/0545	=	15.67	11.463	₹.	24.584	63	90	6. 5.	153	152	40	59.65	z	1 69	4.63	3

I DESCRIPTION OF THE PROPERTY OF THE PROPERTY

S MINITE AVERAGES: DATA

15 HINDE AVERAGES: DATA

DTG.Z	4	100	25	N.	1918	3	o fi	SHIPS	15.	H61;		4			_	1 000		
	deap	de-gE	ghap	p d d	g/cm##.5	1017.79	desid	J. 1. 1. 1	ded	h.de	Perfe	3	mins		the d	3	. Ξ	
202/1502	1.5.68	11.92	11.791	32.538	24 7.39	2 %	#.V¢	9 -	14.5	153	40	5.	3.6	2			4	2
202/1517	13.70	11.95	11.78.3	32.533	24 743	10 2	36.0		196	241	40	5.	2	z			~	3
202/1532	13.66	11.92	11,852	32,535	24 7.31	18 3	346	¢	265	272	4 6	2.0	59	2			36	3
2112/1547		12.15	11.966	32,535	24 7119	10 4	3.311	9	.52°	7.116	40	20	:: E	z			2	3
202/1682		12.36	12, 825	32 535	84 6VB		34.	s	402	51%	96	51.	2	z	53	3.0	4	3
202/1617		12.38	12.045	٠.	24.692	12.3	355	9	143	270	40	0.5	2.5				=	~
282/1632	1.5.96	12 25	12.842		24 687	ಷ ಪ	.546	יע	161	5/2	4)	95	7	2			1.4	3
202/1647	13.95	12.21	12. 152	32.515	24.678	5.5	3.25	9	170	27.0	40	3	.518	z				7
28271702	***	***	12.056		24.671	ر ا ا	\$5.6	٥.	15.3	26H	4.	46	26	2			=	3
2112/1717	****	****	12.1173		24.657	10 0	3.14	/d ←	600	5/2	40	49.	25	z			2	7
282/1732	**	****	12, 132		24.613	12.1	544	9 (268	201	46	46	51	2				3
202/1747	****	****	12.165		24.550	11.7	346		366	262	46	40	46	z			5.5	7
282/1862	***	****	12.187		24.505	8.81	3411	5 -	24%	2.7.E	40	19	96	z			9	3
2112/1817	****	****	12.183		24.408	10.4	355	4	500	27.1	46	43	30	z		1:4	=	7
28271832	****	****	12.141		24.583	10.2	361	3	192) ER	=		61	z			11.	3
202/1047	14.60	12.65	11.978		24,638	10.3	351	9 5	175	121	40		55	z				-
20271982	14.74	12.38	12.085		24 777	10 7	350	5	175	17.1	41)	2.4	64	2		140	=	2
202/1917	14.85	12.09	12.067			10.3	363	5	17.5	17.4	4		1.6	z			4	_
202/1932		11.73	11 996	32,686	24.621	E &	354	=	127	17.5	-		3	2				=
202/1947		11 01				5	34.0	2	179	41	4 11	7	34	z			*	-
205/2002		10.68				-	344		167	9,1	40		2	: 2				3
202/2817	14.76	10.60				5	347		179	17.6			6.1	z				-
202/2032		11.01	15.311			16 11	547		1.7.7	17.1	_	, 	20	2			4	
202/2048		11.69				× 22	354	7.2	178	17.5			4	Z			=	-
202/2103	16 44	12.17	18.837			9.8	358	1 /	179	17.4			64	2				3
202/2118	16.53	12.17		33.656	24.1113	12.9	354		170	173	43	15	21	Z			5	7
202/2133	16.82	12.46				11 8	35.5	5.3	168	173	安子安		*	*			*	*
202/2148	17.64	12.62	20.229	33.845		5 27	3.18	= 9	179	174	24		42	z		14.	1	-
28272803		12.49				ن. ا الله	344	7.8	17.0	17.4	4.5		0.0	2			=	3
202/2218	17.01	12.50	19.616	33.806		42.B	342	7.2	177	174	40	-	53	2			9	7
282/2233		12.49		33.798		13.1	342		2	17.4	3.5		90	.2			=	2
2112/2248		12.21		34.102	23.750	13.7	343	7.8	176	174	39		29	z			9	_
20272363		12.96		34,680		13.7	34.3	7.1	176	17.5	39		7.4	z			=	2
202/2310		13.38	23.136	35, 1114	-	13.7	344	7.1	172	168	39		37	2			2	-
282/2333	17.96	13.49		.45, 1162	23.944	(3.2	347	7.1	173	16.9	31)			2			~	3
202/2340		13.61		35.111		13.6	343	0	17.3	169	3.6	40	7.3	z		æ	1.	3
20.5/040.3		13.71		35.179	23.675	1.5.2	345	0 . /	174	169	36	37	5	2			=	3
203/0018		13.84		35,117	23.769	12.9	339	- ~	175	169	39	34	16	z			=	7
203/00.53		13.94	23.819	35, 184		12.5	3.54	6.9	175	169	39	.30	10	z		36	5	3
203/0048	•	13.98		34.647		1.0.1 1.0.1	3.3%	6.9	174	170	39	23	46	z			44	7
203/1103		14.05	٠	35.025	23.844	12.3	3.35	6.7	176	176	3.5	5	2	z		•	66	3
203/0118		14.25	24,329	34.891		42.9	3.37	6.7	17.3	173	39	50	06	z			÷	7
203/0135		14.58	24.144	34.674		12.6	3.37	6.7	175	170	5.5	12.	62	2			90	3
205/0148		14.51	24.646	35.066		11.4	3.39	5.6	173	170	***	**	*	*		*	*	4
283/0203	20.02	14.74	24.982	35.261	23.561	12.1	3.34	6.7	17.5	170	36	11.	22	z		. 4	Ξ	3
8120/802		14.89	24.664	34.955	23, 426	20.0	3.37	6.8	173	174	36	1	75	z	69	7	3.0	=
2027000		14.74	25.067	54.952	23.301	13.1	3.47	6. H	174	1/4	Š.	~	46	z	69	-	E	2
84207612	30.56	15.11	25.250	34.999	23.2811	11.7	333	6.9	175	174	3.9		¥.	z	. 69		7	7

15 MINDLE AVERAGES: DATA

2,510	TA	Tip	18 dead	SAL.	SICT	45 8/8/16	3 1	SHIPS	CSE	HOE	den	1.AT	u.	- Herr	LONG	y
						20 mm and day, now, 10	-						-		-	
203/0303	20.69	15.18	25.335		23, 364	6 11	327	6 9	175	174	38.5	7.75	z	69	2.3	3
203/0318	20.81	15.29	25.248		23.330	11.1	3,24	6 9	174	174	H.	4 38	z	2 69	1 87	3
203/0353		15.39	25.618	35.076	23.825	18 8	327	6 H	175	1.7.1	30.4	6.78	2	8 69	7. 1	3
203/0408		15.56	26.021		23.261	10.0	324	8.9	179	1 11	30 4	3.46	z	8 69	0.7	3
203/0423		15.64			23, 115	10.7	36	6.7	176	160	30	11.17	2	67	=	3
20.370438	21.47	15. ZH		35.295	23. N42	11.	322	6.7	174	134	98	6.9	z:	69	= :	3 :
203/0453	24.69	15.47		33.174	66.605	2.0	3.30 3.30	9.7	170	276	20.5	4.70	2 2	707	· ·	3 :
2020/200		45.04		34 662	900 000	2 . 2	200	u U	0.7.7	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	202	100	Z 3	200		3 5
203/0538	21.57	16.06	26.240	35 093	23 043		500		139	277	0 20	16.	zz	69		3 3
203/0553		16.16				5	5.41		5	283	E	69 1	: 2	56	5	3
203/0608		16.31				11.0	33)	1.6	66	276	30 3	11.77	z	69	8 27	3
203/0623	21.97	16.42				9.5	345	1.3	74	190	38	0.85	z	69	7. 44	3
203/0638		16.43	26.334			H. 7	382	£.5	92	152	38 3	86.0	z	69	18.9	3
203/0653		16.14	26.352			7.4	334	1 . 1	6.3	273	3.1	10.97	z	69	SB	3
203/0708		16.01				7	332	<u>م</u> :	0 :	26H	333	1.92 1.92	2:	69	o.	3
203/0723	77.12	16.06				9 1	N 1	ဆ	901	752	7 (F	10.00	z :	7 .	4. /	3 :
85/0/502	21.83	16.18			23.134	2 °	36.5		4 6	564	5.5	67.13	2 :	70	4	3 :
2070/202		10.60					100	2 •	201	0 1		0 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2 :	70		3 :
20272027	10.10	10.16			7	e :	5114	1.0		200		58.61	z:	7.0	9:	3
202/0020	+	10.01				= 5	2 1 2	C C	001	200		2 4	2 :	70		3 :
203/0853		16.40				2 0	365	. 0	187	1000		34. 45	: 2	60		3 3
203/0908		16 17				6.7	3.02	. 2	180	275		200	: 2	704		3 2
203/0923		16.22				ı. V	304	9	H-9	202		30 32	: =	69		3
203/0938	1.0	16 34				S.	296	S	640	271		0.39	z	69	2.0	3
203/1323	23,82	17.44				6.1	366	3.7	269	270			z	69 1	6.46	3
203/1338		17.69				6.1	992	3,73	569	271		66.6	z			3
203/1353		17.69				6.2	263	= ·	277	270		30.09	2:			3 :
202/1400	0.00	10.03				0 0 4. 5	0 0 0 0 0 0	4.5	100 100 100	107		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	z			3 7
203/1438	24.13	17.86	27.619	35 597	22.978	. E	267	7. 6	167	24.7		29	: 2			3
203/1453		17.83				6.01	247	5.	65	247	38	1.20	z			3
203/1508	24.17	17.86				10.2	271	3.1	39	318		52.2	z	-		3
203/1523		18.20				10.5	270	4.3	99	20		33.33	z	-	5.67	3
203/1538		18.21				11.0	296	4.6	0.6	65		33.76	z			3
203/1553	24. 45	17.46				1.8.0	237	- - :	126	1.39		55.17	z:	•		3
8091/502	24 76	70.75		•		7.7	2,04	N e	14/			36.14	z:	69	E .	3 :
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203/170B	****	****			24 454		24.0	10	26.0	000		40	2 2	1 07		2 :
203/1723	****	****		35.869	23.157	6	242	3 PT	267	220		16 68	: 2	69	2 . 4	3 2
203/1738	****	****		35,830	23.089	8.6	239	4	27.1	267		9 189	2	69	0 0	3
203/1753	****	****	27,869	35,802	23.049	11.7	228	6.0	1.3.3	133		29.48	z	69	0.2	3
203/1808	****	****		35.602	. 23. NS2	12.3	231	2.7	184	133		9.18	z	69 1	7 HE	3
203/1823	****	***		35.813	23.075	***	**	9.2	89	198	-	B. 82	z	69 1	2	3
203/1838	25.10	18.56		35.807	23.072	13.2	243	1.6	7.5	271		9.25	z	69	4 35	3

S BINDLE AVERGELS: DATA

S MINHTE AVERALES: DOTA

7:11:	F.F	106	1.5	SAL	1212	83	GHA	SHIPS	135.1	Sign	_	A.			3143	
	deapE	deg	Sperb	t do	g/cm##3	m/enec	ded	335/6	ded	hed	0.40	3 : 2	<u>4</u>	hap	ε	3111
0.7	25.34	19.18				101	562	٠.	245	261		9 26	z	6.9	20.	3
H-4/0723	25.37	19.27	28. 11211	٠.		6.7	26.5	01	5.5	093		9 38	z	69	211 1	2 4
04/8730	55.33	19.25				4.4	6.57	7	12	404			2	33	9.3	3 =
04/0753	25.31	19.43	-			7.4	6.36	₹.	34.0	698			z	69	21.1	3
0479830		19.53				1.1	7.1	4	199	27.11			z	20	- 5	33
n 4 / 0023	25.35	19.56				7.9	100	4	140	27.6		H. 1.5	z	63	- H.	3
04/30/50		17.64				¢	. 5.1	٠.	143	1.70			2	69	= = =	5
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n4/0923	25 46	19.02				1,7.6	1.45	·	156	1.5.			7	6.5	4 61	3
014/8930	25.44	19.76				1.5.9	1.6.3	-	0 1	15.7			2	1.5	. 4	₹ *:
14/0953	25.44	19.04		٠.		13.7	263	ē.	1.47	0.50			z	4.7	1.7.1	3
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44/1023	25.41	28.12				14.2	690	eri.	1111	250		179	=	69	19 6	3 3
BE91769.	25.46	26.28				63.9	995	e4	5.5	25.1			z	40	1.7	F .3
114/1053		28.33				13.6	5.7.3	3	011	243			z	6.3	19	3
184/1180	28.28	20.48				11.3	27.0	6.	161	247			2	69	1.6	P1 13
04/1123	26.92	20,65				8.1	59%	Ξ	311.3	569			z	69	19.4	3 =
98.11766	25 180	20 62			-	12.8	26.15	·c	123	24%			2	69	19.7	3
114/1153	25.79	20.68				12.0	11/6	0.	209	241			z	69	19 9	3
B04/120H	26.11	20 85				12.3	27.0		21.0	4.		0.1.0	z	69	20	:
104/1223	26.16	20.89				5.46	119,5	r.	175	241		68 6	z	6.0	P. H.	: :
884/1238	26.49	25.16				5 11	2613	~;	163	16%		٠.	z	69		() :I
114/1253	76.59	21.25				11 2	062	n.	164	1) 15 6			Z	6:2	. 0.	7
114/1348	26.67	21.31	٠.			2 01	268	~	167	145	300	9.50	z	60	20 0	H ts
114/1323	26.01	21.41				5 0 5	265	· ·	176	2.59			z	30		19 9
0471330	26.72	21.35				8 6	200	=	55%	Ser.			2	69		87 14
18471357	26.46	21.26				10.01	123	2.3	4.5	342			z	63		1
8471412	26.97	21.65				4.6	267	5. 5	4.4	6.1			*	***		* *
14/1427	27.2B	21.90				9.B	292	3.6	61)	7.3			z	63		3 /
114/1442	27.75	22.23	٠.			1.01	261	٠٠ ا	613	118			z	6.3		2 5
04/1680	56.69	21.32				11.6	297	6	141	227			Z	69		3
14/1615	26.59	21.21					267	•	3	508	E :		z	60	5	M (1)
1971658	76.57	21.23				11.7	152	-	?	111.5			z.	6.9		= :
2447845	76. H4	/4.1.				= :	45.7	N :	D	45.			z :	60		3 :
04/1/40	****	***		4		Y		= : : :	70	# C C			2 :	44	٠ د د	3
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00 / 1 / 1 / 00	****	****				0.0		n i	100				2 7	2.		3 :
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11 / 12 / 13 / 14 / 15 / 15 / 15 / 15 / 15 / 15 / 15	26 77	77 50				3	27.5	7. 5	0 0 0	2 2 2			2 2	3		3 :
N4/1845	26.63	200				4 5 1	200		100	36.4	-		2 2	000	5 4 5 9	3 -
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104/1915	67. 34	50. 30					26.4		3.4	141			2	200	T 0.	3 3
004/1930	26.03	21.41	27.647	35, 975	23.252	111	550	เก	119	161		A BA	: z	65)		7
204/1945	26.75	21.35		35.966	23.242	11.9	261) (N	121	100	311 2	28.30	: 2	6.9		3
0002/50	26.65	21.27	27.670	35.970	23.240	12.2	202	.7	136	2,32		7.90	z	63)	7	3

15 BINGLE AUTOCES, DATA

7.510	4 H	100	13	SAI.	1918	SB	98	SHOPS	CSF	HDC	_	-			E Ords		
	deap	dent	Jbap	*	1)/r.m**.5	n/4.191.	-	M/*.6.C	ોલ્ય	وإخط	1)6:4	Mins	511	વુક્ત	3	Solf	
20472015	76.57	21.22	27.671	35.940	23.240	13.2	260	4.1	177	232			Z	6.9	s.	1 64	~
204/2030	26.45	21.15	27.653	35.999	23.268	13.7	26.0	2	219	231			Z	6.9	10	1 /9	_
204/2045		21.14	27.637		23.279	1.3.3	262	.3 ((22.0	232			*	63	=	1 683	~
204/5059		21.18	27.574		23.270	13 3	26.2	3.0	223	2.51			z s	69	1.5	1.1	_
204/2114		02. 20. 10.	27.7KB	35.946	23.213	4.5.4	692	<u>ر</u>	\$ 0.50 \$ 0.50 \$ 0.50	7.32			3	63	4	-	7
20472129		2.5	27.805		23.167	ر ا ا	561	- '	9.72	2.7			Z :	6.3	<u>.</u>		-
204/2/44	26.47	26.23				S :		~: ·	2.5	2 C			2 3	60	_ :		-
2012/102		02.17				16.7							z :				
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1333/607								= C					z :	10			
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264/2343		30.30						e e	0.50	200			2 3 2 Y				
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204/2344		27. 27				. •	2.0	 		1 17 2 17 2 17 2 17			. 4				
28472359		21.29				4	245	i m	245	236			: Œ	6.9			_
205/0014		21.26				7.0	239	15. 10	24.5	23.5			2	69			_
20570029		21.23				3.	234	2	543	236			Z	69			_
205/0044		21.24				٦.٢	25.7	٠. در	243	23.5			3	6.9			-
5007502	26.24					S. 0	622	3.5	244	236			Z	69			_
205/0114	02 92					S. S.	2.30	3.5	24(2.34			3.6	69			_
505/0129	56.21					4.6	5.5.7	∯. 15	2.30	2.31			2	69 .			_
205/0144	26.13					٠ ن	15.5	ئاً. ج	237	231			.2	6.3			7
205/0159						7 1	24.5	3.6	2.30	232			2 2	69			_
205/0214						7.	10. 10. 10.	*	239	25.0			2	69			~
20270229						o. :	23.5	3.6	248	23.2			7	69			_
205/0244	25.79					2 1	2.59	·0 ;	= : 	3			2:	\$ Q			7
20270237	67.75	٠				5.7	4 4 5	, e	5.4.3	6.34			Z :	6.0			
6020/502	25.60	20 84	26.70%	35 197	70 674	. v	0.45	÷ 4	10 m	9 5 7 0 V 0	5 6 6 6	4 . 4	ر د ح) Q	6 2		2 3
205/0344	25. AB						200	. 4	3 6	200			3 0	2.			, -
20570359						7.3	252	<u>ج</u>	733	228			z	0 1			_
20570414						7.0	253	4.4	220	225			2	7.0			7
205/0429						7.5	246	4 6	222	221			7 7	7.0			_
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205/0459						五 s	25.	4.	223	() () ()			z:	20			_
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202/022	20.13	24.00		33.430		ر: _*	200	4 4 2 3	2.54	0.50		46. 4	zz	- 5	2 0		
905/0639	20 02	20 40				- U	0.00			220							
205/0644	•	20.11		34.340		9 PM	2 4 5	0	240	200			ב עמ	2			
205/0659	24.30	19.98		34.340	22 634	4	240	4	234	2 24			2	2.	00		
205/0714		20.10		34.313	22.614	. r.	747	. 0	230	2.3			2	20%	. c.		, -
505/0729	Ŋ	20.16		34.341	22.635	4.3	236	4.7	2.30	230		38.1	Z	2.0	4.		_
0	24.64	20.20	25, 733	34.341	22.635	4	2.36	4.9	2.30	22.9		36.6	Z	2.0	36	_	7
205/0759	24.69	20.08	25.733	34.342	22.635	7.8	553	4.6	55.6	600		35 0	2 5.	7.0	36		_

15 MINUTE AVERAGES: DATA

DYG. Z	4	TDP	13	5A).	5761	55	Û PA	SHIPS	363	501	Ī	LAT			Ortes	
	Shap	Jbap	GedC	ap t	4/58**3	M/sec	help	395/8	(14)	(isa)	desp	mins.	· ·) (p	8000	3 (1
205,0014	24.52					, c	3.56	1. 4	229	229	•	3.5. 4.2	2		t.	0 0
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205/4844	24.14		٠.		_	2.7	269	1 2	3.58	2.58		5.6 5.5	z			
6580/508	2.5.79					= E	296	4 6	677	2.41		29.04	z			
245/8914	24.08		٠.		-	н Н	650	4.6	688	2.45		45 75	Ξ			
205/0929	24 13				_	6.1	253	4.8	600	230		90.96	z			
245/11944	24.21				-	6 9	45.	4 7	1331	3.51		15. 67	2			
505/0959	24.31				- :	6.7	256	4.7	230	600		23 11	Z			
2017/1014			٠.		٠.	9.9	952	4.7	2.510	2.50		91.62	2			
205/1029	24.04			- 7	-:	7.1	267	4.7	23.0	2.52		20.15	z			
205/1044	23.88				٠.	7.7	26.5	4.7	2.51	231		18.66	2			
205/1059					-:	7.1	5) 42	4.7	626	232		17 16	z			
205/1113					٠.	7.8	152	4.7	225	231		15.67	2			
205/1128				-	-:	0.0	292	4.9	226	230		14.09	z			
205/1143	24.27					975	264	5.3	227	230		12.4)(z			
205/1158				- 7	Ξ.	7.4	274	5.1	227	220		10.71	z			
205/1213	23 23				٠.	9 /	301	6.9	201	2.31		8.3	2			
205/1228					Τ.	3.0	344	e in	552	328		6.33	z			
205/1243	85.90					3.7	=	5.1	122	230		4.60	z			
20571258	16.57				Ξ.	3.9	10	5.1	223	677		2.81	z			
205/13/3	22.90				٠.	¥:	52	5.1	2.35	7.44		1.16	2			
20571328	22.96				Ξ.	4.1	33	0 . S	250	260		5.0	: Z			
205/1343	23.11				Τ.	4.7	96	9 · E	278	906		59.86	2			
20571359	23.34				-:	4.6	18	ري ا	559	224		59.82	z			
205/1414	23.62				Ξ.	6.9	45	4.1	32.5	37		***	₹		-	
205/1429					Ξ.	0	19	₹ .	ب ن	46		1.97	I			
50571444	23.95					is S	357	 1.	5.5	6.5		**	*			
205/1459					Ξ.	4.7	4	64.53	134	141		****	*		344	
20571514						5.7	352	2.B	183	190		18.47	z			
205/1529	24.50				Τ.	5.9	c:	2.8	216	228		58.88	z			
205/1544	-				Ξ.	ر 4.	Un	6. 2.	75.7	27.5		57.64	z			
205/1559				٠.	٠.	3. 6	9	2.3	290	300		52.04	z			
205/1614						6.4	=	1.4	592	281		50.83	z			
205/1629	24.51					6.9	e N	3.3	256	281		50.64	z			
205/1644	24.50					6.9	·æ	9.	238	252		5H. 47	z			
205/1659					Ξ.	7.1	lv.	ĸ.	22.7	592		50.30	z			
205/1714	24.50					7.2	7	ભ ભ	23H	237		57.94	2			3
2012/1729	24.85				т.	6.9	62	100 100 100 100 100 100 100 100 100 100	216	233		56.73	z			

APPENDIX B: Parameter Summary

Parameters, calculated from the variables in accordance with IV. B, are tabulated in time here. The entrees are 15-minute averages. The parameters are:

Parameter	Description	Units
DTG, Z	Julian day/Greenwich time	day/hour, min
TA-TW	Air-water temperature difference	°C
TVA-TVW	Air-water virtual temperature difference (TVW is evaluated assuming air temperature and dew point equals water tempsee IV.B).	°C
RH	Relative humidity	%
TAU	Stress from Smith (1980) parameterization	dyne/cm ²
CD	Drag Coefficient for momentum x 10 ³ (Smith, 1980)	• •
υ *	Friction velocity	cm/sec
L	Monin-Obukhov length	m
Z 0	Roughness height	cm
Н	Sensible heat flux (Smith, 1980)	watt/m ²
Ε	Evaporatine heat flux (Smith, 1980)	watt/m ²

15 MINISTE AVERAGIS. POPARA (1.85)

March Color Colo	D16.7	WI - 41	301-001	<u> </u>		200	* -	- 1	11.7		
Mark 1.75 2.60 996 121 100 113 114 115 114 115 114 115 114 115 114 115 114 115 114 115 114 115 114 115 114 115 114 114 115 114 115 114 1	1	uedt.	at-di.	7	(1/CM**/	×16	J. 1. 1. ZW J	٤ :	2	E/84 %.	W/ W##.
1,75 2 81 91 193 194 195 194 195 194 1	8970486	3	63	96	2.5	68		8 632	2244F-82		,
17.5 2.00 99 1431 144 14.5 14.6 14.	189/6437	1.74		H &	0.75	\$		16.11	111111111111111111111111111111111111111		
16.07 1.08 1.45 10. 11. 4.0 1.66 1.66 1.66 1.66 1.66 1.66 1.66 1.66 1.66 1.66 1.7 1.7 1.66 1.7 1.7 1.66 1.7 1.7 1.66 1.7 <t< td=""><td>2540/681</td><td>1.75</td><td></td><td>98</td><td>.131</td><td>\$</td><td>18 55</td><td></td><td>,</td><td></td><td>•</td></t<>	2540/681	1.75		98	.131	\$	18 55		,		•
1.77 2.40 4.41 1.95 1.04 1.05 <th< td=""><td>7020/684</td><td>1 0.5</td><td></td><td>66</td><td>1.51</td><td>416</td><td>11 54</td><td>11 911 -</td><td>1</td><td>1 6611</td><td></td></th<>	7020/684	1 0.5		66	1.51	416	11 54	11 911 -	1	1 6611	
	8970522	1.77		*	195	.60	12.83	-130 6	1		0.7
4. 18 4. 2 4. 3 138 104 10 70 4. 0 140 4. 0<	2050750	.20	4.	*	175	117		-17.1	1	•	
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. –	90	1.32	60	469	1 1		1 688	CB-15185	1 886	737 31
-	37	1.43	5.6	414	66		6.65	4420F-02	75.0	-6. 801
٠	96	66	56	37.3	6.6		-131.0	3901AE-112	7 00 %	-1 405
190/1044	58	.53	5.6	. 153	90.	15 37	-17.2	.1630E-02	٠.	
	20	30	86	.17.5	.87	12.68	-1.3 5	. 110.15-62	12.199	
	- 114	17	96	315	44	16 32	-36.7	33551 -0.2		
	16	. 0.3	95	. 08:3	. 83	0.35	5 . 3	. 67911: -6.5	10 181	
	15	. e2	46	. 158	90	11 58	-14.4	16000 02	10 020	11 313
19170154	21	. 07	9.3	199	H.	12.93	8 86-	. 21076-02	9.716	122, 652

15 MINIUE, AVERABLES, PAPARITIES

9.03.7	MI-IN degf	TVA-TVW OPGE	ž 4	101 d/cmxx2	CD X10-3	LIA CM/Serie	_ε	2.0 Cm	C**80/13	E/88/3
191 / 02.09	1 50	1.61	5.6	. 0.53	7.3), (),	- 1 E	.39331-113	7.275	-3.959
19170229	4		1.6	. 936	5%	£ .5	1 2:	3790 0.5	5 5.37	-14 1888
19170239	2.24		1.5	. 055	.76	6 55	+ · · · ·	54231-113	4 294	-
19170254	3.26	3.67	115	0.70	3.5	1. 67	7:50 7	7462E-03	1.18%	
19170309	3.07	3.46	<u>.</u>	960.	131	76 5	23 × 30	. 1003F-02	-1 051	-1.15 H64
191/8324	3.09	3.39	66	. 912	.60	2	:	1222E-03	6.50B	-
191/0339	3.53		E 6	. 915	7.5	3.56	-	1596E-113		
151713434	20.0		E (1871)	66.	\ = 3	7.7	62.86E0.5	5/6 2-	
191/11409	5.00 00.00	2.7	E 0	100	C. 5	3. S	2	. 1137F62	25.655	382 355
161/07454	200.0	10 7 E	2 2	201.	2 0		0.00	0.73CE-0.3		7.07. 00-
19178453	5.64	4 19	0 0	12.0	1 N	2 67	: = } } ! !	7442E-0.3		
191/0509	3.16	3. 56	5	. 061	1.2.	7 34	5 04	6423E-03		
19170534	3.65	4.18	66	. 987	. 80	9.40	1 12	9059E-113	-2 705	-27 700
19:70539	4.57	5.12	66	. 1153	.74	6 65	6 6	5574E03	-2.7H4	
19178554			*	. 064	78	7.29	1.5	. 670.583		-36 535
191/0609	4.24	4.74	*	.156	50		1-0 1-0 1-0	.1620E-02	-9.605	1100 1110
191/0624		29.47	*	.207	60.		1.89 5	75-11-1N		- 25 d . (8.5 d
191/0639	9 65	4.10	*	265	26.		26.6	22-3-5-2-5-2-5-2-5-2-5-2-5-2-5-2-5-2-5-2		
191/191	.5. 5B	5.77	*	5 m	\$.		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	31651-112		444 616
171/0/16	कर्त ।	4.74	*	252	5		7.	2584F-92	-14.323	750.037
19178725	×-	***	* ;	15%	5.0		***	NAT HERSE	· · · · · · · · · · · · · · · · · · ·	-
04/0/1/1		61.4	* *	0.42	6.4.0) ;	70-48477	17.4(61	
191/11/55	0.00	9.0	* *	67.6	- C	14.57	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	201011111111111111111111111111111111111	-1.330	171 174
0100/121			6 M	1 G G	1 6.7		2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	201 30 1 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	110 040	837 69-
191/0640			+ *	505	4.		1 /4	6849F-82	-28 ARE	-61 550
19174055			*	217	69		74 3	22.4.45-02	-2 973	-21, 494
191/0918	2.13	2.35	66	.145	. 85	in Bd	11H.2	. 14981-112	0.020	-17 111
19170925	2.05		65	. 215	60	13.24	522 1	. 221 O.F 0.2	417	-19 1153
191/0940	75. 23. 24. 23.	0.5 1	6.5	. 042	.73		-3 B	4297E-113	4 951	
191/0755	3.4.		60	110	2. Q		5.5	11305-02	3 174	-1.5 0131
3701/161	1.19	1.30	200	544.	E. 0	_	-13 9	. 1176E02	9 9 9 9	
101/1065	900	1.55	000	7000	, CO	45.67	000	70-325-17.	\$ / F	100/100
2501/161	3.4	7.4	66	100 100	64	13.48	5.09	00 - 1997-00 00 - 1997-00	3 707	
191/1110	1.20	1.33	*	332	6.		-138 2	3400E-02	3.007	
19171125	06.	1.01	×	141	F) 4	10.71	5 91-	1445-02	6 972	
191/1140	.74	.85	*	.112	. 82	9.53	-101	.1145E-112	6.074	-H 202
19171155	66.	1.14	*	. 266	. 92	14 71	-5H. D	. 27265-112	5 1177	-15.552
19171210	1.28	1.44	*	.350	94	15.89	-1.56.1	.3179E-02	2.762	-10 673
121/1275	1.51	1.69	*	350	5	16.06	-612.7	. 35.8.5 0.2	669	-21 212
191/1241	****	****	* ·	****	***	****	大学をかる女	*****	*****	*****
6531/161	****	*****	*	****	***	***	***	米米米米米米米米米	***	****
191/1912	****	****	*	****	****	****	***	****	******	****
19171701	****	****	* 1	****	***	****	****	* * * * * * * * * * * * * * * * * * * *	***	***
19171542	****	****	* *	*****	***	****	***	*****	****	****
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D16.2	Jo-14	IVA-1VII degC	± 14	DAIL d/cm**2	C0 X10-3	11.8 CM/564	_ ε	7.8	E/8#S	2448/3
	****	4 4 4 4 4	1 4	3 5 4 5 5 4 7				the design of th	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	the same and the s
19171432	***	****	* *	H98.	4 C. C.	8/ 61	本中本中中華	20-38-44	· · · · · · · · · · · · · · · · · · ·	****
191/1447	*****	*****	*	202	90	12.46	*****	.2004F-02	******	*****
191/1502	****	**	50	. 162	. 0.6	-	安全安全安全	16658-02	安華安安安安安	****
191/1517	*****	****	96	141	. E.4		****	1453E-02	****	水水水水水水水水水
19171532	****	***	11.	28.0	. GH	12.78	****	. 205(dE-02	*******	*****
191/1547	****	****	96	215	613	17	*****	2220E-42	****	******
2091/151	**	****	ا دن	192	. F.C		****	197.51 - 62	长水水水水水	********
191/1617	****	****	5	.210	CH.		并亦亦亦亦本	7162E-02	XXXXXXXXXXX	*****
191/1632	***	****	5	160	H	_	與學術學學	. 974BF-83	将母母将并并不	*****
191/1647	*	*****	5.5	100	3.	00 6	米米米米米	1039E-02	X******	****
19171702			5.	116	20.		6.9	12046-02	-12 661	
19171717	5.33	2 86	9	.165	.08		9.6	1714E-02	-15.563	
19171732		5.77	2	168	. 86			175.41-02	-15,749	-37.256
191/1747		2.48	5	141	64	10. ZE		1464E-02	-14.692	-34.702
2001/141		5.69	3	****	***	×	子子子并并	* 李安安安安年	法法法法法法法法	***
171/1817		5.73	2	. 004	80		6.3	.8756E-03	-8.617	BBC 96-
19171832	5.63	6. 12	20	. 071	. 78	2 65	G G	. 7.36.FIF-0.3	-B. 292	-27.446
191/1847		5.60	65	260	90.		7.0	.9685E-0.5		-28 473
19171902		5.84	7	. 132	. A4	0.0	61.	1.56(6F, -02	-13 352	-3.8.200
195/1917	5.53	5.65	36	620	.79	H. 16	6.3	.0257E-03	-7.875	-24.346
191/1932	5.38	5.11.3	9.1	. 1157	.77		. S.	. 5960F-0.3	-5.652	23.469
191/1947	5.39	5.02	9.1	. 633	.73	S 24	5.5	. 5455F - 0.5	-2.076	-18.110
191/2002		เรา	2	. 071	. 26	7 63	6.4	. 2335E-113	-6.533	-23 660
191/2817	5. 5	5.80	9.1	. 075	.79		6 5	. 7836F-03	7 047	
19172032		5. 82	3	. 856	.78		ر ا ا	1,FH381-13	-6.875	-7. S. HUG
75172047	5.26	5.62	5	6.44	.75	6.04	6.3	+6001-03		_
	5.43	5.86	20	11/11	. 78	25.7	ال س	72456 - 0.5	-7.472	
191/2117	5.27	2.67	9	590	. 78		ع 3	. 6HGGF0.3		_
191/2132	5.62	0.4 1.42	36	109	. R.2	6 44	- · ·	. 1182E-02	-9 7/E	-26 826
777/2147	5.24	5.65	S :	. 044	.75	6 81	5. S	4545E-63		-
2022/14			3 0	9811.	. 76		5.5	.5775E-03	325 S	-24 681
141/621/		5.53	9 6	S 1	.72		-141.1	2628F-03	. 063	
101/25/25	9. 70	5.67	0 4	759.	110			5965. 0.3	4.370	
01/0200		10.00	7 7	100.	17.	4.41	5. 47.	. 445E-U.S	3/6	14.1%
9172320	0000	98 C	* *	******	****	*****	****	****	****	***
91723.55		2 82	*	*****	****	*****	****	********	*****	******
91/2355		5.49	68	0.37	7.4	5 67	7 7 7	7.0-72.052	404 6-	********
92/0010		5.53	BE	11411	7.4		. v	41461-83	1945 C-	
5200/26	5.36	5.78	0.6	. 022	7.	4 29	-37. 8	2324E~03	500	
0100/26	4.68	5.11.3	34	. 025	72			25711-03	611	
5500726	4.77	5.13	9.6	1107	585		0 6	1100E-112	-H 613	
9270110	4.89	5.29	7.	. 1166	. 78		7	68641-163		
5210726	4.68	5.49	83	.058	277	6 94	6.5	.6061E-03	-3.694	
192/0140	4.49	4.88	9.3	. 1131.	. 73	5.34	-1105.	.3535E-03	. 01.5	
192/0155	4.75	5, 89	66	680	.80	8.56	8.8	9220F-03	-6.877	
92/0210	4.53	4.92	94	.112	E2	6.61	10.3	.1164E-02	-H 0.39	-27.584

15 MINULE AVERAGES: PARAMETERS

016.2	JA-1W degC	TVA-TVW deg):	₹ 2 ×	d/censk2	X111 -3	UB	ع يـ	70 70	II W/w**2	F 4×67
192/0225	4.19	4.59	96	050	.76	6.41	96.	. S178F-N3	-1 214	-19 462
192/0241	4.70	4.58	.0	46.9	5.	7.55	2 22	7177103	-3.214	
19270255	4.47	4 86	64	CLF II.	.71	3.85	6 3 =	. 111711111.5	2 B79	-11.1865
192/0310	69 6	61.5	÷.	\$ 11 E	7	4 45	5. 9.	.2460E-43	1.294	-1.8 7.54
19270325	4.74	5.1.5	9.1	. 031	.73	60 9	207 7	3169F-03	- 044	
19270340	4.77	5.1.3	90	. 0.34	.7.3	5 .50	20 3		605	
19270355	4 39	4.74	92	7.81.	.83	11.96	10.6	.1011F-112	-6 345	٠.
19278410	4.72	٦.	C.	3.065	.71	7 3.5	:	6766F-183	795 6-	-21 467
19270425	3.90	4.26	56	1176	. 79	3. ns	16.9	70.32E - 11.5	-7 723	
19270448	4.17	4.56	90	5.58	Ē.	=======================================	×	.900%E 0.5	5 P. 24 B	
1977/0455	3.73	4.00	96	690	. 718	7 54	24 7	.71545-113	-1.625	
1927.0510	2.78	3.85	66	. #96	₹.	14 BG	1 615-	93804E-63	155	-18 275
192/0525	2.97	3 27	66	F101.	. B.	4.4.	6.13	. 11116 E. (1.2)	-1.264	
192/05411	3.117	3.59	66	6.00	. 66	G N	-	. 5074E-04	8.082	•
19270555	3.61	4.00	66	590.	.77	BC /	43 6	.6674E-03	028	
192/4510		3.618	66	194	. 89		: /::	2008E-02	148	
192/0625	2.79	3.119	66	.132	60.		66.5	.1362F-02	-1.582	
192/0548	3.82	3. 438	*	1114	111		58.6	1075E-02	H54:1-	-22.665
19270655	3.31	3.67	*	900.	99.	2.25	:	63B4E-114	7,453	
1927.0710	3 68	4.08	66	.019	. 20	\$ 96	7	397.3E-0.5	4 163	-12 726
19270725		4.03	*	500.	.66	2.11		5594F-114	7.203	-2 0.35
192/0710	₹ ?	3.11	*	. 6.15	69.	3.46	· ·	1501-6-03	96 446	8:45 83 - *
19270755	25 2	2.79	*	. 1123	. 71	4 37	£	. 2554F-113	8.960	. 9. 161
155/0010	2.37	6.9	66	11611	6 9.		5 63-	93056-03	27,015	-15 773
192/10825	2.81	3.10	66	119	. H3	9.H7	FLS 6	1226E-112	11.176	1 -74.440
195/0841	2000 T	1.34	×	. #36	6/.	5 40	-1 E	3666-6-43	003 0	वाहर ५-
1927/1655	66.	4.83	*	. 093	E.	B 73	8 · 4	816-1-3556 T	7.347	-6.180
19271910	52.1	1.77	66	****	***	***	安安安全安安	传传并有等共传并将	李本本本本本本	安米洛洛洛 水母母子
192/0926	.76	77	*	*****	×××××	***	***	****	****	*****
1927/0941	. 21	72	*	****	长光光光头	老安小年茶等	安州河外州州	好得得得所其并所於	兴州共兴兴兴兴兴	举兴水水水水水水
192/1956	1.56	1.71	66	508	CH.	12.96	-86.6	21171-02	2.533	
1181/261	44		66	924	77	6.53	-4.7	29-14SH9.	6.584	-7.363
192/1826	1.62	1.77	<u></u>	.176	×:	10 15	. 24. G	12976-112	3.944	-11.086
195/1041	4 N	10. AB	*	22.2	06.	13.63	1.3.5. 5	. 23.39E -0.2	-1.775	-23.7116
192/11/56	. S	12. H.	*	119	M T	9 . BS	-9115.7	12275	660	-19.677
19271111	1 . 39	55.1	À 1	196	Ī.			78.38F - 0.3	669 5	-3.671
192/1126		1.64	66	. 113	B2		-17.0	1:54602	4 B.40	
19271141			66	.211	.09		4.35.4	21666-02	47.4	
19271156		3.41	6	.123	. B3		37.7	.1267E-02	-2.504	-23.73
192/1211	3.58	3.95	66	. 107	æ.		3.0%	. 11086-02	-3.717	-26.147
19271226	****	*	9	. 1165	.77		****	669%E-03	****	****
165/1541	3.55		\$	950.	97.	6.80	6 658-	. 5026E-03	074	-18 776
19271256	3.68	4.113	1.6	1194	00.	B 76	19 4	.9676E-113	-3 251	22 1815
192/1311	3.56		Š	860.	Ŧ.		€	.1016E-02	5. 002	-20.633
19271326	3.28	3.53	94	129	.63	43,29	67.8	1334E-02	-3.655	
192/1341	3.39	3.63	6.6	. 274	. G	14.97	31 3	2H24E-02	-10 020	
192/1356	3.83	4.13	6	. 432	66.	111.61	3.4.Q	4459F-112		-36 94.3
192/1411	.5. 48	3.72	5	.501	1.01	20.26	46.1	S170E-02	-16.095	-32 869

15 HINGE AVERABIS: PARABITERS

D of 5, 7,	MI-AI	10G-10W	Z	TAN	<u>(1:1</u>	#	-	117	I	Ŀ
	gbəp	geap	×	0/cm**2	X10-3	CM/Seed	ε	C.M	2448/3	C**W/3
76717661	1	3.41		300	7.6	17 85	2	36921-112	12 022	697. 8.6
19271441	202	3.38	3	311	6	5.63	1	30.021-02	1.66.6	
19271558			6.6	205	53	15.27	41.5	C)) - THE 65	-11.041	
192/1613	3.05	5.24	26	.376	1.6.	17.53	47.3	\$678F-62	-10 644	-21 743
19271628	3 18	3.30	6	.372	96.	17.44	43.1	. 30 136- 02	-11 526	-21.901
19271643	5.99	3 10	9.5	208	. 9.3	15 27	48.2	27.36E-82	-7 692	-10.719
19271658	3 85	3.85	65	274	. 92	14 97	37.6	26230-02	-7 9.50	-17.711
19271726	3.01	3.21	6	.244	16.	14 14	1.61	. 2518E-02	-6.769	-19.154
192/1741	****	***	*	****	****	****	女子女子子子	******	****	*****
192/1756	4.01	4.27	0.6	. 2.55	86.	1.3, :40	\$ 0 G	24226-02		-25, 240
192/1811	3.94	4 26	۲. خ	.061	1.1.	7.89	20 2	.6326E((3	-1.689	-16.674
19271926	3.02	4.12	7.3	. 052	.76	6.51	24.5	5.39.6E0.3	- 355	-14.696
192/1841	4.24	4.56	92	.054	.76	6.64	15.5	. 5540E0.3	-1 773	-16.228
192/1656	4.21	4.49	8.5	550.	.76	6.75	15.3	.5741E-03	690 1-	-1.3.779
192/1911	3.51	3.72	36	. 023	. 7.1	4.33	6.1	236 HE-03	3.913	750 7-
192/1926	3.50	3.72	9.1	620	.72	4 16	er . es	. 250 JF-0.3	3.741	-7.618
192/1941	3.62	3.94	9.5	.012	. 60	3 09	yr. }	1206E-03	5.686	-7.912
192/1956	3.38	3.60	973	416	. 7.0	2, 75	-1.3	1.094F-03	4.714	-7.057
192/2011	3.59	3.06	63	620.	.72	4.87	-3.7	.2983E-83	2.900	-10.241
1927/2026	3.56	3.82	0. 0.	. 072	.78	7.67	34.6	74096-03	1.22.1-	-1.4.952
19272841	3.83		60	900.	. 60	38 9	16.9	60526-03	-3.264	-3.5.79.3
192/2056	3.73	4.00	3	. 032	. 73	5 69	4.6-	. 3.26 (F - 8.3	2.214	-14.299
192/2111	3.58	3.89	3	. 627	.72	4 72	- 15 - 15	2H10F-03	3 147	-11.422
192/2/26	3.02	4.18	36	654	. 70	6.67	48.5	. 5517F-03	1.5.74	-17.963
192/2141	3.64		0 0	D . C	# X .	(C)	* (17876-03	3 978	-11.293
19772156	1 2	5 7 6	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	529	27.	4. 51	s :	2014F-83	3.500	
176/6611	0 0	9,79	* *	02.0		11.	<u>.</u> .	. 20005 .	V. 540	
176/6666	70.0	3.77	* 3	V6.0	4 00	n c	, , , , , , , , , , , , , , , , , , ,	. 377 BF - 0.3	1.765	751. 1157
109/0054	6 0 N		÷ >	270.	999		= M - C - C - C - C - C - C - C - C - C - C	01636-03	-	100
19272311	10 m		* *	1.47	e E	11 00		16966-40	12 100	191 - 72-
192/2326	3.27		66	371	96	17.44	9.10	. 5830E-82	681.51-	
19272341	3.59	3.97	66	. 171	. 86		21.7	1769E-02		
192/2356	3.29	3.64	66	. 320	.94	16.28	36 7	3306E-02	-10.050	-39.002
19379011	3.24	3.58	66	.203	. 93	15.22	3.55 3	2919E-82	-9.367	-35.941
193/0826	2.83		66	.116	. 02		6 98	1.20115-02		-21, 100
193/0441	2.76	. 6 . 6 . 6	6	.248	. 91	14.24	50.1	2555E-02		_
19.37.01(5.0)	7.69	7. 7.	2	797	. 86		60.7	1722E-02		
193/0111	1.08	1.17	<u>.</u>	.020	.71		7	.2491E-03		-3.129
195/0166	D t	N.	2 5	. 510	9.4		-42.6	. 5288E-02		0.53
175/0141	. 63	11.1	> 0	751.	. 84 10	3 6 5 6	16.3	1412F-82	1.8.968	3.47.5
103/03/1	14	77.	0	47.4	100	20.01	1 / 1	4469E-02		2 0077
193/0226	. 7	35	66	100	66		- 37a B	45464-42	1 739	-14 576
193/0241	1.22	1.34	66	430	66		321.0	4487E-62	1.910	
19.3/8256	. 52	. 57	66	. 291	.63	15.41	-43.0	2991E-02	7 820	
193/0311	.74	.82	66	.333	.95	16.50	1.89-	.3429F-82	6.000	-8.308
193/0326	. 96	1.06	*	307	. 94	15.86	-77.5	. 31.60E-112	4 851	-11.253

15 MINDLE AUPPAGES: PARABETERS

10.0000 10.0000 10.0000 10.0000 10.0000 10.0000 10.00000 10.00000 10.00000 10.00000 10.00000 10.00000 10.00000 10.00000 10.00000 10.00000 10.00000 10.000000 10.000000 10.00000 10.00000 10.000000 10.000000 10.000000 10.00000 10.000000 10.000000 10.00000000 10.00000000 10			;		;	i	Į:		i	:	
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2.75 3.16 3.44 3.64 3.16 3.16 3.83 (19-10) 3	19370341	2.29	2.54	*	158	6.4	14 34	1050	. 2594E-02		-25.306
2. 0.2 3. 5. 12 8.8 3.5.4 9.5 15. 75 8.5 3.5.0 -9.5	19.3711356	2.75		*	3:46		11 10	30	. 155.56F - (1.2)	. 5.30.5	
3.2.2. 3.4.0 3.4.0 10.5.10 10.5.10 10.5.2 3.4000-102 -11.0.443	193/0411	2.03		*	.343	5.6	16 76	5 4 5	35,3(11 (1.2)	-11.247	3% 2.39
3.5 3.70 82 3.76 1.6 3.5 3.6 3.6 4.6 <td>19370426</td> <td>3 22</td> <td></td> <td>*</td> <td>240</td> <td></td> <td></td> <td>33.6</td> <td>. 29 Oak - 4.2</td> <td></td> <td></td>	19370426	3 22		*	240			33.6	. 29 Oak - 4.2		
3.75 4, 17 44, 17 <td>19.3/0441</td> <td>3.33</td> <td>3 70</td> <td>*</td> <td>326</td> <td>56.</td> <td></td> <td>\$6. 2</td> <td></td> <td></td> <td></td>	19.3/0441	3.33	3 70	*	326	56.		\$6. 2			
3.50 4.51 4.85 9.2 15.10 76.6 6.25371-602 -14.8 3.70 -4.81 48.8 2.93 -9.5 15.11 76.6 6.25371-602 -14.8 3.84 -4.82 <td< td=""><td>193/0456</td><td>3.75</td><td>4.17</td><td>*</td><td>G227</td><td>670</td><td>(3 69</td><td>1</td><td>. 236.16-02</td><td></td><td></td></td<>	193/0456	3.75	4.17	*	G227	670	(3 69	1	. 236.16-02		
3 59 3.96 4.84 255 59 1.44 7 56 7 1.68 3.87 4.10 88 255 59 1.44 7 1.69 4.10 88 3.52 59 1.65 3.84 4.45 4.87 4.87 1.61 1.75 1.00 4.45 4.87 4.60 4.47 4.62 4.87 4.60 4.60 4.72 4.60 4.60 4.72 4.60	19370511	3.70	4.11	*	578	. 92		900	26716-02		-
3 6 9	1937.0526	3.50	3.98	*	253.	õ	14.47	b 9.:	.2637F · (C)		
3.9.7 4.10 8.8 4.362 1.95 1.6 3.4 4.440 1.10 8.8 4.37 1.6 3.1 4.4 <	193/0541	3.65	4.06	*	29.3	. 93	15.55	F. 35.			
3.97 4.42 *** .447 1.00 19.37 3.4 6.7791-6.2 -10.045	193/0556	3.69	4.10	*	.332	5.5	آ ا ا	54.4	. 54.5% F - 47.	-13.065	-40 542
4. 04 4. 44 8. 8 3.37 97 17. 02 9. 4. 04 4. 04 4. 04 4. 04 4. 44 4. 44 4. 44 4. 44 8. 8 3.37 97 17. 02 9. 7 17. 02 9. 7 17. 02 9. 7 17. 02 9. 7 17. 02 9. 7 18. 02 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 9. 7 <t< td=""><td>19370611</td><td>3.97</td><td>4.42</td><td>*</td><td>457</td><td>1.00</td><td></td><td>34 6</td><td>477915-62</td><td>19.677</td><td>-57.439</td></t<>	19370611	3.97	4.42	*	457	1.00		34 6	477915-62	19.677	-57.439
3 R2 4 24 *** 232 .84 .242 *** .242 .99 13 11 .293 .13 13 .242 .99 .14 10 .28 5 2 3 2 3 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3	193/0626	4.64	4 49	*	5117	16.	17 82	4 40	40028-02		154 764
3.84 4.27 *** 242 90 14.00 22.2496949 -11.594 -40	19370641	3.62	4.24	*	212	60.	17 19	21.0	.2193F-02	-10.276	19 941
4.53 5.05 *** 301 93 45.74 38.9 Fe-02 -10.875 -66 4.66 5.24 *** 343 95 16.86 21.9 35.9 Fe-02 -6.1 4.66 5.24 -6.1 4.66 5.24 4.66 5.24 3.57 95 16.86 2.97 9.7 16.86 -6.1 4.66 -6.1 3.67 -6.1 -6.1 4.66 -6.1	19370656	5.84		*	. 242	06.	14.00	5 22	. 249tar. 112		
4, 59 5, 43 3, 34 3, 95 16, 86 21, 9 3, 3, 16, 86 -6, 10, 497 -6, 10, 405 <t< td=""><td>193/0711</td><td>4.53</td><td>5.05</td><td>*</td><td>.301</td><td>. 93</td><td>15 74</td><td>20 0</td><td>31216-02</td><td>-10.272</td><td>-56 364</td></t<>	193/0711	4.53	5.05	*	.301	. 93	15 74	20 0	31216-02	-10.272	-56 364
4.66 5.24 *** 343 95 16.80 23.35524-02 -60.05 16.91 *** 36.0 *** 36.7574-02 -60.05 *** 16.80 -65.3 16.30 *** 20.0 *** 20.0 *** 20.0 *** 20.0 *** 20.0 *** 20.0 *** 20.0 *** 20.0 *** 20.0 *** 20.0 *** 20.0 *** 20.0 *** 4.0 *** 20.0 *** 20.0 *** 4.0 *** 20.0 *** 20.0 *** 4.0	19370726	4.59		*	.345	. ¢.7	16 86	21.9	. 35,81E-02	-30.476	
4. 17 4. 64 *** 264 *** 264 ** 264 ** 264 ** 264 ** 264 ** 264 ** 264 ** 264 ** 264 ** ** 4.0 ** </td <td>19370741</td> <td>4.66</td> <td>5.24</td> <td>*</td> <td>343</td> <td>.95</td> <td></td> <td>21.3</td> <td>3552F-02</td> <td>-20 BS0</td> <td></td>	19370741	4.66	5.24	*	343	.95		21.3	3552F-02	-20 BS0	
3.92 4.40 *** 204 .92 15.70 2.12 29909-0-02 -13.50 -10 21.5 2.09 -13.50 -10 -13.5	193/0756	4.17		*	208	. 9.3		a	28-13-14.	-15.485	635 54-
3.84 4.31 34 4.31 34 4.31 34 4.31 34 4.39 193 15 17 24 9.3096-02 14.02 16.00 14.02 16.00 1	193/0811	3.92	4.40	*	.201	.92		21.5	2909F-02	-13.509	
4.02 4.53 8.4 299 .93 15.67 29.9 .14.907 -14.907 3.54 4.02 8.4 -299 .93 11.94 -14.907 -14.907 3.54 4.09 8.4 -39 11.94 -14.907 -14.907 3.52 3.99 4.42 8.8 -447 .99 14.16 -14.407 -14.407 3.79 4.24 8.8 -581 1.04 21.64 -14.63 -14.13 -14.13 4.24 8.8 -581 1.02 21.64 -14.63 -14.1	193/0026	.5. 114	1.31	*	.200	. 92	15 17	7.5	25000E-02	-13.118	
3.64 4.09 *** 436 .99 18.96 38.4 4.070 -16.686 -10.289 -60 3.52 3.96 *** .546 1.03 27.17 40.6 -10.1289 -60 3.94 4.24 ** .546 1.06 23.31 46.8 .6009E-02 -21.359 -61 3.94 4.54 ** .564 1.05 25.0 1.02 27.2 -71 4.04 4.54 ** .564 1.07 28.6 .6009E-02 -21.359 -71 4.24 ** .564 1.02 25.0 .65.9 .5867E-02 -71 -71 4.24 ** .564 1.02 28.0 .66.9 .7877E-02 -73 -71 -73 3.63 ** .593 1.07 28.6 .78.9 .7877E-02 -14.064 -78 -78 -78 -78 -78 -78 -78 -78 -78 -78 -78 </td <td>193/0641</td> <td>4.02</td> <td>4.53</td> <td>*</td> <td>662</td> <td>. 93</td> <td></td> <td>e.</td> <td>36954-62</td> <td>-14.907</td> <td>81 1, 1 1, -</td>	193/0641	4.02	4.53	*	662	. 93		e.	36954-62	-14.907	81 1, 1 1, -
3.52 3.96 8.8 5.46 1.03 21.17 40.6 5.64eee 62 -11.1259 -61 3.79 4.42 8.8 5.64 1.06 23.31 46.96 -19.1259 -61 3.79 4.24 8.8 5.64 1.06 23.31 46.9 -19.166 -71 -61 -71 -71 4.24 8.8 5.64 1.03 27.65 3.7 9.61396-02 -71.345 -71 4.24 8.8 5.64 1.03 27.65 3.7 9.61341-02 -7.5 52.7 -71 -71 -71 -71 -71 -71 -71 -71 -71 -71 -72 -71 -71 -72 -73 -73 -74 -72 -73 -74 -73 -73 -74 -73 -74 -73 -74 -74 -74 -75 -74 -74 -75 -74 -75 -74 -75 -74 -74 -74 -74 </td <td>19370856</td> <td>3.64</td> <td>4.0%</td> <td>*</td> <td>4.30</td> <td>66</td> <td></td> <td>48.4</td> <td>4.0001-112</td> <td></td> <td></td>	19370856	3.64	4.0%	*	4.30	66		48.4	4.0001-112		
3.94 4.42 *** 447 99 19,16 54,4 46,975-92 -19,153 -64 4.24 *** .564 1.04 21,66 45,16 60,975-92 -24,56 -73 4.24 *** .564 1.02 21,59 51,22 .54886-02 -75,37 -73 3.33 3.75 *** .564 1.02 23,69 56,9 -7486-02 -74 -73 3.63 3.75 *** .522 1.02 23,69 57,9 57496-02 -76,47 -73 2.90 3.61 *** .693 1.02 23,69 57,5 77476-02 -76,47 -57 3.40 *** .693 1.02 23,73 .60,9 77476-02 -76,47 -53 3.40 *** .694 1.07 23,46 .77 -74,476-02 -76,47 -57 3.40 *** .67 1.07 23,46 .77 -74,61 -76	193/0911	3.52	3.96	*	.546	1.03	21.17	411 6	Scatch - 02		
3.79 4.24 8.8 581 4.146 71.06 45.14 661 75.55 -64 4.24 8.8 561 1.05 23.31 46.9 661.9 -7.35 -7.5 -7.7 4.24 8.8 561 1.02 20.59 3.6 3.7 -7.1 -7.7 <td>19.37.1926</td> <td>3.94</td> <td>4.4</td> <td>*</td> <td>447</td> <td>66</td> <td>176</td> <td>٠ ٠ ٠</td> <td>. 4627F - 92</td> <td></td> <td></td>	19.37.1926	3.94	4.4	*	447	66	176	٠ ٠ ٠	. 4627F - 92		
4 4.51 ***	19.370941	5.79	4.24	*	. Se.	7 · 0 ·	71.66	45. 3	. 6.0 5 9F - 0.7		
3.3 3.75 *** 5524 1.02 20.68 51.2 5304041-02 -74.70 3.6 3.8 *** 5522 1.02 23.62 55.62 -16.467 -57 3.63 3.40 3.8 ** .693 1.07 23.62 76.8 -16.467 -57 3.40 3.6 ** .694 1.07 23.85 75.7 70954-02 -16.467 -57 3.40 3.6 ** .694 1.07 23.85 75.7 70954-02 -16.467 -57 3.40 3.6 ** .694 1.07 23.85 75.5 70954-02 -16.467 -57 3.5 4.6 4.07 7.7 23.86 7.7 70954-02 -16.467 -57 3.6 4.6 4.07 7.7 7.0 7.0 70.7	195/11956	£ 0 €	4. 1.1.	* :	.661	0.00		46.83	20-27197		
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2.99 3.46 3.4 4.4 7.0 </td <td>102/10/0</td> <td>4 67</td> <td>5.7.5 A0.5</td> <td>÷ ></td> <td>2000</td> <td>30.1</td> <td></td> <td>0</td> <td>5.5680.102</td> <td>1 4 0 6 4</td> <td></td>	102/10/0	4 67	5.7.5 A0.5	÷ >	2000	30.1		0	5.5680.102	1 4 0 6 4	
3.40 3.41 3.42 3.44 <td< td=""><td>75037201</td><td></td><td></td><td>÷ •</td><td>2.07</td><td>2.0</td><td></td><td>1.00</td><td>300 37 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6</td><td>14.00.4</td><td>7.70</td></td<>	75037201			÷ •	2.07	2.0		1.00	300 37 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	14.00.4	7.70
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3.26 3.52 *** .575 1.04 21.21 57.5 .593(E-02 -15.673 -59. 3.15 3.38 ** .625 1.05 22.63 .60.7 .6451E-02 -15.805 -50 2.46 2.40 ** ********** ********* ******** ******** ******* ******* ****** ****** ****** ***** ***** **** **** **** **** **** **** **** **** **** **** **** **** **** **** **** **** **** **** *** <t< td=""><td>103/1126</td><td>. 4.</td><td></td><td>÷ 4</td><td>464</td><td>1 02</td><td></td><td>S L</td><td>50 - 36.6.1.C.</td><td></td><td>012 59-</td></t<>	103/1126	. 4.		÷ 4	464	1 02		S L	50 - 36.6.1.C.		012 59-
3.15 3.38 ** .625 1.05 22.63 .60.7 .6451E-02 -15.805 -50.0 2.46 2.40 ** ********* ******* ****** ****** ****** ***** ***** ****** ***** ***** ***** ***** ***** ***** ***** ***** ***** ***** **** **** **** **** **** **** **** *** <td< td=""><td>193/1141</td><td>70. 1</td><td></td><td>- 14</td><td>5.75</td><td>1 0.4</td><td></td><td>50 60</td><td>CO Z6E-03</td><td>-14 473</td><td></td></td<>	193/1141	70. 1		- 14	5.75	1 0.4		50 60	CO Z6E-03	-14 473	
2. 46 2. 40 *** ******* ***** ***** ***** ****** ****	193/1156	3.15	3.38	×	625	 	100 A	2 09	6451F-02	1 × 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0 ×	-41 184
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4.11 4.60 ** 981 1.14 70.39 66.0 1016E-01 -52.454 -664. 4.37 4.90 ** 1.009 1.16 22.94 67.5 1432E-01 -37.192 -99. 4.14 4.64 ** 1.009 1.12 26.99 59.2 9429E-01 -37.192 -99. 3.99 4.54 ** .720 1.10 25.59 59.3 18246E-02 -26.207 -07. 3.65 4.43 ** .765 1.10 25.59 59.3 18246E-02 -26.207 -90. 4.11 4.66 ** .751 1.10 26.06 5.4 1856E-02 -20.27 -90. 4.57 6.23 ** .219 .89 13.46 14.2 2294E-02 -20.451 -62. 5.64 6.30 ** .230 .90 13.79 36.5 1856E-02 -21.466 -63.	19.575241	3.65	4 30	*	159.	1.06		49.3	677.91-02	-73.455	0.70 199
4.37 4.90 *** 1.009 1.16 29.94 67.5 15129E-01 -37.192 -99 4.14 4.54 ** 1.009 1.12 26.99 59.2 9129E-02 -31.059 -104 3.99 4.54 ** 1.720 1.08 24.32 53.4 1252E-02 -26.207 -67.2 3.99 4.54 ** 1.720 1.10 25.59 59.3 18246E-02 -26.207 -90 4.11 4.66 ** 1.720 1.10 25.40 53.4 127E-02 -21.270 -90 4.32 4.07 ** 1.02 25.40 53.4 1826E-112 -31.609 -90 4.57 5.25 ** 7794E-02 -31.609 -92 5.57 6.23 ** 1.20 26.46 11.2 12914E-02 -31.466 -63 5.64 6.30 ** 230 90 13.79 46.5 120.431 -63.4 4.66 5.18 99 1805 1.10 25.77 46.5 1256E-02 -34.413 -193	19.371256	4.11	4.60	*	. 981	1.14		66.0	10166-01		-60.043
4.14 4.64 ** 1806 1.12 26.59 59.2 912%=02 31.059 -104.33.99 4.54 ** 1720 1.08 24.32 53.4 1245E=02 -26.207 -67.23.99 4.54 ** 1.720 1.08 24.32 53.4 1245E=02 -26.207 -67.23.45 4.45 ** 1.700 25.40 53.4 106.25F=02 -27.270 -90.43.4 5.2 4.67 ** 1.700 25.40 53.4 105.2F=02 -31.609 -90.43.4 5.2 5.2 6.23 ** 1.200 25.40 14.12 12.09.6=02 -31.609 -92.25.54 6.30 ** 1.200 13.40 14.12 12.09.45 -6.2 5.64 6.30 ** 1.200 13.7 56.5 14.4 12.2594E=02 -21.466 -63.4 14.6 5.18 99 13.4 12.27 56.5 11.565E=02 -34.413 -193.	19371311	4.37	4.90	*	1.009	1.16		67.5	. 53.29E-01		-49 544
3.99 4.54 ** .720 1.08 24.32 55.4 7452E=02 -26.207 -407. 3.45 4.43 ** .797 1.10 25.59 59.3 H24EE=02 -26.457 -99. 4.11 4.66 ** .765 1.09 25.40 53.4 .0127E=020.72.0 -90. 4.52 4.07 ** .826 1.10 26.46 53.4 .0556E=42 -31.609 -92. 4.67 5.25 ** .219 1.09 24.48 13.3 7794E=033.29H -92. 5.54 6.30 ** .230 .90 13.7 794E=020.451 -63. 5.64 6.30 ** .230 .90 13.7 36.5 .1366 -63.	173/1326	4.14	4.64	*	908	1.12		5,7 %	. 912ta - 02		-114,595
3.85 4.43 ** .797 1.10 25 59 59 3 48246E-02 26 437 -95. 4.11 4.66 ** .765 1.09 25 40 53.4 .0127E-02 -20.270 -90 4.32 4.07 ** .086 1.10 26.46 52 4 .0556E-82 -31.607 -92 4.57 5.25 ** .751 1.09 24.48 52 4 .0556E-82 -31.270 -92 5.57 6.23 ** .219 .09 13.46 11.1 .2204E-02 -20.431 -62 5.64 6.30 ** .230 .90 13.7 .414 .2394E-02 -20.445 -63.445	193/1341	3.99	4.54	* *	.720	1.08		6.5.4	. 7452£ ~02		67.399
4.11 4.66 ** .705 1.09 25.48 53.4 .0127F-02 -28.270 -90 4.32 4.87 ** .86 1.10 26.46 52.4 .8556F-82 -31.609 -92.4 4.67 5.25 ** .751 1.09 24.08 43.3 .7790F-02 -33.228 -92.55.2 6.23 ** .219 .89 13.46 14.2 .2284x6-02 -20.451 -62.55.24 6.30 ** .230 .90 13.79 14.4 .2394E-02 -21.466 -63.4 4.66 5.18 99 .805 1.10 25.77 46.5 .1356x6-02 -34.413 -89.	193/13%6	3.115	4.43	*	.797	1.10		50 W	. B246F-02		-55, 106
4.32 4.07 ** .026 1.10 26.46 5.3 7796F-R2 -31.607 -92. 4.67 5.25 ** .751 1.09 24.08 43.3 7796F-02 -33.278 -92. 5.57 6.23 ** .219 .09 13.46 14.2 22045-02 -20.431 -62. 5.64 6.30 ** .230 .90 13.79 13.4 2394E-02 -21.466 -63. 4.66 5.18 99 .055 1.10 25.77 36.5 11365E-02 -34.413 -193.	19371411	1.1	-	*	. 705	2 · 0 ·		53.4	.01275-02		B''? 06-
4.67 5.25 ** .751 1.09 24.08 43.3 77965-02 -33.228 -92. 5.57 6.23 ** .219 .89 13.46 14.2 2285-02 -20.431 -62. 5.64 6.30 ** .230 .90 13.79 13.4 23948-02 -21.466 -63. 4.66 5.18 99 .805 1.10 25.77 36.5 113658-02 -34.413 -193	193/1126	4.32		*	930	1.10	26.46	4 33	. H556F-42		-9.1 1.55
5.57 6.53 ** .219 .89 1.3.46 11.12 .2283.56-0.2 -20.451 -6.2. 5.64 6.30 ** .230 .90 13.79 13.4 .23948-02 -21.466 -6.5. 4.66 5.18 99 .805 1.10 25.77 36.5 .13555-02 -34.413 -193	193/1441	4.67		*	.751	1.09		43.3	77964 - 02	-	-93 HS6
5.64 6.30 ** .230 .70 33.79 33.4 .2394E-02 -23.466 -63. 4.66 5.10 99 .805 1.10 25.77 36.5 .1365E-02 -34.413 -193	173/1956	5.57		*	.219	68.			. 22 H.46 - 0.2		-62.070
4.66 5.18 29 .805 1.10 25.27 46.5 .11362E=02 -34.413 -103	193/1511	5.64	6.30	*	.230	06		11 4	2:394f -02		
	193/1632	4.66	5.18	66	. 805	1.10		36.5	. 11:36%F(12)		

15 MINUTE AUFRAGES. PARAMETERS

CERTAL MATERIAL CONTRACTOR CONTRACTOR AND CONTRACTOR OF THE CONTRA

9.5.7.16.47 6.75 7.34 0.7 6.79 7.34 0.7 6.79 7.34 0.7 7.34 0.7 7.34 0.7 7.40 0.7	2 319	Joep deag	Joan Joan	8 ×	100	C0 X58-3	U\$ (8/1)	ع نـ	Z.8 C.M	C	# m/m*#?
7 34 7 44 7 44 7 44 7 44 7 44 4 44444 2 450416 2 44444 7 49 7 40 7 5 7 40 7 5 7 60416 2 44444 7 49 7 7 7 9 100 2 60 2 7 7 7 2 60416 2 7 7 40 7 7 7 8 2 7 7 10 2 60416 2 7	193/1647		1	9.5	672	50.4	27. 24	5.00	. 65.12802	411 (145	-76.301
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7. 45 7. 94 7. 45 7. 94 7. 45 7. 94 7. 45 7. 94 7. 45 7. 94 7. 47 7. 47 7. 47 7. 47 7. 47 7. 47 7. 7<	19.37.1827.	7.49		90	506	. 9.3		6	. 500000-02	-36.245	
7, 64 6, 13 84 255 92 14 60 44, 5 20,127-612 -44 7, 84 6, 54 66 92 14 46 7 20,127-612 -44 7, 84 6, 58 6, 98 95 14 6 7 7 25,624-62 -45 7, 44 14, 12 7 7 14 4 7 7 25,624-62 -45 7, 44 14, 12 7 7 14 4 7 7 14 5 -45	19371651	7.4%	3	29	785	. 8 8		is S	.1973E-(P		
8.43 9.43 9.43 9.44 9.70 14.41 7.9 200 cell 276 9.8 14.51 7.9 200 cell 27.6 4.6 4.5 4.6 4.6 4.6 4.6 4.8 9.8 14.6 4.7 4.6 <td>193/1941</td> <td>7.60</td> <td>-</td> <td>Ŧ</td> <td>959</td> <td>200</td> <td></td> <td>ۍ ۲</td> <td>.2717E-82</td> <td></td> <td>-54.923</td>	193/1941	7.60	-	Ŧ	959	200		ۍ ۲	.2717E-82		-54.923
7.88 9.46 66 254 91 14 43 7 9 86.44-02 -45 7.48 6.54 6.98 92 16.47 14 1 33.44-02 -45 7.40 6.74 6.94 92 218 97 16.47 33.44-02 -45 4.45 6.94 6.94 4.67 16.47 34.48-02 -45 4.46 4.95 95 16.47 34.48-02 -27 4.76 4.95 95 16.72 24.53 -41.77 4.77 4.96 95 16.72 24.53 -41.77 4.77 4.76 16.72 24.76 -42.76 -47.76 4.78 4.76 16.77 4.76 4.76 -17.76 4.77 4.76 16.77 4.76 4.77 -17.76 4.77 4.76 4.77 4.77 4.77 4.77 -17.76 4.77 4.77 4.77 4.	193/2841	H. 43	٠,	64	.276	.92		5 /	.2502E~(2		-70 504
7, 01 0.52 0.00 33.3 95 16, 67 14, 14 3.349E=02 -0.45 6, 34 6, 34 99 14, 14 14, 14 3.349E=02 -0.45 6, 34 6, 99 210 99 14, 14 3.349E=02 -0.45 4, 46 6, 99 3.66 95 16, 72 94 3.341E=02 -0.45 4, 46 4, 95 96 40.9 16, 47 97 16, 67 -0.75 4, 27 4, 67 95 40.9 16, 47 97 16, 67 -0.45 4, 28 96 40.9 96 40.9 16, 77 -0.45 -0.45 3, 41 4, 97 96 40.9 16, 77 97 -0.46 -0.26 -0.26 -0.26 -0.26 -0.26 -0.26 -0.26 -0.27 -0.16 -0.26 -0.26 -0.26 -0.26 -0.26 -0.26 -0.26 -0.26 -0.26 -0.26 -0.26 -0.26 -0.	193/21117	7.80	9.46	25	.251	3	14 45	6 %	. 26235-02	-35, 372	63.254
7. 444 94.24 94.0 94.0 14.1 94.1 94.1 94.0 14.1 94.1 94.1 94.0 94.0 14.1 94.1 14.1 94.0 94.0 14.1 94.0 14.1 94.0 14.0 94.0 14.1 94.0 14.0 94.0 14.0 94.0 14.0 94.0 14.0 94.0 14.0 94.0 14.0 94.0 14.0 94.0 14.0 94.0 14.0 14.0 94.0 14.0 14.0 14.0 94.0 14.0 14.0 94.0 14.0 14.0 94.0 14.0	193/2143	7.01	H.52	90	333	.95		111 4	.3492E-02		
6. 34 6. 99 92 219 69 13.4 6. 99 92 10 69 10	19.3721511	7.48	1.20	86	. 4.50	66.		1.4.	. 45 LEE-42		Τ.
5. 49 6. 05 9.5 3.25 9.5 16 46 16. 3 39.18E-02 -27. 4. 46 4. 75 9.5 16. 9 2. 6 336.18E-02 -27. 4. 46 4. 9.5 9.5 16. 9 2. 6 336.18E-02 -17. 4. 46 4. 6. 7 9.5 3. 6 9.6 4. 6. 7 -14. -17. 3. 52 3. 9. 3 9.6 -457 1. (14) 19. 57 4. 6. 6 336.18E-02 -17. 3. 63 4. 6. 7 9. 6 -487 1. (14) 19. 6 4. 2. 9 -14. 3. 63 4. 6. 7 9. 7 1. (14) 19. 6 4. 6 1. 6. 6 -14. 6 1. 18. 1. 18. -14.	193/2213		66.99	6.6	9119	.09		6	.2189E-02		-57.341
4.27 4.71 94 336 95 16.72 24.5 33.516-02 -17.4 4.66 4.66 95 36.9 96 47.0 4.20 -21.0 <t< td=""><td>193/2220</td><td>5 49</td><td>80.9</td><td>5.6</td><td>325</td><td>56</td><td></td><td>16.3</td><td>.341.3F-02</td><td>-25.616</td><td>-61.163</td></t<>	193/2220	5 49	80.9	5.6	325	56		16.3	.341.3F-02	-25.616	-61.163
4, 4, 6 4, 6	19372243	4.27	4.75	46	336	56		24.5	.3521E-02	-17.058	40.635
4.28 4.67 95 359 96 47.28 26.6 35.41 -4.04	193/2298	4.46	4.95	5.5	906	. 98		3 /S	424G:E-02		
4 19 4 67 9 6 4 87 9 0 14 41 29 6 4 67 4 67 4 67 4 67 4 67 4 67 4 67 4 67 4 67 4 67 4 68 4 67 4 68 4 67 4 68 4 67 4 68 4 7 8 4 68 4 68 4 68 4 68 <td< td=""><td>19372313</td><td>4.28</td><td>4.67</td><td>68</td><td>358</td><td>36</td><td>-</td><td>26 6</td><td>.3761E-02</td><td></td><td>-63.31.</td></td<>	19372313	4.28	4.67	68	358	36	-	26 6	.3761E-02		-63.31.
3.52 3.93 96 457 1.00 19 16.00 15.825-612 -14 3.52 3.93 96 145 10 99 16.00 15.825-612 -1 4 3.63 4 14.32 -14.02 -1 4 3.63 4 14.4 4.99 -3.69 -3.69 16.00 -3.32 -3.40 -3.69 17.95 36.1 -3.40 -4.69 -3.69 -3.69 -4.69 -3.69 -4.69 -3.69 -4.69 -3.69 -4.69 -3.69 -4.69 -3.69 -4.69	193/2324	4 19	4.67	96	447	06		29.6	. 42:70F-02	_	-57 900
3. 94 4. 39 97 1445 145 14 1.522E-162 -7 2. 25 3. 67 97 1024 27 4 16.44 1522E-162 -7 2. 14 2. 37 94 14 40 55 5 4446E-02 -8 3. 63 4. 14 99 346 97 17.96 36.35 4446E-02 -8 4. 65 5. 27 99 304 94 16.44 55.5 6464E-02 -8 2. 76 3. 6 5. 7 3. 6 36.5 6464E-02 -8 2. 76 3. 6 5. 7 3. 6 46.6 7. 7 46.6 -8.5 6464E-02 -9 4. 70 5. 7 3. 6 47.5 47.4 47.4 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 -8.7 <	19372343	3.52	3.93	96	.457	1. ((1)		43.3	. 4801F-02		780 65-
3. 25 3. 67 97 02.0 71 4 0.0 -5. 4 25.02E-03 4 -4.2 98 14.57 13.5. 43.6E-03 -4.4 -4.5 3.6.5 43.6E-02 -4.4 -4.65 -5.2 40.0 97 14.6 97 3.6 9 -4.0 99 14.6 95 3.6 9 -4.0 -7.1 -4.6 -5.5 44.6E-02 -7.4 -7.9 -7.4 -4.0 -7.4 -4.0 -7.4 -4.0 -7.4 -7.9 -7.2 -7.4 -7.9 -7.2 -7.7 <td< td=""><td>193/2350</td><td>3,91</td><td>4.39</td><td>6.6</td><td>145</td><td>SH.</td><td></td><td>16.11</td><td>. 1522E-12</td><td></td><td>-37,104</td></td<>	193/2350	3,91	4.39	6.6	145	SH.		16.11	. 1522E-12		-37,104
2.18 2.37 98 -412 98 18.57 18.65 4.14 99 -346 97 17.98 36.5 4.16.87-62 -4.4 3.63 4.14 99 -346 97 17.98 36.5 4.46846-62 -2.3 4.49 5.16 99 -308 94 16.04 55.0 32486-62 -2.3 2.76 3.16 99 -309 94 16.04 55.0 34.6866-02 -2.7 3.34 3.83 8.3 8.3 8.3 40.686-02 -2.7 5.74 1.99 99 -299 99 18.6 16.0 -2.3 40.666-02 -2.7 3.34 3.83 8.3 8.3 40.666-02 -2.7 -2.8 -2.8 -2.8 -6.6466-02 -2.7 4.6 6.40 8.7 4.20 99 18.7 40.0 -2.8 6.8646-02 -2.3 5.4 4.6 1.0 1.0 1.0 <td>194/0113</td> <td>3.25</td> <td>3.67</td> <td>1.6</td> <td>.020</td> <td>.71</td> <td></td> <td>4.6-</td> <td>.25 02E-03</td> <td>4.764</td> <td></td>	194/0113	3.25	3.67	1.6	.020	.71		4.6-	.25 02E-03	4.764	
3.63 4.14 99 .386 .97 17.95 36.1 40637-02 -14 4.65 5.27 99 .409 .94 14.49 55.5 .4416-02 -23 4.79 5.14 99 .577 14.4 21.5 5.6 .66 -27 .23 2.76 5.16 99 .299 .299 .294 15.87 .66 .67<	55.00/661		2.37	96	.412	96		1.3.8.2	4344E-112	-4.492	
4.65 5.27 99 409 96 10 40 55 4.4111E-02 -23 4.76 5.31 99 57 1.64 81.95 56.5 6.0864E-02 -7 2.76 3.16 99 299 94 15.87 16.08 -7 2.76 3.16 99 299 94 15.87 46012 -7 2.79 2.79 2.79 99 19.64 16.15 3.15 -7 3.34 3.43 3.43 3.94 90 18.15 42.34 -7 15.87 -7 15.75 -7 15.75 -7 15.75 -7	194/0050	3.63	4.14	66	.386	1.6		36.1	. 44635-42	-14.998	-59 Pec
4.49 5.41 99 .572 1.84 21.95 36.5 6.656E-02 -27 2.76 3.46 99 .308 94 16.04 55.0 329E-02 -7 2.78 3.46 99 .329 94 15.82 4608 -7 2.79 3.94 .90 16.14 5.86 40.04 -6.15 -7 3.34 3.83 *** .329 .90 18.70 -6.15	194/6105	4.65	5.27	66	409	. 9 H		25.5	4.51(1)E-02		75.120
2.76 3.16 99 308 94 16 04 55.0 3242E-02 -7 2.79 2.99 324 17.84 16.04 53.151E-02 -5 2.79 2.79 99 18.78 16.04 5.16E-02 -5 3.34 3.4 3.8 324 90 18.78 40.3 40.54E-02 -5 3.34 4.02 48 7.0 18.7 40.0 40.0 -40.0 -40.0 -6 6.11 6.16 6.16 8.8 42.0 18.7 40.0 -40.0 <td< td=""><td>194/0120</td><td>4.49</td><td>5.11</td><td>6.5</td><td>.577</td><td>3.84</td><td></td><td>36.5</td><td>.6466F-42</td><td></td><td> (15. 45R</td></td<>	194/0120	4.49	5.11	6.5	.577	3.84		36.5	.6466F-42		(15. 45R
1, 74 1, 99 99 299 15, 16 15, 160 5 315,15-02 -5 2, 29 2, 29 321 97 15, 16 15 40 40 40 -5 -4 -4 -6	194/0135	2.76	3.16	66	308	66.		55.0	.324SE-02		-42,231
2. 29 .324 .97 17 54 50.45 -5.99 -5.43 -5.94 -6.41 -6.42 -6.42 -6.42 -6.42 -6.42 -6.43 -4.1546-62 -13. -6.43 -4.1546-62 -13. -6.46 -6.47 -6.46 -6.47 -6.46 -6.47 -6.46 -6.47	194/0150	1.74	1.99	66	299	66.		1608.5	3151E-02		-26.276
3.34 3.43 *** 394 90 46.45 42.3 41516-62 -153 5.54 4.02 *** 680 199 16.76 10 0 44056-02 -155 6.11 6.87 *** 680 1.00 26.05 33.9 68546-02 -155 6.16 6.80 *** 692 1.00 26.05 33.9 68546-02 -41 5.51 6.19 *** 692 1.07 23.93 52.5 72156-02 -31 5.51 6.19 *** 692 1.07 23.93 52.5 72156-02 -31 5.54 6.31 *** 564 1.04 22.01 26.9 61026-02 -31 5.54 6.51 *** 371 97 12.07 16.76 12.02 6.75 7.60 *** 371 97 16.00 1.0 9 5266-02 -35 6.75 7.61 *** 492 1.01 20.14 20.6 51116-02 -35 6.76 6.11 *** 688 *** 492 1.02 20.14 20.6 51116-02 -36 6.77 7.62 99 7.74 1.08 24.71 2.01 16.66-01 -55 6.78 6.47 7.72 8.72 99 7.73 1.03 24.71 2.01 16.66-01 -55 6.78 6.47 7.72 8.72 99 7.73 1.03 24.71 2.01 16.4 41276-02 -34 6.78 7.72 8.72 99 7.73 1.03 24.71 2.01 16.4 41276-02 -34 6.78 7.72 8.72 99 7.73 1.03 24.71 2.01 16.4 41276-02 -34 6.78 7.72 8.72 99 7.73 1.03 24.71 2.01 16.4 41276-02 -34 6.78 7.72 8.72 99 7.73 1.03 24.71 2.01 16.4 41276-02 -34 6.78 7.72 8.72 99 7.73 1.03 24.71 2.01 16.4 41276-02 -34 6.79 7.70 8.70 99 7.70 1.03 24.71 20 7.70 16.70 -33 6.70 7.70 8.70 99 7.70 1.03 24.71 20 7.70 16.70 -33 6.70 7.70 8.70 99 7.70 1.03 24.71 20 7.70 16.70 -33 6.70 7.70 8.70 99 7.70 1.03 24.71 20 7.70 16.70 -33 6.70 7.70 8.70 99 7.70 1.03 24.71 20 7.70 16.70 -33 6.70 7.70 8.70 99 7.70 1.03 24.71 20 7.70 16.70 -33 6.70 7.70 8.70 99 7.70 1.03 24.71 20 7.70 16.70 -33 6.70 7.70 8.70 99 7.70 1.03 24.71 20 7.70 16.70 -33 6.70 7.70 8.70 99 7.70 1.03 24.71 20 7.70 16.70 -33 6.70 7.70 99 7.70 90 7.70 90 7.70 90 7.70 16.70 -33 6.70 7.70 8.70 99 7.70 90 7	194/0205	5.73	2.62	66	.320	1.5		58.1	. 3094E-42		-30, 270
3.54 4.02 ** 420 99 18.78 40.05 440.56 46.7 46.06 47.06 <td>194/0220</td> <td>3.34</td> <td>3.83</td> <td>*</td> <td>394</td> <td>06.</td> <td></td> <td>42.3</td> <td>.4151E-82</td> <td>-13.199</td> <td>-57.036</td>	194/0220	3.34	3.83	*	394	06.		42.3	.4151E-82	-13.199	-57.036
6. 11 6. 87 ** 817 1.10 26 05 33.9 85466-02 -46 6. 86 6. 80 ** .601 1.04 22.30 .53.9 .62646-02 -41 5. 49 6. 16 ** .455 1.01 23.93 .53.9 .41 .41 5. 51 6. 19 ** .455 1.04 22.80 .41 .41 .37 .41 .37 .41 .41 .41 .41 .41 .41 .42	2520/46	3.54	4.02	*	400	66.		10 0	.4405E02	-15.277	-59.350
6. 16 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 16 8.8 6. 17 6. 18	19470323	6.11	6.87	*	.817	1.10		33.9	.8546E-02	-46.780	
5. 49 6.16 ** .455 1.00 23.93 32.5 .7215E-02 -31 5. 53 6.31 ** .492 1.07 23.93 32.5 .7215E-02 -37 5. 63 6.34 ** .566 1.04 22.01 26.9 .6102E-02 -37 5. 54 6. 57 ** .574 .97 15.7 13.9 .402 .17 6. 25 7. 60 ** .374 .97 15.5 .13 .9 .380 .17 .17 .18 .17 .17 .18 .18 .17 .18 <td>191/03.58</td> <td>6.86</td> <td>6.88</td> <td>*</td> <td>109</td> <td>1.04</td> <td></td> <td>15. N</td> <td>.6264E-#2</td> <td></td> <td>-107. 1124</td>	191/03.58	6.86	6.88	*	109	1.04		15. N	.6264E-#2		-107. 1124
5.51 6.19 ** .692 4.07 23.93 32.5 .7215E-402 -39 5.63 6.31 ** .157 .164 22.01 26.9 .6102E-402 -37 5.94 6.67 ** .157 .164 .17 .17 .17 6.75 7.60 ** .374 .97 .10 .17 .37 .17	194/0353	5.49	6.16	*	.455	3.68		57 6	.4743E-02		-85.705
5.63 6.34 ** .566 1.04 22.01 26.9 .6402E-42 -37 5.94 6.67 ** .157 .66 11.40 7.7 16.37E-412 -17 6.75 7.60 ** .374 .97 17.57 13.9 .38169+-02 -35 7.11 8.11 ** .386 .94 16.01 10.9 .40.2 .35 .44 .55 .35 .35 .35 .35 .44 .55 .35 .35 .35 .35 .35 .44 .55 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35 .35	191/0416	5.51	6.19	*	.692	1.87		32.5	. 221.56-1(2		-103.424
5.94 5.67 *** 157 (46 11.40 7.7 1637E-42 -17. 6.75 7.60 ** 371 .97 17.57 13.9 3809E-02 -35. 7.11 8.14 ** 380 .94 16.00 14.9 3.226E-02 -35. 6.73 7.81 ** 393 .97 10.0 14.9 3.226E-02 -35. 6.13 6.18 ** 492 1.01 20.14 20.6 5111E-02 -39. 6.14 6.18 ** 1.04 1.15 29.36 41.7 9190E-02 -26. 6.24 6.41 ** 1040 1.15 29.36 42.0 1086E-01 -55. 6.24 6.88 ** 1.04 1.12 27.20 36.2 9490E-02 -54. 7.34 8.25 99 .734 1.08 24.71 26.0 7691E-02 -54. 7.34 8.25 99 .524 1.08 24.71 26.0 3691E-02 -54. 6.39 7.26 99 .468 1.02 28.99 14.27 3.39 3.39 3.39 3.40 10.3 3.39 3.39 3.39 3.39 3.39 3.39 3.39 3	19470431	5.63	6.31	*	. 566	1.04		56.9	. 6:02E-42	-37.468	-97.370
6.75 7.60 ** 371 .97 17.57 13.9 348(91-02 -35.71 13.9 348(91-02 -35.71 13.9 348(91-02 -35.71 13.9 348(91-02 -35.71 13.9 348(91-02 -35.71 13.9 348(91-02 -35.71 13.9 348(91-02 -35.71 13.9 348(91 -35.71 13.9 34.12)	174/11446	5.74	6.67	*	.157	919		1.1	16.37E-112		-59.208
7.11 B. H1 ** .5H9 .94 t6.00 10.9 .5256E-02 -35. 6.93 7.81 ** .393 .97 16.09 14.2 .412fE-02 -39. 6.13 ** .451 1.00 20.34 .40.0 .45. .39. <t< td=""><td>194/0501</td><td>6.75</td><td>7.60</td><td>*</td><td>. 371</td><td>.97</td><td>12.57</td><td>6.5</td><td>3809r-02</td><td></td><td></td></t<>	194/0501	6.75	7.60	*	. 371	.97	12.57	6.5	3809r-02		
6.93 7.81 ** 393 .97 10.02 14.2 4121E-02 -39. 6.13 6.88 ** 492 1.01 19.34 18.8 4714E-02 -35. 4.74 5.14 ** 492 1.01 20.14 20.6 6.151E-02 -35. 5.46 6.11 ** 1040 1.15 29.36 42.0 11086E-01 -55. 6.21 6.96 ** 1040 1.15 29.36 42.0 11086E-01 -55. 6.21 6.96 ** 100 1.15 29.36 42.0 1086E-01 -55. 6.21 6.96 ** 100 1.15 29.36 1.02 -51. 6.27 7.82 99 .734 1.08 24.71 26.0 7691E-02 -51. 6.90 7.04 99 .394 1.02 28.90 1.75 5502E-02 -49. 6.47 7.26 99 .468 1.00 19.71 14.0 4226E-02 -39. 6.42 7.20 99 .468 1.00 19.71 14.4 4690E-02 -36.	194/0516	/ 11	. E	*		44		\$. 3276E-12		1.65 /6-
6.13 6.68 xx	194/0531			*	393	. 97	10.02	4.2	. 4325E-02		-1114.742
4.24 5.29 ** .492 1.01 20.14 20.6 .51515-02 -26. 5.46 6.11 ** .483 1.12 27.82 41.7 .9496-02 -44. 6.24 6.88 ** .1040 1.15 29.36 42.0 .14865-01 -55. 6.21 6.96 ** .692 1.12 27.20 .87.80 .51.60 -55. 6.27 7.62 29 .734 1.08 24.71 .76.0 .76916-02 -54. 7.34 8.25 99 .524 1.08 24.71 .76.0 .76916-02 -54. 6.90 7.84 99 .534 .98 .16.10 .41.0 .45276-02 -39. 6.47 7.26 99 .484 .98 .16.4 .48916-02 -39. 6.42 7.20 99 .464 .98 .10.14 .48916-02 -39. 6.59 7.39 99 .552 1.03 .21.41 .21.9 .57726-02 -33.	194711546			*	. 451	1.18		18.8	4714F-02		-95. (119
5.46 6.41 ** .483 1.12 27.82 41.7 .9498E-02 -44. 6.14 6.88 ** 1.040 1.15 29.36 42.0 1.086E-01 -55. 6.21 6.96 ** .892 1.12 27.20 36.2 .9318E-02 -55. 6.97 7.82 99 .524 1.08 24.71 76.0 7691E-02 -54. 7.34 8.25 99 .524 1.02 28.90 14.1 45.1 45.1 -48. 6.47 7.26 99 .484 .98 18.32 15.8 4227E-02 -39. 6.42 7.20 99 .464 .98 1.03 21.44 .4890E-02 -35. 6.59 7.39 99 .552 1.03 21.41 28.9 .5722E-02 -33.	194/0601	4.24	5.29	*	. 492	1.01		28.6	. 5111E-02		-73.545
6.24 6.88 ** 1.040 1,15 29 36 42.0 1486E-01 -55.0 6.24 6.96 ** 1.02 1,12 27.24 36.2 93.86E-02 -51.04 36.2 7.82 99 1.02 24.71 76.0 7691E-02 -54.07 7.84 8.25 99 1.524 1.02 24.90 17.5 15502E-02 -449.04 7.7 7.26 99 40 10 19.74 16.10 19.74 16.10 19.24 16.10 19.74 16.10 19.74 16.10 19.74 16.10 19.74 16.10 19.74 16.10 19.74 16.10 19.74 16.10 19.74 16.10 19.74 16.10 19.74 16.10 19.75 17.10 16.59 7.39 99 1.52 1.03 21.41 20.9 1572E-02 -33.0	194/8616	5.46	6.1.1	*	. 483	4.		41.7	.9198E-02		-109.341
6.21 6.96 *** .892 1.12 27.24 36.2 9318E-02 -51. 6.97 7.82 99 .734 1.08 24.71 26.0 7691E-02 -54. 7.34 8.25 99 .524 1.02 28.99 12.5 .5502E-02 -48. 6.90 7.84 99 .394 .98 18.10 14.22 15.8 4227E-02 -39. 6.47 7.26 99 .468 1.00 19.74 18.8 4286E-02 -36. 6.59 7.39 99 .552 1.03 21.41 28.9 .572E-02 -38.	194/0631	6.14	98.9	*		1,15		42.0	.1 (BAE-01		-132.1129
6.97 7.82 99 .734 1.08 24.71 76.0 .7691E-02 -54. 7.34 8.25 99 .524 1.02 28.98 17.5 .5502E-02 -48. 6.90 7.04 99 .394 .98 10.10 14.0 .4527F-02 -39. 6.47 7.26 99 .484 .98 (8.32 15.8 .422F-02 -35. 6.42 7.20 99 .468 1.00 19.70 16.4 .4690E-02 -36. 6.59 7.39 99 .552 1.03 21.41 20.9 .5772E-82 -43.	194/0647	6.21		*	. 892	1,12		36.2	.9.51 BE-02		-126. 428
7.34 8.25 99 .524 1.02 28.90 17.5 .5502E-02 -48. 6.90 7.04 99 .394 .98 10.10 14.0 .4527E-02 -39. 6.47 7.26 99 .404 .98 (R.32 15.8 .422E-02 -36. 6.42 7.20 99 .460 1.00 19.70 16.4 .4690E-02 -36. 6.59 7.39 99 .552 1.03 21.41 20.9 .5772E-82 -43.	194/0742	6.97		66	.734	1.08		26.0	.7691E-#2		
6.90 7.84 99 .394 .98 18.10 14.0 .4527E-02 -39. 6.47 7.26 99 .484 .98 (8.32 15.8 .4226E-02 -36. 6.42 7.20 99 .468 1.00 19.70 16.4 .4890E-02 -38. 6.59 7.39 99 .552 1.03 21.41 20.9 .5772E-82 -43.	194/8717	7.34		66	. 524	1.02		17.5	. 5502E-02		-12:3.219
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6.59 7.39 99 .552 1.03 21.41 28.9 .5725-42 -43.	194/06/02	6.42	7.20	66	.468	9 . 00	19.70	16.4	.4890E-02		-100.163
	194/0012	6.56	7.39	66	. 552	1.03	21.41	2E. 9	. 5772E-42		-118.376

15 MINUSE AVERAGIS. PARASI-TERS

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2.310	deal:	Ton-Tow Heet	= ×	d/cm**2	1.0 X10-3	30%/W3	_ ε	3 5	2**E/B	W/8**
194/0032	6.67	7 48	66	.511	1.02	20 61	4.6.4	. 5349F- 112	-42, 7511	-100 3.36
194701147	6.38		66	351	5.6		-	367115-62	-3.2.919	
194/0902	6.14	6.1113	66	294	. 9.3	15 62	3.9.6	311741-112	-PH 241	-70 233
194/0017	6.11	6.85	66	818	68		2 %	2217F-02	-	-67.690
194/0932	6.11	6.115	66	. 219	607	-	6.9 6.1			11.6 69-
154/0547		7.41	66	.302	60.		11.7	.315BE-112		-05.146
19471002	6.25	7.03	66	. 426	66		17.4	4454E-02	-35.743	-93 309
191/1017	6.33	7.10	46	. 486	1 11		19.4	S000E-02		-100,242
19475032	6.21	6.96	66	365	96.	17.48	1.2	.3012E-112		-146 7111
194/1047			66	. 460	1 0 1		20.5	.50116-32		-9.5.964
194/1102		6.115	66	564	1.04		24 3	.61119E-02		-104.115
194/1117		6.29	66	. 539	1.03		6.68	. 5620E-02		295.16-
194/1132	5.71	6.39	66	. 562	1.13	25.58	4 50	Sh65E-112		Sec. 1102
194/1147	5.91	6.62	66	.386	16	17.75	17.1	4057E-02	-31.540	-B4.611
194/1202		6.H3	66	. 433	6.6	18 95	111.2	45241:-112	-34.877	-91.561
194/1917	5.67	6.34	6.6	. 491	1.01	20 02	22.6	S125F-12	-33.965	-1313.690
174/1232	5 75	6.39	66	365	.96	17.40	16.9	. 3N1 PE-02	650 PG-	-7H 540
194/1247	5.55	6.20	66	27.1	200	14.95	13.5	2H16E-112	-23.237	-60.691
194/13112	5.01	5.59	66	1964	96	11.64	50.6	1706F-112	-13. 1196	-48 617
19471317	5 29	5.91	66	. 0191	67.	61.18	6.2	B436E-03	. · 0.23B	-37, 945
194/1332	4.51	5.02	66	660	Ĭ.	9.05	6.6	1025F-02		-34 B1V
194/1347	4.46	4.97	66	. 171	146	11.89	1.3.6	. (7B) E-02	-11 60.3	4.5 123
194/1402	5.22		66	. 6.8.1	.79	81.19	6.4	. H45HF-11.3	-G. BU7	166 98-
194/1417	5.20	£.0)	66	. 1169	97.	7.57	6.1	.7211E-03	-6.612	-34,279
194/1432	4.51	5.03	66	.019	.70	9.00	-2.4	. 201551-03	2.5119	; -16.335
18471442	4.83		66	. 1126	. 7.3	4 63	-16.1	.2597E-03	995.	-20.146
194/15112	5.17		66	. 058	1.1.	6.93	6.1	6051F-113	-6.199	-31 451
194/1517	5.18		66	. 025	. 72		-386.3	. 2586E-0.3	. 02.3	-21, 312
194/1532	5.30		66	600	. 67	2.67	4	911 HF-04	4.175	-13 205
194/1547	2.67		66	. 042	.75		4.4	4.540 E-0.3	4 272	-29.493
194/1602	5.92		66	.007	.67	2.37	FO:	. 20HOE-04	4.405	-13 460
194/1617	5.88	6.59	4	. 042	. 75		3.9	. 4.54 HE-0.3	-4.819	31, 255
174/1632	6.00	6.72	66	.064	. Z.	7.31	4.2	. 6729E-03		-38 805
179/164/			66	.061	//:	7 10	٦.	6.35760.3	- F. 2.5°	57.547
20/1/8/1			¥ 0	. 869	₹ :		ur. (. 7245E-113		44
/1/1/6/	6.70		/ 6	H-60	9/		N -	50555-05	-11.287	57 . 0.3.3
174/17/56	6.34	7.03	\$ 5	. 023			4 0	SHEEDENNY.	-1.523	20 TO
16/1/6/2				010	6		V 0	00-30501		200 C1-
174/1002			9 6	0110	40.	200	N -	4217225	4.457	-11.547
174/101/	200	3/.0	9 0	+ 6	.04	70.0	- (. 1 950C-05	1.165	-15.540
174/1036			N 1	/20.	2/	4 77	3.5	2871E-113	126.2	-25 895
194/1847			25	500.	. 66			4724F-04	4.970	-9.362
194/1902			5	900.	99.		ev.	. 5956E-114	4.247	-11 355
194/1917			60	.002	. 67	क क ()	· ·	.7491E-04	3,320	-10.650
194/1932	9.50	7.115	22	900	.67		M	.6715E-114	3.713	-9.195
194/1947	7.19	7.73	æ	. 0	. 67	6. 1. 1.	7	. 8079E-04	2.195	-13.720
194/2002	7.70	6.24	E	.015	69.	3.55	7.7	15925-03		-14.464
194/2017	7.23	7.63	61.	500.	99.	<u>∓</u>	er.	. 500.3E-04	3.920	-6.614

ICRS
PRRABB
AVEPAIN S.
THE STATES

Z.21	1A-1W	106-10W deg):	2 ×	(AU 6/cm**2	150 X111-3	11.k	_ £	28	11 21 21 21 21	L w/m*#?
14/2432	6.93		7.9	. 84.3	. 65	1 21	-	35691-04	5.167	
74/2047	5.42	5 66	1.0	. 00.3	6.5	1. (0)	18	27478-114	6.947	-2 550
4/2102	4.07		7.61	. 0.62	.61	111.	0 1	2443F-84	7.613	
7115/6/	5 65		1.1	. 102	10.	2. 6	1 1	. 1070F-02		
14/2132	2.67		1.1	.133	64		2.5	1406E-02		
14/2147	7.47		25	. 169	416		5.9	. 1783F-42		-31 145
74/2202	8.38		5%	187	90	10. KT	5.6	1975E-02	-33 086	
14/25/17	7.60	0.01	76	. 119	.03		4.3	インスをデーエジ		
74722.32	7.67	0.12	1.1	255	3.	1.9 61	7.7	27116-02	-35.264	-42: 780
7475547	5.00 .00			N :	3	60.5.	- : = :	たりこととこのか		
7472502	5 11	5.38	78	.159	.H6		ο. •	. 1677E-02		
74/2317	4.17	1.25	6/	25.5	5	14'. 'B'.	9 = 1	2679E - 02		
74/2332	4.69		.	136	5		1.3 0	14211-12		-
1975397	5.64		50	N : 0 = 0 N : 0	Ē,		185	N = - 187 - 187	-19.674	
2000/5	71.0	n	s ž	1 / N	5.5	200	e n	36374-62	127.983	
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2010/5/	2.50		000	97.6	000	•	20.70	0000000		107.004
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76/0/5/	1 79		10	1 65	E		-144 9	2663F-63		
7.70202	3.20	53.53	65	284	53		27.6	2127E-112	-6 944	٠.
75/4237	4.25	4.61	26	165	Di.	11,66	11.6	171.56-42		29.347
75/0232	2 34	2.56	93	. 052	49.	3 34	4	1256E-03		.3 651
57.02.48	3.52	3.02	64	. 1178	6%	15 03	30.5	807(45-83	-1.574	
75/03/03	3.78	4.83	56	130	.84		10.5	1355E-02	-5 619	-24.754
75/0318	3.54	3.86	96	180.	.79		27.3			
5/0333	3.75	4.11	44	. 125	. 63	30.58	17.6	1297E-02	٠.	
25/0340	3.40	3.04	96	. 067	9.		27.4	9#05E-03		
15/0483	3.46	3.79	96	181	5		24.8	1031E-82		
75/0410	5/75	4. 11	3,6	. 106	Š.		17.	1197E-112		
75/04/55	5.91	4.59	26	.135	5		15.9		-	
8669757 86707 36	5.04 9.04	3.78	/0	960	<u> </u>	2 0	= L	10111107 10111101	13.35%	75.5 DOV
15/11S11B	25.5	4	2.0	175			369		0.0.0	
75/0533	1.68		62	4	613		-154 6	2302E-02		
75/ US4B	1.04	1.10	96	169	. 86		-25.5	17:91:-02	5.903	
509075	1.38	1.47	26	128	. 03	96.4	-17.6	3234E-02		-6.449
75/061A	1.29	1.30	6.6	124	. H.3	10.06	-17.6	_	5.432	
75/0633	.31	.29	1.6	.198	. 88		-2.0.2	.2034F-02	9.497	2.091
25/064B	18	25	6.5	171	.06		-12.0	17556-112	12.086	
5/0743	43		65	.203	65		-30.3	2912F-02	-	5.813
75/0718	44	44	26	.315	47		-47.5	3245E-02		+11.
25/8733	36	56.	62	398	.97	18.84	-120.4	.4099E-02	4.560	
75/0746	•	1.95	21	928.	96.	17.14	316.4	.3699E-02		
25/0803	1.98	2.67	26	.488	5.63	19.99	183.5	. 5033F-02		
25/00110	2.72	2.92	1.6	.409	. 78	18.30	63.9	. 4820F-02	-0.963	51.478

1S MINUTE AVERAGES: PARAMETERS

Z.910	TA-TW dead	TON-TUM dege	Z ×	(4H)	CD X3.0-3	1)* (m/sec	ع ت	Z8 CB	H W/m*#2	E**W/M
195/0833	*****	****	47	.216	60	13 26	*****	. 2215E-02	*****	*****
155/0848	*************************************	********	27	20 EM	· B9	1.5 31	安安子外并於	22318-42	安安安安安安安安	安安安全司司安安安安
19570903	*****	*****	96	.331	56.	16 41	米米沙米米米	33926-62	*****	*******
195/1918	****	芳芳传芳芳芳	96	22.9	96	1.5 65	水子水水水水	. 2346E-162	*****	***心心·***
195/1933	****	***	96	.258	. 51	14 58	本本本本本本本	.2650E-02	******	水水水水水水水水
195/0948	****	****	96	. 246	16	14 16	安安安安全	.2526E-02	经安全公司的	****
195/1003	****	***	96	455	\$?		***	2380F-82	*****	本本本學學學學學
195/1018	新班班特许	発情的を持ち	\$ 0	305	2, 2		· · · · · · · · · · · · · · · · · · ·	23Con 63	***	安全 かららうりゅう
19571048	*****	******	2 0	367	7 6	12.37	· · · · · · · · · · · · · · · · · · ·	37595-02	· · · · · · · · · · · · · · · · · · ·	安全不会安全会会会 安全的 医克里氏病
195/1103	****	****	5.6	373	9.6	17.45	*****	3428E-02	******	****
195/1118	****	米米米米米米	96	474	1 0 0	19.64	仍得将并将按	. 4860E-02	本本本本本本	******
195/1134	水水水水水水	****	96	.331	.95	16.42	安全安全	3395E-02	*****	老本本本本本本本
195/1149	****	****	96	. 411	. O.		关系不清所有	. 4211E-02	转接接头条件专 件	****
195/1204	****	****	ي د د	726	1 OE		****	7453E-02	****	· · · · · · · · · · · · · · · · · · ·
175/1617	*****	· · · · · · · · · · · · · · · · · · ·	7 0	000	ر 20 1		安排 香港等等	40 40 00	-	****
105/1303	****	****	2 3	202	2.0	00 D1	安全 大学	4647E-86	· · · · · · · · · · · · · · · · · · ·	新年年が年本年本 みとものののはよります。
195/1335	4 15	4.20	82	232	0		201	24046-82	10 624	11 949
155/1350		4 0 4	7.8	980	#	8 3.5		117441 0.5	-3 810	2012
195/1405	3.95	3.94	75	.116	. (42		14.8	1198E-82	-5.857	7.451
19571420	4.07	4.04	73	319	66		24.9	3.506F-02	-16.036	004 0
195/1435	4.29	4.26	73	.273	.92	14 97	20.2	20-3650G	-15 564	5.,584.1
19571450	4.47	4.46	7.5	. 203	BG .		1.5.1	. 21441-112	-13, 453	.8. 700
195/1505	4.52	4.58	73	500	06.	٠.	15.9	.2311F-02	-14.693	1.6.3%
1957/598	4.39	4.36	10	. 210	. E.		16.4	. 2255F-162	-13 719	
195/1535	***	****	*	*****	. 87	11.96	***	1803F-02	· 法并并 · · · · · · · · · · · · · · · · ·	****
195/1550	4	4.10	27	. 210	32 € 32 €	1.5.14	17.0	.2176.5-02	12.547	5, 987
195/1605	4.33	4.50	2 6	157	. e	11.35	13.6	1623E-02	-18.406	4.577
195/1620	4.58	4.50	2 6	118	5 0 7 0	# 13 · · · · · · · · · · · · · · · · · ·	5.0.4	1217E-112	-4. 744	\=\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\
195/1650	4 35	4 38	21	- 80	9 8	12.02	- Œ	200475	11.014	1001 2
195/1705	3.72	29.5	7.5	230	6.6	13 98	2 0	2462F-02	-10 744	16 613
195/1720	3.40	3.30	74	. 067	. 78	7.41	12H. 2	.69111-03	7.65	6. 459
195/1735	3.92	3.89	74	218	. 89	13.39	20.3	. 225Bt02	-11.103	4 905
195/1750	4.17	4.15	7.4	. 0.31	.73	5.64	5 6-	3196F-03	1.261	1.532
195/1805	3.47	3.37	73	. 073	.78		42.3	.7584E-63	-1.036	
175/18/0	60	2.04	/3	0.52	.76		5.5	. 541.010.3	. 110	950.4
195/1835			7.3	111	E.		43.9	.1147F02	-1.655	12.687
195/1850			7.3	.112	. 82		-247.1	.1162E-02	336	16.889
195/1905		1.87	7.3	199	. 68	15.79	404 9	.2060E-02	- 464	95.958
195/1920	2.46	20.00	73	960	1 0.		-47.7	9969E-#3	1.382	16.178
195/1935	*	***	62	. 1FE	.67		****	1847E-02	****	-4
195/1750	5.14		15	022	. H.	1.5 50	4. 4.	. 2296E-02	-6.734	
275/2005	4.63	4.13	7	100	3		E .	1881E-02	-10.6130	697.6
175/2020			7	75.1	69	10.75	10.0	1451E-02	-6.114	1.2.920
17372033	4 d	6.16	33	44.	v	30.90	0 406	14985-02	- 297	
175/2050	S. N.	2.0%	5/	.187	N æ.	7.41	49.4	11146-02	1.756	118.566

15 MINUTE AVERAGES. PARAGE U.RS

016.2	TA-IW	WOI-AUT	H	I AH	CD	*	-	0.2	Ξ	ų.
	gbap	gbap	и	d/cm**2	X16-3	CM/Serie	ε	ε	12××12	41/614.45
175/2105	4.65	4.01	7.3	141	84	10 78	1.5	146 36 82	-7 858	25.8. 3
195/2128	3.44	3 35	13	196	Ξ	12.67	5 5.	700356-02		
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195/2205	2.85		7,6	573	· E9		484 5	2.5011-62	572	300 000
195/2220		2.74	1.1	.215	. 8%	13:19	4,4	20-10664	43.11511	11.337
19572735		1.48	11	230	3.	11 76	19.5 6	2	1 260	-
195/2250		1.119	1.1	. 237	0.6	13.5%	0 276	245.46- 02	6.4.8.	
19572305	1.17	.87	41.	.240	5.	14.28	6.00	7.5211-112	4 188	
195/2320	1.72	1.48	1.1	73.57	(F)	1.5.96	4.5.4	. 2456F-02	700	
95/2335	2 74	2.63	3/	169	98.		54 8	1749E-82	800 %-	_
195/2350	1.36	80.7	1.1	199	. 68		V 0.5	206015-02	8.78.8	
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981/0030	5.60	89 5	56	683	1.87		35. 6	718.5107		
911/085.5	29 5	6.43	53	632	1.85	22.98	27.8	. 66.84F 45		
90 YO Y BY	6 64	7.35	86	.343	56.	16. PB	1.5 3	3590F-02	-34.2BB	C14 6/-
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98/0938	4.60	5.27	56	.637	1.05	-	35 0	6620E-02	-31.500	
8540706	4.41	4. 72	6.5	. 687	1.07	7.3.79	4.3	.712BE-02	-29.254	
96/1008	4.53	4.96	5.	744	1.08	24.77	9 4	.772(0C-02	-31.751	-67.78.3
9871823	4.73	5.19	S.	.642	1.06	23.0	36.7	.6671F -82	.31.044	
26/16/58 50/16/52	4. 6.7	4.6%	ر د ر	726	2	24 45	- 7 4	75735F-102	23, 117	
26/1055	9.00	73.5	ה א א	/9/	.0.			//35E-02	620.022	
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9871208	3, 43		56	.687	1.85		55.8	6295E-02	-18.745	
98/1223			64	760	1.09	_	86.9	.7875F-82	-16.838	
9871238			56	.782	1.09	25.37	8 5%	.0109E-02	-19.168	-42.162
9871253	2.65		56	009.	1.04	22.23	816 3	6225,515-0.2	-11.912	-30.793
9071308		3.08	95	476	1.00	19.313	6.69	4943E-02		-31 194
9871323	2.63	2.85	95	. 430	66.	1.00, (62)	71.5	. 44621 112		-56. HPO
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3. 44 3. 73 9.3 3. 85.2 9.1 14 39 3. 11 14 39 3.	198/1539	3.00	4.2.4	5.6	294	7	14.115	÷	25.334 11.2	٠.	_
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5 91 6.45 92 .570 1 04 24 24 59/30F=02 -78,64 .78 10 .78 .61 .78 .61 <t< td=""><td>19871924</td><td>87.5</td><td></td><td></td><td>676</td><td>1.07</td><td></td><td>36 0</td><td>20-15-07</td><td></td><td></td></t<>	19871924	87.5			676	1.07		36 0	20-15-07		
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4 07 4.27 66 .902 1.12 27.29 62.4 .9360E-02 -30.50 -30.57 -40 3.92 4.10 65 1.06 1.15 20.83 73.0 1.0475_01 -50 -50 -40 2.92 3.07 68 .679 1.07 23.84 43.5 7.134E-02 -79.33 -40 2.92 3.07 68 .667 1.05 22.47 13.10 .65.84E-02 -79.33 -40 2.16 2.17 66 .724 1.05 22.47 1.01 22.73 60 -724 1.09 22.05 1.01 72.45E-02 -72.49 -724 1.09 22.05 1.01 72.43 -72.16E-02 -72.49 -72.40 -72.43 -72.16E-02 -72.49 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -72.40 -7	1507.2054	4.46	4.73	6.	. 6141	1.1		11.1	8753.E-112		
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4. 41 4.74 80 .679 1.02 23.88 43.5 713.46 -02 -269.963 -17.52 52.0 37276 -02.43 -17.52 52.0 -02.44 80 .63.8 1.05 22.55 131.0 .63591 -0.433 -17.52 -0.40 -0.433 -17.52 -0.40 -0.40 -0.433 -17.52 -0.40 -0.40 -0.433 -0.72 <t< td=""><td>19872124</td><td></td><td>4.10</td><td>90</td><td>1.004</td><td>1.15</td><td>-</td><td>73.0</td><td>10-375-03</td><td></td><td></td></t<>	19872124		4.10	90	1.004	1.15	-	73.0	10-375-03		
2. 92 3. 07 68 .358 .96 17. 52 52. 0 .37275-02 -9.333 -17. 52 2. 16 2. 17 87 .606 1.05 22. 47 13. 10 .65581-02 -9.549 -6. 2. 16 2. 17 87 .606 1.05 22. 55 13. 10 .65581-02 -9.549 -6. 3. 27 2. 73 86 .729 1.06 24. 59 100.7 .7416-02 -17. 802 -6. 3. 27 3. 39 65 .729 100.7 .7416-02 -17. 802 <td>198721.39</td> <td>4.41</td> <td>4.74</td> <td>90</td> <td>679</td> <td>1.62</td> <td></td> <td>43.5</td> <td>.7134E -02</td> <td></td> <td></td>	198721.39	4.41	4.74	90	679	1.62		43.5	.7134E -02		
2.38 2.44 88 .683 1.05 22.47 131.0 .65381-02 -9.549 -6. 2.16 2.17 87 .616 1.05 22.55 138.5 64046-02 -7.55 1 3.27 3.39 86 .724 1.09 23.06 74.3 .7416-02 -17.800 -17.800 *********** ******** ******* ******* ****** ****** ****** **** ***** <td>19872154</td> <td>. 9. 6.</td> <td>3.07</td> <td>96</td> <td>358</td> <td>.96</td> <td></td> <td>9.55</td> <td>377715-02</td> <td>-9.433</td> <td></td>	19872154	. 9. 6.	3.07	96	358	.96		9.55	377715-02	-9.433	
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177/0935	4.83	5.28	64	959	. 1.	_	47.5	. 893.9E-02		
19970991	4.95	5.41	64	.961	1.14		51.3	. toune-ni	- 40 BIB	
159/1005	4.62	5.06	86	1.245	1.20		70.6	. 1299F01		-
129/1020	4. 53	4.97	5.3	.918	î. E3	52 55	SS 33	. 9596E-62		
1997/1035	4 43	4.08	86	. 763	1.10		6 94	. HJ 03F-02		•
1501/661	4.25	4.65	2	.967	1 14		6.5.4	10:01-41		
199711116	4.36	4.70	63	806·	1 14	28.51	6. (3)	. 5 0 2 4 E - 0 5	_	
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156/7641	4 (5)	36.36	. 6	1.055	91.1		5.75	118.5F - 01	200 .04:	
177/1336	5.73	6.30	54	. 965	1.14	20.33	43.3	10101-01		
15871381	4.90	5.36	5.6	1.512	1.24		H2.3	15791-01	٦.	
197/1406	4.79		93	4.449	1.23	34 67	6.5	.1514F-01	٠.	
19971421	6.72	k 85	93	1.251	1.20	32.36	51.2	131115-01		-112 010
199711436	5.67	6.23	93	1.300	1.22	33,86	6.5.4	14441-03	-57.577	-111,417

15 CHRITTE AVERAGES PARISH (FRS

P.115.7	IA-IW desqE	HVA-TVW deat	z ×	TAB	C10 X10-3	(14 (14	- ε	= = = = = = = = = = = = = = = = = = = =	5. ** ** **	E 4/1442
19971451	5.40	5.43	1 3	1 340	1.2.1	3.3 46	61, 4	19(1)(1)	-5.5 646	-18.5 772
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19971991	5 7.3	62. 9	42	1.548	. 7.55	31, 716	11 69	. 16(1.51" 1) 1		
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15971551	5.13		() ()	1.49.3	42.		1./			
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19971636	5.77		<u>ر</u> د	.617	52	_	1.1.1	6470E-02	-	-
19971651	2 96		Ω. 2	194	Ē.		- 	R328E-02	٠.	
1927/17/16	5.60		~ 6	. 6884	1.10		34 6	H47/56 02:	•	
150/1221	4.165		63	. 64.3	1.06	2.5.47	37 .5	69 396-02		
1977/1736	4 67		67.6	.366	96.		24.7	38766-62	-27. U49	
(9971752	5 24		276	. 52.8	(.02		7. 92	546%-112		
19971087	5.33	5.84	92	. 464	9 . ((0		53.5	4B6.4E-02		-65 077
19971832	4.63	S. 05	6.5	.547	1.03		.3.5 10	. 57166-02		-56 574
19971837	5.00		2	.619	1 0.5		33.3	647.31-02		
19971652	4 65	2.02	92	1.266	1.29		79 6	13945-01	-43.709	-R1 340
19971907	4 N		42	1.256	1.20		75.1	13141-01	916 19-	-78 98
(9971922	4.04		65	6.074	1.16	25 11	74 6	10-38111	-55 211	
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1987/461	4.40	4.91	6	1.500	- N		6.06	15666 - 11		
2007002	4.62	5.87	94	1.464	1.24		114.6	15501-01		
2007002	4.42		44	1.242	1 19	32.40	7.8.7	112926-111		
2007003	4.20	4.60	64	1 517	1.24	35.47	6.66	.1585F01	-41.772	-62 530
2807/005	4.92		64	1 619	1.26		117 7	. (69nE-11)	-52 390	-102 353
204/0107	4.09		94	1.527	1.25	35.58	FX 53	.1595F-01	559 85-	-99.515
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15 NUMBE AVERAGES: PARAMETER

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20070208	3 72		~	.982	1.14		76.5	10226-01		•
240/0/63	3 99	4.33	· .	1.610	-		71.5	1.0515-02	-31.64b	
200/05/30	4 30		5.6	673	7.0.		44 6	.70.66443.	-27, 6019	-
280/0553	4	4.61	7.3	444	66	19.16	3.1 6	46771-42		
20070680	4.33	4.72	6	374	1.6		± . 5. 6.	36936-02		
234/8623	19 6		6.3	617	6.9	65 24	36 9	64301-02	27.7.7.3	
20070638	4 10		6.3	1 033	1.15		20.3	. 1076E -01		
2300/0853	4.05		67.0	1.338	2.		86.5	1.3941. 01	-3% (F'B	
200/0708	4.78	ម ម	6.6	955	1.04		32.6	57361-82	130 85	60 . 1.09
50078753	4.68		2	10%	1.12		±	. 9395F-113		-(13.1.3
240/0738	4.05		6.	1.009	1 16		75.1	. 14.3.31 0.1	53 606	٠,
200700	4 130	S. 7.3	£ .	1.46.3	. 23		6).3	19-49251	-411 541	
200/0808	5. 12	- :	64 64	1.102	1.10		6.6 (9	12341-01	-47.174	
20070024	4 76	5.19	20	1.032	5.	29.73	= = =	10761-01		
500/0035	4 32	4.70	0; (0	1.141	1.17	30 21	7.5.5	. 110HE-01		
2.66/0154	1.5.4	4.6.5	25	1.207	<u>^</u>		5 66	17565-01	-30. 607	7 -611, 5.34
4949/992	. C.		6.6	5.09	٠		S. 1	1670F-01	-40,837	
6.780786c	/	4.7		1.176			5 () ()	12:2603		
45.49/80%	4.61	4.68	3. 5	1.4.51			2 06	1490E-01	-41. 977	
20078794	4.7.5	2.5	N (1.781	3 · ·		101	- H-1/1/41	75. 57.3	
2001/005	4 (38		2 0	1.214	4.19	31.75	67.4	1266F-01	रूप्ता क्रम्म सम्बद्धाः	
6701/111/	1000	4. 40	200	0.62	1.40		21.0	1.4.541 8.1	41.566	
20071050	1	5 0 0 0	u 0	5/4.			=	. 10335F = 03	182.66	
0011/1107	****	*****	200	000 ,	1 . F. 7	200	******	1 1 2 2 2 2 2 2 3 2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	100 · 1.4 · 4 · 4 · 4 · 4 · 4 · 4 · 4 · 4 · 4 ·	F#11 (10)
20071124	4.7.5	4 95	0.00	318	5 2	20.02	######################################	197.35.443	*******	
20071139	4 96		66	1.235	1.19		6 59	1287F - 81	-45 A1B	
28671154	4 65	5, 96	27	1.599	1.26		0.00	1. 1.6.6.6.F D.1.	-40.011	
248/1209	4 65		92	1.504	1.24		0 00	.1570E-01	-46.755	Τ.
24071224	4 47		61 61	1.192	1.11		78.4	12435-111	-41.212	
20071239	4.76		636	1.062	1.16	59 68	59.6	. 1 1 0 GF - 0 1	-40.696	_
20071254	4.69	80.8	55	1.19B	1 19	31 4H	6.83	124HE-81	-42 784	
20071309	4.62		9.1	1.337	1.21		1.1.1	.1394F-01	-44,290	-
238/1324	47.4	ر 3 ت	9.1	1.47.5	4.04		6.5.9	15586-61		
20071339	5.03	2 49	7	1.569	1,25	36 11	0.3.3	. 1643E-#1	-	٦.
20071.554	5000	15,5	7	1.552	52		61.7	1626 01		
200/1409	6.11	6.71	9.1	1.7/7	1.29		75.5	. 1866E-01	~	
280/1424	5 41	5.92	7	1.745	1.28	581.12	£ 55	18316-01		-1119.639
200/1439	4.99	5.45	91	1.631	1.26	36 96	07.0	1752E 01	-53,367	-96. 63B

15 MINUE AVERAGES PRESIDERS

D16. Z	MI-AI Mpab	TVA-TVW Jenff	K X	1AU 4758*2	X 2.0 ×	11.8	∪ ŧ	e .	:**E/3	F 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15
100/1454	5.95	6.52	5	1 749	H.: 1	411 113	76. 6	. 103741:01	-67 946	-116.1.1176
200/1509	5 11.3	5 40	9.1	1 340	- 2:		71 0	1-41(1) -111	-47 315	185 074
20071524	4 25	95. 7		6.19	78.	57 114	- 6%	175147-111		_
20071540	5 T	20. C	5	1.398	~ ₹.		7.5 4	1446661		_
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28071655				16.0	7 -		: « :	131121		
20071710	****	*****	*	****	1.10	78 95	*心本本公本	05611-02		. 44
20071725	4.75	5.119	66	. 033	11	- 1	47.4	HZ07E-32	-35, 1145	-43 902
20071749	5.19	29.5	66	. 682	1.07	97 110	34 9	7133f - h.2		- 71 409
20071755	4 67		6	955	1.6.5		A.3 D	. CB0:1: -02	-2B.034	
20071818	5.37	5.98	5.6	629	1.11	26. 19	40.2	- 6	-	~
208/1825	2.5	6.23	2	669	7.1		31 13			
20071040		5. 6.4 4.4	S o	1492 100			4, 0 5, 4 4, .	CB-4007.4	688 67	215 57
2007/002	78 1	0.00	. 0	014			20.2	00 30000	-	200 77
200717002	5 G.			943		65 7.6	5.0	VII 666 - 42		-86 46.5
20071940	. w	6.96	6	1.025	4.1	29.18	47.9	167.31-11.1	-	_
20371555	5.96	6.52	6	528	1.04	67.73	7.82	. 62021. 02		131 82-
20072010	5.51	6.01	6.6	. 965	1 14	28.35	45 %	.101(E-01	-46.746	Da 1445.
5/10/2/00/2	4.91	5 34	91	. H4B	1 1	26.53	96.8	8867E-02		
20072040	4.39	4.76	5.	. 667	1.06	53.55	42.6	.697.2E-112		
208/2055	# : :	5.44	3	537	1 . 11.3	N.	6.0	. 5619E-02		
20072110	5.63	6 1.5	0 %	. 662	90 +		30.6	1		155 27
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701/01/20 300/00/0	- 0 - 0 - U	5. AB	<u> </u>	1.142	£	27 27	2 19	10-11616	144.075	266.175
0103/047	5. 67 5. 95	-	n o	1.507	- c	200	200	13777-01	7.00 75	
20075240	6.53	7.12	06	664	7.7		30 %	0.57-10-82		
28072255	5.78	6.2.9	0.6	626	1.1.5		41 8	97((6):- 02	47 H29	-44 117
20072311	4 35	4.67	8.6	1 1411	1.17		75 3	1165.6-61	-37.859	-56.370
280/2326	\$ 69	3.00	0.6	560.1	1.16	50 05	11.5.19	11.356-61		-456 0.33
20072341	3.30	3.58	2	119	1.17		6.76	11591-03	-	
748/7556	5.67	3.71	= v	1.595	7.0	3.5 8.6	1.69.1	1.5%3F 0.1	5.5 09.4	738 94-
11007702	707	77.5	4 0	704 6			* : : : : : : : : : : : : : : : : : : :	10 - 30 CO 1	40.570	
266 / 00.04	0 + 0	ם יים	ò	1 564	100			10		
781/18156	4 77	n 17	0.0	896	- - - - -	20.00		04224-02		-44 AS7
201/0111	51	3.31	91	944	1.13		0.40	9749F-02		
20170126	4.37	4.72	92	1 809	68.		11.1	1.0765-01		
201/0141	4 90	5.32	66	2.213	1.34	47 71	130.1	22960E-01	-60 7.57	
20170156	5.33	5.79	9.5	2 492	1.38	45 5.4	57.5	. 25 (H9F - 01)	-70.71.5	-116.145
201/0211	5.45	5.93	9.5	2.766	1.41		134 2	.2074F-61	Τ.	_
20176726	20 I	6.87	6.5	2.044	1.32	41 (1	76.1	. 212515.	•	
205/0241	S S	5.69	63	1.894	1.30		9.5.6	1972E01	- 60.602	-107.580

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2.3110	IA-1W degs	JVA-TVW deqE	2 × 2 ×	TAU d/cm**2	CD X1.0-3	[14] [14]	_ t	5 S	H/M**	F. 42.
20170256	1, 93	17, 9	9.4	2 421	1.57	41 /1	1111. 13	25:37.1-01	76 744	-142 529
20170311	5 37	000 5	5.0	2.367	1 36	44 26	110 6	2400F-01		
20176326	4 159	5 33	7.5	2.091	1 715	41 57	114	2177101	~ 514 . HGS	
20570341	90 8	5. 5. 5.	6	2.118	1.3.5	41 81	113 0	. 22 u SE-03		-100 (400)
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201/84.6		50.5	7.	772	÷ :		:: · • :	. GO 46.E 42		
701/0441		S .	·.	1.690	1.5			1770F-01		
28173456	4	5 7.5	5 6	567.		es (8)	: : :: :: ::	18775-01		7.51 (19)
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20170627		, e	2.0	681			7.	Lieux dr G.S.	Can 1:	
201/0642	. n.	5.61	(N)	563	1.07	23 99	5 5 S	70-4ch72		-71 1.39
2811/8652		5.42	92	.993	1.14		52.8	1 (1.54.15 -1) 1		
201/0712	4.69	5 10	61%	4.009	1.15		27.73	3.053E-03	-37. 052	
20170727	4.97	5.48	22	. 826	1.11	26.14	44.1	. B644E-02	-37 69H	
201/0742	5.61	6.13	6.6	.947	1.13		45.5	98876-02	-47.299	
2017/07/57	ณ ณ บ	5.68	55	. 65 E	1.1.1	26.10	44.6	. 6445E-02	-39.957	
203/0812	5.37	ر ا ا	0	.880	1.10		5 () (5)	(14) 24 - 167	-41 .366	
/340 / 48.	5. E.A.	5.47	3	415	1.62			55546-02	S18 63:-	-53 DEA
2601/102	4.35	4.70	N 0	.502	1.64	DD	4 / X	6.0 - 1 0.9	-26.304	
75307183	14.50	4.46	27.5	1.669	1.16		6.5	11.15111	411 74.5	-6.1.376
21/0/10/2	10 T	0. S. S.	2 2	1 162	= :		4 5 5			-(1) (1.3)
/3/4/10:	2 3	6.7.B	N S	255.			25	1679H: U.		
75607100	и. С. т.	6.00	. c.	1 076		26 H	2.5	11.505.43	- 57. 717	11 4 2 A
20171612	4.56	4.92	3	1 105	1.17		,	1 1 4ch - 61		
2017105	4.76	2.09	N.	1.143	1.17		64.6	.) [187.4-41		
20171842	5.02	5.45	0.6	1.321	1.53		65.0	13735-01	- 40 033	
20171657	4 74	5.17	27.00	1.188	1.18		6.5.9	12.141-01		-74,855
201/1112	5.14	5.59	0.1 S	1.624	1.26		87.0	1690F-01	-55.621	
#2.1.7.1.2.1	5.35	2. 2. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3.	2	1.539	٠. د د د		74.15	16036-01		
26177143	יי יי מיי	30.0 0		3.635	27	36.77		3.78.56 - 63		-104 125
0017/107	70.07		0 0	1.176	7.1	24 . 45		18-16-21	126.755	
0661/106	000	2. 6.7	20	25.5	2 2		9 27	ED 10000		100 000
262/1243		70.0	. 5	3,46	7 7	10 10	0.70	4.34.7E-04		
201/1258	100 N	5.64		1.926	. 3		47.6	10-3'.80c'	-	•
701/1313		5.70	63	1.6114	1.24		20.07	1621F-01		-97, 396
2017352		6.54	16	1.619	1.30		6.65	18.511-111		
201/1343	5.89		66	1.032	1.29		60.2	. 1938F-01	-6H HZ1	Ξ.
20171358	# : []	90°.	16	1.924	1.30	39.16	9.7.6	16965	•	
20171413			0 6	1.607	1.26	36.44	2 / 2 / 2 /	16731-01	-	-67 305
204/102	ν. Α. υ	5.77	# C	1.560	2.65	.55. 74	7.1.3	1.6275-01	1.50 2.52	256 76-
C64.17103	. c	= - - 0	7.1	1.138	1.1/	30.70	F	. 334571-03		200 AM-

15 NUMBE AVERAGES: PARSONETORS

p1G.2	TA-TW	IVA-TUB	¥ ×	TAU	CE	317	_ 8	70	五 五 3 4 4 2 7	T / 3 & % %
	1			and a straight five spile page (seed fact						the flavour and many page ages and a segment
20171456	5 35	5.01	20	140	(%)	\$7.64	0 0	1779.HE-01	157 16	-96.308
201/1513	4.64	50.50	96	₹.S. 1	4.54	3.5. 46	H 1 . ".	15/11/11 61		
20171528	4 56	4.98	7.6	1.514	***	5 5	- 48	11677751		
205/1543	5.24	5.61	16	1 811	60 +	38.70	9 H G	111(06)113		
201715511	3 56	6 H4		1.156	3		55.6	12865-01	-51 701	-B:1, 683
2111/1613	4.69	96 5	0.6	1.1169	1.16		27.7	11116-01	- 47.345	-67, 900
20171620	4.86		36	1.000	1.16		59.1	11.518-10		-68, (78
201/1643	4.75	5.11	36	6.76	1.13		N. 52	95936-02	-	
28 (71651)	5.16	5.63	9.0	1.145	1.18		6.8 7	12.341:18 (554 72-
201/1713	5.89	6 48	26	1.000	1.15	20 . Oll	4.14	10451-01	-51.524	-90.535
2017/17/201	6.16	9 20	16	PB4	61)	28.57	10.1	3 025E-0 (5.4 0.19	
2017/17/44	5.34	8.79	63	1.086	1 15		40 %	. 1 ((47F()1		1.24 66-
65617116	4.77	5.16	16	1.035	1.15	29.74	6.7.3	(477E-101	-4ii 5711	509 79-
20171614	96 6	5.39	9.1	1.024	1.15		S = 2	10671-111	-42 50.5	-72.771
26171189	5.72	5.67	16	606.	8. -	27 55	45.8	9425F - H2	-42. 329	-74 459
201/1644	4.93		9.0	.783	1.0%	55° S	472 5	G1-12518	-36.272	
VIC / 1159	4.95		7.	.666	1.06	1.5 47	9 95.	69461: 45		-611.410
201/1914	4 66	5.29	3.6	.619	1.05	27 63	54.8	64511-02		
6061/146	81 5	5.53	16	1.47	(0.9	24.86	511.7	. 77841 112		
20171944	5.53	6.03	9.1	89.0	1.12	27.1%	41 5	92061-112		-H.2. 61.9
981/109	4.96	5.38	1.5	60.6	1.14	SH . HZ	7.05	SP-TONAG.		-71.000
201/2014	4.77	5.16	9.1	.903	4.12	27.31	5.0.6	9.399F-112	973 75-	66.189
201/2029	5 184	5.47	16	97.6	5.4	27 134	413.9	9265-32	146. PH?	-72,048
20172044	4 62	4.99	,- 	400	1.13	27.60	53.6	91,9116-119	-36.699	-62.3.43
20172059	£.	5.67	-	47.6	- 14	28 32	43.6	. 11114E-91	-44.015	-77 666
2.03 /21.14	16.4	5 38	5	166	1 13		5.11. 4	90.90102	-	
67127197	5.45	56.5	93	11.20	-		2. d)	Bisour - 02	-9.5 4.511	
20172144	5.40	6.34	55	.012	1.50	24. 94	18.17	. (14751:02	-45 784	
20 (72159	4.4%	4. H.3	92	. 903	*	167.72	1 25	9.57 (E- 0.2	-34.7611	
201/2214	4.9%	5.37	6.6	1.210	1 19	35 65	4.4.3	12586-03		_
45557105	. 48	5.98	20	. 740	1.13	27. 5F	1	727.5E-02		-114.457
20178244	2 (17	6.45	26	1.39	1 10	26.19	35.6	(15.76E-11.2		- Hil 937
6538/100	\$ E.A	6.39	<u>ئ</u> ئ	777	1.169	25.57	33.9	611(71-02)		-06.933
2018/2314	5.56	6.87	25	.577	1.84	21.13	27.0	SB. 31-155	-36 178	-71.651
62527192	. 48	5.99	2	4.5.5	66.	14.98	9.0	45.56.1. 182		
20172544	4. /5	5.1%	2.	57.3	3.	13.57	7. 7.5	STATE OF		
20 (72359	4.4	4.76	65	193	Œ.	12.59	5	20 : 13651	- (8.5%)	-30.970
24278814	2.02	5.49	83	. 211	. 85	(1) (1) (1)	17.6	21971-02		
6280/202	3.95	4.24	92	. 162	.86		16.4	167.35 - 112		
242/0045	4.72	5.11	67	2012	. 89	13.65	6 7:5	21451-02		
20278180	5.06	5.40	92	.318	. 94		(. /.)	3.501E-82		
26270115	4 60	5.19	6	. 258	69		= प	20-40922		
202/0130	4% g	6 92	92	160.	011	69. 11	1. 6	. 9505E-6.5		
202/0145	6.76	7.39	2	.063	177	7 7.3	ر د	6502E-0.5	-10.978	-3.3 490
202/0200	4.90	5.29	2	160.	Ξ.	11 67	T N	. 9477E-113		-24.868
202/0215	4 82	5.23	56	. 116	× 5	9 110	5.5	525.00-02	-9.765	
20270230	5.66	9) 9	3	. 652	.76	6.52	٠ <u>.</u>	. 54401 - 16.5	- 5. 085	-24.890
2027/8245	5.61	6.11	2	.649	.76	6.40	9.4	51560 - 03	- 5 331	-23 785

IS MINUE AVERAGES: PARABETERS

Z 31d	ML-61	100-100 degt	13 ×	TAII 4/cm**2	£10 - 3	04	_ £	2.0 C.3	2 × × × × × × × × × × × × × × × × × × ×	E 445/M
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212/0315	5 2	5 87		61.0	7.0	- THE	- 5	1.69.34 - 8.3	1 181	43 000
247/0330	5	5.73	2.	050	7.6	() ()		5224.56-0.3	4.479	136 137
202/0345	6.94	7.61		640.	7.5	4.49		. 2548F-0.5	-3 552	
pay/and	7.20	10.11	91	P 3 H .	69.	.3 4h	1. 4.	150PE-03	97.6	-12 314
24270415	166	H. H8	÷	015	7.0	8 1.9	2.5	1620E-03	-2 541	
202/0430	7.90	19.11	2	0.0	99.	231 6	-3:7.B	1.0.390; -0.3	700	
2112/0445	7 69	H. 48	2.	.007	.67	ر ا ا		75741-84	1 1164	
0050/202	ر م ا	7.01	7	. 011	. 6B	00 3	*C	11355-03	718	
202/0215	0.23	9.11	7	680	89. 9.	7. 7.8	4/1 3	.9764F-(14		
202/0530	6.46	7.80	7	. 183	-	52.6	1. 6	1 11/7/6 6.2		-40 ((1))
202/0545	4.34	9.60	93	.302	6.5	37 H/	26.4	. 402.46 -6.	716 MG-	
0090/202	5.79	2.04	7	326	56		5.5	3.69° 0.2		
202/0615	3.36	3.58	91	. 403	G& :		45	41701-82		_
242/0630	5.40	4. [1]	- ·	233.3	٠٠ خ	52.	5. 65.	19.54 - B2		
707/8645	5.56	3.08	5 3	4.54	>		5 .	4-851-02	228. MEN.	
00/0/202		5.78	Z :	- 5164			2 5	5971107	791.167	VII. 1924
61/9/202	0.00	20.00	2 3	785	50.0		च है इ.स.	20-4047G	4/a . ar-	
0070700	3.01	2 2 2	, 0) i	10.71	2 4 4 4	30 - 350 25		210 027
0007000		000		2000 2000	6.7.0	2 19	0.0%	10 31700		200
903/00/6	0 . 0	0	0 7	404		10 0 0	7 707	41641 03	6/0 0	
05.007.507	n C	0.00	0 1	700	99	7 2 4	2 7	. 1 Mark 10.	7 66.1	
202/0H45	100	2 6	ò	37 %	0	1 6	7 4 9	30 MARCH 25	660 9-	
202/0901	3.10	3.28		222	000		 - 5 - 5	2.546F-03	6 775	80/ 91-
202/0916	3.14	3.35	9.1	555	6.0	13 50		23225-02	-6.876	
792/0951	6/ 2	2.93	9.1	622	0.5	94 30	5 6%	6-111.	-13,463	
2027/0946	2.76	2.95	93	.692	1.07	64 52	BB. d	7129F-82	-14.333	-
202/1801	1.76	1.79	16	. 1331	1.10	26 42	261.4	. 652mm - 02	-6.311	
202/1016	2 52	2.20	44	1.339	1.25	5.5 04	234.0	. 1376E-03	-14.454	
242/1031	1.95	00.0	9.1	1.494	- 24 - 24		277.6	1.0-325-01		-10 626
202/1846	1.83	1.87	5	1.462	1.23		329.3	15881-83		
505/1101	6 4 6	4 5 C	~ 0	1.556	42.1	36 15	527	1707E-01	14.545	741.11-
202/1131	, n	200		1.0.1	1.60		1.000	11.201:-01		-14 554
202/1146	2.30	2.39	9.5	1.200	1.48		107 1	12351-43	-15 388	-
2027/201	1.46	1.49	9.1	1.503	50.		547.2	16245-01	-7.930	
242/1216	1.47	1.47	56	1.591	1.25		558.4	.1633t-01	-7 8.45	383
282/1231	1.30	1.29	16	1.302	1.22		758.B	1419E-01	707.6-	4.850
2112/1246	1 48	1.49	9.1	1.449	1.23		524.7	1489F-01	-7.250	219
202/1301	1.57	. 58	2	1.572	٠. د د د د	35, 82	47.11.15	16165-01	1666 10-	-1.659
202/1316	1.58	65.	50	1.642	1.26		484 2	. 1609681		•
202/1341		2 c c		1.895	1.50		7 400	. 1.9550101	12.671	
212/1340	Di i	26.	9 3	がんこう	1.55	्र इ.स.	3.5 2.5 2.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3	2155-41	٠.	
20271402	7.67	E .	2 0	1.650	97.	56.75	458.9	16951:03		500 to
2007/1417	1.74	л « С	200	1.536	4.7.4	35.17	2.77	15585-83	-	
20271456	1.61	197	7 2	1.764		2 4 7 5	9110	10125-01		.5.452
COC/ 144/	1.78	1.17	, E	3.7//	1.0.1	40.17	4.5%	. 40.55t -03	-13.786	- 5.44

S MUNICE BUERNALS PERSONFILRS

2.010	IA-TW degC	TVA-TVW deat	3 %	100 il/cm4%2	C16 X 1.6 3	114 CB/-FF	_ £	20	E ***/B	F 4/0/4
242/1542	1 157	1.91	613	1.344	1 21	.4.5.1.1	3916	1.5041 - 8.1	-11.6514	-2.67
202/1517	1 91	1.94	68	1.681	1.25	Sec. 17	1, 24, 1	16 101 01	-13 641	627 8-
2027.15.52	10.1	1.82	50	1.676	1.27	32 110	574 3	17246-01	-12.500	-1-664
20271547	1.90	1.93	90	1.665	3.26	36 90	439.9	.1715E-01	-13 849	-4 7/1
202/1602	2.05	2.09	83	1.598	1.31	10 01	346.9	.2651E-01	-17.747	055 0-
202/1617	2.84	5.09	63	2.561	1.30	45 77	4.54 9	2640F-01	-20.664	-6.345
20271632	1.92	5	69	5 . S.	. 30 . 30		4/1 5	10-1205	-10.5118	
202/1647	1.67	1.90	60	2.672	1.40		0 . z . c	.275 4F -01	-18.477	457
たまな1/25%	****	****	* :	**************************************	S :		等 河 等 好 安	23461 - 01	****	· · · · · · · · · · · · · · · · · · ·
71/1/2/12	****	****	* :	****	50 i		****	. 24176-01	*****	*****
20271757	******	*****	* *	**********	 	100	****	281116-81	*****	· · · · · · · · · · · · · · · · · · ·
2001/200	****	****	*	*****	. 2.		***	15371-01	***	***
202/1017	*****	****	*	本本本本本本本	1.73	34.16	本小谷本本本	.1470F-01	本安本本本本安本本	外外本本本本本本
2017504	****	* * * * * * *	*	*****	1.2.		於其亦其此亦	1465-61	本本於本本本於本本	母母所得 作情母母於
20271047	2 70	8.70	0.7	1.611	1 26		100 3	. 1665E-01	-23.05B	-15 737
5081/803	2 7.8	2.78	86	1.800	1.29		205.5	19506-01	-25.86.8	-0.964
202/1917			H.3	1.645	1.26		1169.0	. 170 if 01	-25.257	-
2841/202		2.96	ā	1.447	1.23		149.0	14961-61	-25.72B	
20271947	2 59	. S.	70	1.343	1.21		376.5	1307E-01	-26.801	20.4.91
202/2042	1 47	1.23	1.1.	1.201	H 18		4 1.64	1.17.55 E0.1	-5.015	
202/2012		66.	20	1.345	1.51		31.9 3	. 1389F - 61	9.549	
28.02/202	06	F 1 1	7.5	3. R29	60.		0 trst -	16921-01		
8402/202		-3.67	5	5.570			-160 0	26.661 -01		2.33, 000
5012/202	10.00		2 1	7 . 7 . 5 . 5 . 5 . 5 . 5 . 5 . 5 . 5 .	1.41		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	. 60115E-111	411.787	740 . By -
20272118	96.3		S :	27872	 		7 657	(n - 16866)	45, 163	200 200
20272148	3 19		75	2.644	1 40		9.46	2754F-61	61. 134	272 111
262/2203			. 47	2.667	1 4 5			27771 - 01	4.6 370	
202/2218	-2 60		74	2.832	4.43		- 200 5	2949F-03		
20272233	2.80		7.5	2.968	1.43		. 200	. 3090F - 01		265.962
20272248	4 15		7.5	3.370	1.46		2 293	355 16 - 61		
202/2303	4.98		5 !	3.332	2.47		141	. 3476E-B1	96.270	
20776318	15.43	9.00	T 2	5.50 5.50 5.50 5.50 5.50 5.50 5.50 5.50	1.47		3.50 5	247/21-161	113.663	425.307
262/2348	-5 18		. 4	3 273	1 47	CD 10	- 1 86. 0	3030F-01	67 630	_
243/0003	.5 29		7.4	3.042	1.44		2 721	34446-01	98 243	
203/0018	-5.28	-6.87	7.3	9.869	1.43	40 05	-113 0	3007F-01		
203/0033	-4.91	-6.54	7.3	2.597	4,39		-106.0	.2723E-01	80.151	401.317
20370048	-3.61		7.5		1.39		-141.1	2727t -01		
263/0103	-4.32		72	2.530	1.39		-112.5	.2654E-01		
203/0116	-4.93		7.5	2.050	4.7		-120.5	.2994t-01		_
20.5/0133	-4.55		7	2.689	4		6 07.1	. 20年27年-01		
203/0148	-4.09	-6.56	2	2. es	1.33		F 53-	. 2162E-#1		
2027 02103	14.41	10.5E		1 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1.5/	44.	2 114:	. 755 18E - 0.1	402.50	
0130/07	14.40	0.01		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 4 4 F		136.3	10-10/20	•	
56307600		18.40	= :	75.73	1	47.77	O 0	01201-10		
CU5/UE418	4.6%	-6.42	=	2.223	1.35	4,5 16	2.56-	.2346E-01	79.057	414.460

15 HINOTE, AUGUSTS, PARAGETTERS

TO THE PROPERTY OF THE PROPERT

F) G 2	IA - FW	MAI-VAI	3	IAB	0:0	9:0	_	7.0	=	u
	Sheep	Specto	74	II/CM*#I	X 1 03	Property of	£	5	N#48/2	2***
26.57 0.59.3	-4.66	-6.40	20	2.207	1.36	4.3 7.18	1	29148-41	1.42 61	45.1.499
20370310	-4.34	-6.14	2.0	6.922	1.34	40 14	81 4	20.50) -0.5	21 650	
24.376.35.3	4.76	-6.54	=	1 776	1.29	141 (18)	2 57	1.05/10/01	74 423	390 743
20370408	-4.87	-6.75	2.0	1.801	1.29	_	-2	19056-01	75.063	
2:11.37.042.3	-4 70	.6.53	7.0	1.755	1.20	38 35	9	1814,717-01	٠.	
24 57033B	57.5	-7.24	2	1.924	1.31		7.4.5	.20.57E-01	•	447 1165
7.11 37 11 45.3	4 95	-6.0%	69	2.107	1.34	45.14	11/1 /1	227.525-41	_	
70370500	-4.37	12.2	69	1.706	1.29		112.3	16936 05		
20 2/ 0523	-4.58	-6.41	9%	1.555	1.50		9 69.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		37.9 3.06
203/0538	1.4	-6.47	7.0	1.542	1.25		4 5.5	. 16341-03	-	37/0.245
20.57.0553	4.59	-6.42	2.0	1.364	1.26	36 77	© 554.	16-345-01	-	3111) (11)
809073.02	-4.47		7.0	5.073	1.30	39 71	-11.3 3	19671 -03		406 369
20.370623	-4.37	6.37	9%	1.296	2.7	55 66	5 65-	13776-01		343 B46
243/0638	-4 30	-6 10	= /	1.048	1.16	29.71	-43 1	. 11177-65	606 9%	310.734
03/0653	09 6-	-6 45	7.0	. 20%	1.08	34.56	4.85.	74768-112	P. S. 115.4	277 571
20370708	-4.63	05.9-	69	646	1.06	23 33	-7.3 0	6.045.	51.626	275.156
203/0723	-4.69	1.4.4	69	5.00	1.02	26.96	-17.7	26-795-35	40 632	250 347
20.376738			70	.369	06		1.52	.41.25E-02	44.617	P.72.338
20.370753			2.0	469	1.01	20.29	- 15.9	.5140E-32	49.5HZ	251.012
203/0808			2	.528	1.02	25.05	-16.4	. 560 i E - 02		-
20.370023			0%	619	1.05		-17.6	. 55.64.E-02		
2037,0038		-7.35	7.0	. 800	1.10	58 58	1.96.4	.840PE-02	64.050	
203/06.3		1.56	9%	700	1.10	150. 63	6 52-	82745-02	61.245	
203/0203	-5.39	-7.4B	62	. 551	1.03	21.53	4 95-	. 56:41F-02	85.256	
203/0923	1.36		60	.377	1.6		6 01-	40041-02		2 2 3 0 . 5 9 5
20:370%30		-7.30	67	308	66	10 03	e. 5.	. 44 (BC) E-02	40 357	240.614
20 1/13:3			1.9	. 4.56	6	19.25	-17.1	45556-02		
20.5/1.530		00. W.	67	444	1.00	19.43	-56.3	4744E-02	٠.	2.57 9.50
20.471.35.3		-5.61	67	. 468	1.00	19.70	18.7	. 492(15-02		242.397
203/1408	-3.00	-5.76	89	.497	1.82		6 65-	. 5307E-62	46 603	1562.620
203/1423		-5.30	68	1.349	1.22		17.1.6	. 199.3E- 91		366.161
203/1438		-5.41	63	.949	1.14		45.9	10151-61		37.7 Sec. 3
20371453	3 59	-5.51	6 B	1.797	4.7.0		6.84-	19216 -03		
20.5/1508	-3.20		67	1.520	1.25		-96.1	. 1626E-01		
203/1523	3.39	-4.16	99	1.630	1.27	37.74	517.3	12426-01		
205/15.58	1.74		64	3°.±	1.30		-167.4	1787F-01		
20371553	- 33		6.3		400		-1.51.6	148911-01		
203/1606	-2.67	-4.66	6.1	2.797	1.42	-	5.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50	. 2976t -01		٠.
203/1623	7.7		9		1.35		-163.6	. 2.570E01		481 402
5.0.4/16.4B		-4 (0.3	60	.901	1.13	-	6.17	. 96531-02		343 (16.)
703/1653	6.6)	4.65	9	.768	1.18		44.4	. 02.37E-02	35, 230	315.902
20371700	****	****	*	****	1.11		***	. GID1 6E 02	*****	本本本本本本本本本
20.571723	米米米米米	****	关	****	1 14	250 45	孫明治所作係	. 1020F D1	****	安安安全 以安安安安
24.37.17.5H	大子 本本大	****	*	*****	1.19	31.04	米水水水水水	. 1277F05	******	****
243/1753	***	****	*	***	1.30	39.79	米米米米米米	1994.E-01	於少女子安治中安	外本本本中中本本本
203/1008	****	****	*	****	1.34	42 30	****	27545-115	****	****
203/1823	安全安全安全	***	*	****	1.39	46.47	****	.2721E-01	****	***
203/1838	-2.71	-4.57	99	2.947	1.44	50.11	-217.1	.3163E-II1	54.172	4(19.152

15 HINDLE AVERAGIS. PERGONTERS

					3			ē		-
D (15. Z	Jbaj.	den)C	2 %	17 maxx2	X10-3	Cm/3:07	- 5	= =	2***	:**w/B
28371853	2.60	-4.50	6В	3.134	1 46	51.60	2 15 %	.3.364101	54 932	
203/19#8			67		1.53	59 37	.347 0	. 42924 - 111	56 414	
203/1923	-2.54	-4.36	67		98)		-167.18	. 246(:1111		
283/1938	-2 63	-4.45	67		1.24	1.5 5.1	6.56	15656-81	Τ.	363 43.2
203/1953			63		1.17	50 41	6.5.3	11655-01		. •
203/2000	-2 79		6.3	1.101	1.17	_	5.39-	,11021-01	41.032	_
20.572023	-2.73	-4.59	23		1.27	57 12	-105.6	17.564: -01	-	
20372050	-2.72	٠.	67	2.176	1.35	_	- 11:11	.2335E-01		-
2437245.3	-2.69	-4.53	14		1.34	47: 145	1 651-	25075, 01	40.756	475) 667
203/2100		T.	4.6		1 45		0 250	3231F-61	~	
20472123	49 8		99		1.39	45 30	176.7	,26531:-01		
203/2138	-2.64		S.	2.302	1,30	_	-172.1	.2557F-01	_	-
203/2153			99		4. 3.	_	1.101.7	.2.3106-01	90.347	
203/2208	-2.65	-4 55	99		1.41	47 47	1.44.7	26411-61		
203/2223	15 8-	27 4-	59	2.686	1.4.1	21 /4	7.46.9	. 20086101	99.54%	
203/2238	-2.81	-4.75	59		1.37	14 87	167 3	2537F-111		
203/2253	-2.91	-4.BB	5.9		1.4.5	40 9.3	193.5	3017E-01		507,614
203/2322	-2.01	-4.74	59		1.43		- POS. 3	30676-01	55,275	504, 345
20372337	-2.89	4.79	44		1 61	63.39	-359 6	506.3E-01		
203/2352	-2.97	-4.89	99		1.62	64 76	-369 4	52H3E-(11		₹.
2007/04/2	-3.01	-4.93	99	4 678	1.60		-345 6	. 5017E-01	6.9 36.3	604.736
200/400	-3 00	-4.91	(3)	4.416	1.50	61.37	9 11:5-	47.57E-01		
20470037	-3.04	-C, 1) (I	99	4.718	191	6.8.37	-343.3	5060F -03		61% 076
204/10052	-3.08	-5 03	99	4.130	1.56	88 38	-293 5	44375-01		
244/0147	21 8 - 1	-5.01	99	3.467	1.49		23.5.5 h	.37 (A.E 0)		540 551
2010/1012	-3.11	-5.85	129		1.42	-	-17B S	29536 01		
284/8137	3.10		1,56	2.324	1.37		-146 6	. 2471F 0.1		
204/0152	-3.05		99	2.349	1.37		-157.8	.2519F-01	56. (10.7	
2020/602			59	1 965	1.51		7.42.	2040E-01		
204/0555	-2.98	-4.43	5.9	1 065	30		. 116 7	2000F-01		
7576/407	16 2-		50	2.016	5.3	91.95		.21625-01	٠.	
214/1252	₹			.763	1 10	V	-45.5	. 6162E-63		
7881748X	\$2.54 5.54		64	6/9	70.1		1.565	20 - 1: R.Z.		
204/0365	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-4.75	40	046.		24. 40	1. 1.3	79-30-10-C	790.55	200 102
20470353			6.4	644	1 66		0 67	A9185-02		
264/0487	2 2		9	586				60.000		
204/0422	2.73		65	.001	1 1 1		-45.3	8602F- 02		
264/0437			69	.902	1.13		152 3			
204/0452	-2.73		66	.931	1.14		5.45	1000E-03		
70207604	-8.73		99	865	1.05	_	181	. 6424F-02		261. 495
204/0522		-4.63	67	1.971	1.32	96.06	-132 5	.2116E-01	40.557	418.7.6
244/4537			67	2.1.34	1.34	-	0.96.0	10-916-87	49.634	4.511, 733
204/0525	-2.75	-4.58	09		1.20		-74 4	13035-01	•	
204/0607	-2.74		6.6	. 662	1.07	23 76	4.28.	.710yE-02	34 1116	261 172
284/0622	-2.78	-4.60	99		, 08		-37.E	7474102	٠.	-
704/0637	-2.79		99	1.227	1.20	32.34	-74.7	1.31.7F -#1		342 665
204/0652	-2.71	-4.54	39	2.974	1.44	50.35	-217.8	.3195E-01	54.277	

15 MINDLE AVERALIS, PARADETERS

p.113.2	IA-1W degt	TVA-TVW degt	<u> </u>	TAU d/cm**?); D X (0 · . 5	10; /10;	2.5	2.0	E/###/8	E/8**2
204/0768	-2.67	-4 410	9	1.484	1.25	35, 435	= 7.5	(0-3545)	43.368	36.3 1169
204/0723	59 2-	-4.46	(3)	1.359	1.22	34 04	67.7	14661-011	42 346	
244/4730	69 8	-4.50	633	9:34	1.11		7. T. S	1.0046-01	50 639	300.603
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214/1023	-2.55	-4.20	72	3.522	1.50	54.83	-282.3	3707E-01	-	46.5 262
204710.56	-2.58			3,34%	1.40		7.697	.3597E-01		450,237
209/1053	-2.37	-3.90	?	3.140	1.46		-762 1	3.407F-01		433,435
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204/1123	-2.01	-3.56	72	. 051	1.12	26.98	-60.5	. 91678-02	30.283	247,574
244/1130	-2.12	-3.67	7.3	٠	1. 43	40 40	-242 2	(8-315-8)		395. 034
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5(91/10)	-1.28	-2.78	7.5		1.27	37.15	-179.2	1730E-11		295,603
204/1636	1.27	-2.69	7.5	2.157			256.5	. 23.36F01		330 699
20471045	7.6	-2.40	?	6.4.06				7.58551-01	25.175	325.278
204/1/00	*****	***	* :	******	1.51		***	2071E-01	**************************************	****
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802/0228	-1 49	-2.74	5.	725	1.119	24.87	1 65-	.77H9F-02	768 66	:
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15 ATRULE AVERAGES: PARABETERS

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APPENDIX C: Sample of data available

Three data files are available: 2 second (raw) data; 1-minute average (raw) data; and 15-minute average corrected data, calculated parameters and data quality assessment (variances, flags).

The 2-second data is on digital tape and the 1-minute data is on disc files. A sample listing of each is in Figs C.1 and C.2. The only difference between them is the 1-minute data contains latitude, longitude, ship course and ship speed. The channel numbers are identified in Table 3. 1.

The 15-minute summaries were produced in real time on the ship. Fig C.3 is a sample of the on-line printout. The top line is time; below is latitude and longitude. PLOG is the output of an uncalibrated pilot log; LORSPEED is SHIPS. WS 10 is true wind speed reduced to the 10m level. TW was water temperature from a thermistor towed behind the ship. This channel was highly intermittent since the tow could not remain in the water continuously. SIGMAS are standard deviations over 15-minute intervals of the various quantities. Below is the data quality assessment. BVAR are background variances, RVAL are threshold variances (operator settable) which if exceeded generate a FLAG. 15 data is the 100 min variance of that channel. The bottom contains operator settable options and variables.

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Fig. C.1. Sample listing of 2-second raw data.

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6 MIN = 2 705062 = 0.000000	11178-15854 11178-104884 10-000000 255-12000 89-68840 89-68840 55-1488	4	28.14284 28.14684 36.15386 11.202.71160 10.00000 255.85333 89.60166
HB = 16 MIN = 2.908087 = 2.00000	DATA = 11172.015254 DATA = 11172.015250 DATA = 10.00000 DATA = 255.12000 DATA = 255.12000 DATA = 255.12000 DATA = 255.12000 DATA = 89.62335	DATA = 388.50052 DATA = 695.1 DATA = 1.573333 HR = 16 MIN = 1.573333 DATA = 0.00000 DATA = 3.265863 DATA = 3.265863 DATA = 3.265863 DATA = 3.265863	DATA = 38489 DATA = 36.14080 DATA = 44202.71100 DATA = 46202.71100 DATA = 60000 DATA = 255.85333 DATA = 89.60166
040 HB = 16 MIN = 2.905067 = 1 DATA = 3.264798	9 DATA = 11172.015254 11 DATA = 11172.015250 12 DATA = 10.00000 13 DATA = 255.12000 15 DATA = 255.12000 16 DATA = 89.65235 16 DATA = 89.65335 16 DATA = 89.65335	0 DATA = 38.50252 1 DATA = -69.1 8564 2 DATA = 1.57333 HR = 16 MIN = 1.57333 1 DATA = 0.00000 1 DATA = 0.00000 2 DATA = 3.565802 3 DATA = 3.565802 5 DATA = 3.565802 5 DATA = 3.565802 5 DATA = 3.565802 5 DATA = 3.565802	7 DATA = . 14328 9 DATA = . 28.14080 10 DATA = . 41202.71100 12 DATA = . 11202.71100 13 DATA = . 0.0000 14 DATA = . 255.85333 15 DATA = . 65369 17 DATA = . 65369
2040HB = 16 MIN = 2.905067 = 1 DATA = 0.0000000000000000000000000000000000	10 DATA	20 DATA = 388.570252 21 DATA = -59.1.8552 22 DATA = 1.57333 04 HR = 16 MIN = 1.573333 1 DATA = 0.00000 2 DATA = 0.00000 2 DATA = 3.265563 3 DATA = 3.565802 4 DATA = 3.565802 5 DATA = 3.565802 5 DATA = 3.565802	S

ig. C.2. Sample listing of 1-minute raw data.

DATA VALIDATION AND SUMMARY FOR THE NRL REMOTE SENSING EXPERIMENT: PHELPS..(U) NAVAL RESEARCH LAB WASHINGTON DC J A KAISER ET AL. 26 AUG 83 NRL-MR-5160 HD-A132 105 UNCLASSIFIED

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MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

```
HAYES CRUISE 82-16-09
                                        SC=RM
     192/2356
40 48.68 N 69 17.36 W
LORSPEED = 4.4 kts, PLOG = 12, kts HEAD = 106 deg. CSE = 130 dea
----- CORRECTIONS TO 10m: ------
TA = 14.490 C TDP = 14.362 C WS10 = 5.277 MPS TRUE WD = 101.65
----- CORRECTIONS FOR SHIP ROLL: -----
ROLL SPEED = .0 m/s RMS ROLL = .6
TW = 11.60 C TS = 15.49 C
SAL. = 30.00 SIGT = 22.02 g/cm**3
TA-TW = 2.886 C TDP-TW = 2.757 C eW-e = -.271E+01 mbar
                                 E = -.346E+02 \text{ w/m**2}
H = -.708E+01 \text{ w/m**}^2
TVA-TVW = 2.915 C TVA = 14.57 C
                                TVW = 11.66 C
RH = 99.1602 \% QW-QA = -1.66 g/kg QW = 8.373 g/kg QA = 10.03 g/kg
TAU = .28 d/cm**2 L = 45.6 m
        .002873 cm
Zo =
Cd = .92E-03 Ch = .36E-03 Ce = .13E-02
U* = 15.10cm/sec T* = -.9E-01 C Q* = .00E+00q/kgm
CHAN. 15 FLAG CUM. FLAG. BYAR RYAL 15 DATA
```

0	0	0.0	.1000E-05	.1000E+04	.1451E+01
1	0	0.0	.1000E-05	.1000E+04	.1473E+01
2	0	0.0	. 1000E-05	.1000E+04	.2699E+01
3	0	0.0	.1000E-05	.1000E+04	.4727E+01
4	0	0.0	.1000E-05	.1000E+04	.1379E+00
5	0	0.0	.1000E-05	.1000E+04	.3504E+00
6		0.0	.1000E-05	.1000E+04	.1363E+00
7	0	0.0	.1000E-05	.1000E+04	.3859E+00
8	0	0.0	.1000E-05	.1000E+04	.1549E+02
9	0 0 0	0.0	.1000E-05	.1000E+04	.3000E+02
10	0	0.0	.1000E-05	.1000E+04	.8221E+04
11	0	0.0	.1000E-05	.1000E+04	184E+00
12	0	0.0	.1000E-05	.1000E+04	.1000E+02
13	0	0.0	.1000E-05	.1000E+04	.0000E+00
14	0	0.0	.1000E-05	.1000E+04	.1062E+03
1.5	0	0.0	.1000E-05	.1000E+04	.1250E+01
16		0.0	.1000E-05	.1000E+04	.3027E+02
17	0	0.0	.1000E-05	.1000E+04	2000E-04.
18	0	0.0	.1000E-05	.1000E+04	. 6292E+02
19	0	0.0	.1000E05	.1000E+04	.1266E+02
20					.4081E+02
21					693年+02
55					.4422E+01
23					.1301E+03

OPTIONS: TA.TDP=1 ROLL COR.WIND=1 SHIP COR.WIND=1 WS1.WS2 OR BOTH=1 PA = 1013.00 HT = 10.00 HW = 22.50 DT = 2.00

Fig. C.3. Sample of the 15-minute data and parameter summary provided on-line during the experiment.

APPENDIX D: List of Instruments Used

TA1, TDP1: General Eastern 1200 MPS, S/N 91005-91008

Sensors: TA1: Rosemount PRT 78-39-3, S/N 95014

TDP1: Rosemount PRT 146RB, S/N 14119

TA2, TDP2: General Eastern 450, S/N 95005

Sensors: TA1, TDP1: General Eastern 450B, S/N

WS1, WD1: Teledyne Geotech WS 201, S/N none

(NRL Equipment No. 38417)

Sensors: WS1: S/N 036

WD1: S/N 037

WS2, WD2: Teledyne Geotech WS 201, S/N none

(NRL Equipment No. none)

Sensors: WS2: S/N 095

WD2: S/N 115

TS, CS: Plessey Thermosalinograph 6600T

ROLL: Robinson-Halpern Model 685B, S/N 1588

Seconday Temperature Calibration Standards:

Dymec Quartz Thermometer 2801A, S/N 618-00031

Probes: Ch. 1: S/N 972-1

Ch. 2: S/N 978-20

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Code 2628 Code 5810 Attn: J.A.C. Kaiser	22 cys 22 cys

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